

Generalized Quadrature Spatial Modulation and Its Application to Vehicular Networks with NOMA

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Abstract—Quadrature spatial modulation (QSM) is recently proposed to increase the spectral efficiency (SE) of SM, which extends the transmitted symbols into in-phase and quadrature domains. In this paper, we propose a generalized QSM (GQSM) scheme to further increase the SE of QSM by activating more than one transmit antenna in in-phase or quadrature domain. A low-complexity detection for GQSM is provided to mitigate the detection burden of the optimal maximum-likelihood (ML) detection method. An upper bounded bit error rate is analyzed to discover the system performance of GQSM. Moreover, by collaborating with the non-orthogonal multiple access (NOMA) technique, we investigate the practical application of GQSM to cooperative vehicular networks and propose the cooperative GQSM with OMA (C-OMA-GQSM) and cooperative GQSM with NOMA (C-NOMA-GQSM) schemes. Computer simulation results verify the reliability of the proposed low-complexity detection as well as the theoretical analysis, and show that GQSM outperforms QSM in the entire SNR region. The superior BER performance of the proposed C-NOMA-GQSM scheme make it a promising modulation candidate for next generation vehicular networks.

Index Terms—Vehicular communications, spatial modulation, index modulation, non-orthogonal multiple access, bit error rate.

I. INTRODUCTION

Index modulation (IM) technique utilizes index(es) of transmit antennas, receive antennas, time slots, subcarriers, linear block codes, or other media to transmit additional information without consuming any additional resource [1]–[3]. Due to the good balance between the spectral efficiency (SE) and energy efficiency (EE), IM technique is considered as a promising candidate for the future sixth generation (6G) networks [4].

The IM concept was first applied into the frequency domain, which is incorporated in orthogonal frequency division multiplexing (OFDM) systems. Subcarrier-index modulation OFDM (SIM-OFDM) was proposed to transmit index bits by subcarriers, which suffers from error propagation influence [5]. To mitigate this problem, enhanced SIM-OFDM (ESIM-OFDM) was then proposed to use one index bit to control two

consecutive subcarriers, which activates only one subcarrier in each subcarrier pair [6]. However, compared with the conventional OFDM, the SIM-OFDM and ESIM-OFDM schemes achieve a much smaller SE. Therefore, the OFDM with IM (OFDM-IM) scheme was proposed to solve this problem in [7], which allows to convey more than one index bit. By OFDM-IM, the information bits are divided into two parts, as index bits and modulation bits, where a group of subcarriers is activated to transmit the modulation bits, and index bits are carried by subcarrier activation patterns (SAPs). Note that the mapping between index bits and SAPs is decided by several existing mapping methods, e.g., the combinatorial method in [7] and the equiprobable SAP method in [8]. It is shown in [7] that OFDM-IM outperforms OFDM under the identical SE. Due to this virtue, a lot of research studies of OFDM-IM have been carried out in recent years. For instance, the bit error rate (BER) performance was improved by subcarrier interleaving strategy in [9], [10], and the achievable rate of OFDM-IM was enhanced by optimizing SAPs in [11]. Because of the mapping rule, some SAPs are discarded so as to degrade the system performance. Therefore, the full utilization method of the full set of SAPs was investigated to improve the system performance of OFDM-IM in [12]. Additionally, OFDM-IM was extended to practical applications, e.g., vehicular networks [13] and cognitive radio networks [14]. Besides, the improvement of SE of OFDM-IM has also been studied by many researchers. The OFDM with generalized index modulation (OFDM-GIM) scheme was designed to encode more index bits of OFDM-IM in [15]. In [14], layered OFDM-IM was proposed to increase the SE of OFDM-IM by extending index bits to the layer domain. Moreover, the multiple-input and multiple-output (MIMO)-OFDM-IM scheme was proposed by incorporating OFDM-IM into the conventional MIMO architecture to considerably improve SE of OFDM-IM in [17].

It is observed that the above OFDM-IM related schemes only use the indices of active subcarriers to carry index bits. However, in order to further increase the SE, the generalized dual-mode IM aided OFDM (GDM-OFDM) was designed to transmit the modulated symbols through both active and inactive subcarriers in [18]. Similarly, in [19], [20], (generalized-)multiple-mode OFDM-IM ((G-)MM-OFDM-IM) was designed to transmit the modulated symbols through all subcarriers and the additional index bits are conveyed by the permutation order of distinguished constellations. It should be noted that although the SE improves, the computational complexity for signal detection is greatly increased, especially when the number of subcarriers is large. Therefore, to combat this effect, the low-complexity detection methods for OFDM-

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Recently, spatial modulation (SM), which applies the IM concept into the space domain, is considered as a special case of the MIMO architecture [25]–[27]. Similar to OFDM-IM, the information bits in SM are also split into index bits and modulation bits. By SM, one single transmit antenna is activated to transmit one modulated symbol generated by the modulation bits, and the index bits are conveyed by the index of the active transmit antenna. Because of the activation of a single transmit antenna, SM has appealing features, such as the high EE and free inter-channel interference (ICI). To obtain the higher EE of SM, space shift keying (SSK), which can be considered as a special case of SM, was proposed to only convey the index of the activated transmit antenna in [28]. However, every coin has two sides. SM/SSK obtains the high EE in exchange for sacrificing its SE. In order to figure out the SE problem of SM/SSK, lots of literature has been proposed in [29]–[31]. The generalized SSK (GSSK) and generalized SM (GSM) schemes were proposed to increase the SE of SSK and SM by allowing to transmit multiple transmit antennas in [29], [30], respectively. Relying on expanding index bits into the in-phase/quadrature domain, quadrature SM (QSM) was proposed to achieve the doubled length of index bits than SM in [31] and [32]. Moreover, the SM/SSK scheme was extended to the space-time domain to improve its BER performance, e.g., space-time shift keying (STSK) in [33], space-time block coded SM (STBC-SM) in [34], [35], and differential SM (DSM) in [36], [37]. It should be noted that all above SM related works only utilize the index(ices) of transmit antennas. Differently, (generalised) pre-coding SM ((G)PSM) was proposed to transmit the additional index bits through the index(es) of receive antennas in [38], [39]. To further explore its application, GPSM was extended to the multi-stream and in-phase/quadrature systems in [40] and [41], respectively.

Inspired by QSM, we propose a novel SM scheme, termed generalized QSM (GQSM), to increase the SE of the conventional QSM scheme. To ease signal detection, a near-maximum-likelihood (ML) low-complexity detection is proposed to relieve high detection complexity of the optimal ML detector. The upper bound on the BER performance and the diversity of GQSM are also derived. In addition, we further study the practical application of GQSM into the downlink multi-vehicle relaying network by incorporating the non-orthogonal multiple access (NOMA) technique. Note that NOMA is considered as the promising technique for 6G networks, which splits multiple users in different power levels and simultaneously serve all users at the same time/frequency/space resource [42]–[45]. Specifically, cooperative GQSM with OMA (C-OMA-GQSM) and cooperative GQSM with NOMA (C-NOMA-GQSM) are proposed to investigate the combination of NOMA (OMA) and GQSM in vehicular networks. In multi-vehicle communication systems, one base station (BS) is set to serve two vehicles (vehicle 1 and vehicle 2), where vehicle 1 is located near the BS and vehicle 2 is located far from the BS, which needs one decode-and-forward (DF) relay to assist its transmission [46]. In C-OMA-GQSM, the BS separately transmits signals to two vehicles in two different phases, which results in very poor performance of vehicle 1 but excellent performance of vehicle

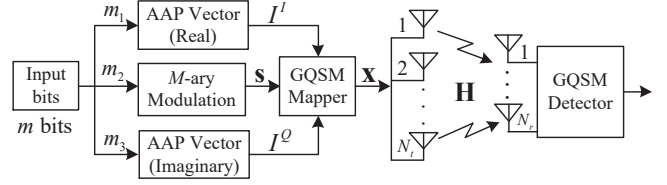


Fig. 1. System model for GQSM.

2. Unlike C-OMA-GQSM, C-NOMA-GQSM combines two vehicles' signals with different power levels and transmits to two vehicles simultaneously. Simulation results show that the GQSM scheme outperforms the conventional QSM scheme, and the proposed low-complexity detection produces the near-ML BER performance. It can also be shown that vehicle 1 (vehicle 2) in C-OMA-GQSM obtains very poor (excellent) BER performance while both vehicle 1 and vehicle 2 in C-NOMA-GQSM achieve comparable BER performance, which is more suitable for practical applications that consider vehicle fairness.

The rest of this paper is organized as follows. The system model, low-complexity detection method, and the upper bound on the BER of GQSM are proposed in Section II. The application of GQSM to OMA/NOMA is investigated in Section III. Simulation results are discussed in Section IV. Finally, this paper is concluded in Section V.

Notations: Upper and lower case boldface letters denote matrices and column vectors, respectively. The complex number field is represented by \mathbb{C} . $(\cdot)^T$ and $(\cdot)^H$ and represent the transpose and Hermitian transpose operations, respectively. \mathbf{I}_M is an identity matrix of size $M \times M$. $\|\cdot\|$ and $C(\cdot, \cdot)$ denote the Frobenius norm and binomial operations, respectively. $\mathcal{R}\{\cdot\}$ and $\mathcal{I}\{\cdot\}$ represent the real and imaginary parts of the argument, respectively. $Q(\cdot)$ represents the Gaussian Q -function [47]. $\text{sort}\{\cdot\}$ denotes the sorting function of the complex argument that sorts the elements in descending order. $X \sim \mathcal{CN}(\mu, \sigma^2)$ represents the distribution of a circularly symmetric complex Gaussian r.v. X with mean μ and variance σ^2 . The probability of an event is denoted by $\Pr(\cdot)$. $\lfloor \cdot \rfloor$ indicates the floor operation.

II. PROPOSED GQSM

A. System Model of GQSM

We first propose the GQSM scheme in Fig. 1 in this subsection. We consider an MIMO system with N_t transmit antennas and N_r receive antennas. By GQSM, p out of N_t transmit antennas are activated for conveying the real part of the modulated signal vectors with the selected antenna activation permutation (AAP) I^I . Similarly, the imaginary part of the modulated signal vectors is transmitted through another p activated transmit antennas, resulting in the corresponding AAP I^Q . Note that the total number of AAPs for the real/imaginary part is $C(N_t, p)$, but only $L = 2^{\lfloor \log_2 C(N_t, p) \rfloor}$ AAPs are adopted for modulation purposes.

As can be seen in Fig. 1, m input bits are split into three parts, m_1 , m_2 , and m_3 , where m_1 and m_3 ($m_1 = m_3$) bits represent the index bits for the real and imaginary parts,

TABLE I
MAPPING TABLE FOR GQSM WITH $N_t = 4$ AND $p = 2$.

index bits	AAP	index bits	AAP
00	{1, 2}	01	{1, 3}
10	{1, 4}	11	{2, 3}

respectively, and m_2 bits stand for the modulation bits generating the modulated signal vector. Specifically, the modulated signal vector $\mathbf{s} = [s_1, s_2, \dots, s_p]$ are first generated by $m_2 = p \log_2 M$ bits, where $s_\tau = s_\tau^I + js_\tau^Q$ with $1 \leq \tau \leq p$, $s_\tau \in \mathcal{X}$, and \mathcal{X} denotes the M -ary constellation set. It should be noted that s_τ^I and s_τ^Q are selected from \mathcal{X}^I and \mathcal{X}^Q , respectively, where \mathcal{X}^I and \mathcal{X}^Q represent the real and imaginary parts of \mathcal{X} , respectively. $m_1 = m_3 = \lfloor \log_2 C(N_t, p) \rfloor$ bits are then utilized to determine the AAP I^I and I^Q so as to transmit the real and imaginary signals $\{s_\tau^I\}_{\tau=1}^p$ and $\{s_\tau^Q\}_{\tau=1}^p$. Let $\mathbf{s}^I = [s_1^I, s_2^I, \dots, s_p^I]$ and $\mathbf{s}^Q = [s_1^Q, s_2^Q, \dots, s_p^Q]$ denote the real and imaginary sets of the the modulated signal vector \mathbf{s} . Let I_α^I and I_β^Q be the α th and β th legal AAPs for real and imaginary parts, respectively, which can be represented by

$$I_\alpha^I = \{i_\alpha^I(1), i_\alpha^I(2), \dots, i_\alpha^I(p)\}, \quad (1)$$

and

$$I_\beta^Q = \{i_\beta^Q(1), i_\beta^Q(2), \dots, i_\beta^Q(p)\}, \quad (2)$$

respectively, where $i_\alpha^I(\eta), i_\beta^Q(\eta) \in \{1, 2, \dots, N_t\}$ with $1 \leq \eta \leq p$. The resulting $N_t \times 1$ signal vectors for the real and imaginary parts are given by

$$\mathbf{x}^I = \{s_1^I, 0, s_2^I, \dots, 0, s_p^I\}, \quad (3)$$

and

$$\mathbf{x}^Q = \{0, s_1^Q, s_2^Q, 0, \dots, 0, s_p^Q\}, \quad (4)$$

respectively. It is worth noting that the non-zero elements in \mathbf{x}^I and \mathbf{x}^Q are decided by AAPs I^I and I^Q . The $N_t \times 1$ transmitted signal vector is finally obtained by

$$\mathbf{x} = \mathbf{x}^I + j\mathbf{x}^Q. \quad (5)$$

For clarity and illustration purposes, we provide an example for the GQSM scheme with $N_t = 4$, $p = 2$ and 4QAM ($M = 4$), including the AAP mapping table, in Table I. The input bits are assumed to be [0 0 1 1 0 1 1]. Accordingly, the first 4 ($m_2 = 4$) bits [0 0 1 1] are mapped into 2 ($p = 2$) modulated symbols $\mathbf{s} = [1+j, 1-j]$, where $\mathbf{s}^I = [1, 1]$ and $\mathbf{s}^Q = [1, -1]$. The second 2 ($m_1 = 2$) bits [0 1] are utilized to select the AAP $I_2^I = \{1, 3\}$ to transmit $s_1^I = 1$ and $s_2^I = 1$ via the first ($i_2^I(1) = 1$) and third ($i_2^I(2) = 3$) antennas for the real part of \mathbf{s} , leading to $\mathbf{x}^I = [1, 0, 1, 0]^T$. The last 2 ($m_3 = 2$) bits [1 1] are utilized to select the AAP $I_4^Q = \{2, 3\}$ to transmit $s_1^Q = 1$ and $s_2^Q = -1$ through the second ($i_4^Q(1) = 2$) and third ($i_4^Q(2) = 3$) antennas, resulting in $\mathbf{x}^Q = [0, 1, 1, 0]^T$. Therefore, the transmitted signal vector is obtained by $\mathbf{x} = \mathbf{x}^I + j\mathbf{x}^Q = [1, j, 1+j, 0]^T$.

Let an $N_r \times N_t$ matrix \mathbf{H} denote the channel matrix whose entries follow the complex Gaussian distribution with zero

mean and unit variance. The $N_r \times 1$ received signal vector is expressed by

$$\mathbf{y} = \mathbf{H}\mathbf{x} + \mathbf{n} = \mathbf{H}(\mathbf{x}^I + j\mathbf{x}^Q) + \mathbf{n}, \quad (6)$$

where the $N_r \times 1$ vector \mathbf{n} denotes the complex Gaussian noise with zero mean and covariance σ^2 . The optimal ML detection can be formulated as

$$\begin{aligned} \hat{\mathbf{x}} &= \arg \min_{\mathbf{x}} \|\mathbf{y} - \mathbf{H}\mathbf{x}\|^2 \\ &= \arg \min_{\mathbf{x}} \|\mathbf{y} - \mathbf{H}(\mathbf{x}^I + j\mathbf{x}^Q)\|^2. \end{aligned} \quad (7)$$

It can be seen from (7) that the optimal ML detection results in the tremendous computation complexity due to a tremendous search space among all possible candidates of the transmitted signal vector \mathbf{x} , especially for large N_t , p , and/or M .

B. Low-Complexity Detection Method

To relieve the detection burden at the receiver employing the optimal ML detection, we aim to propose a low-complexity detection method in this subsection, which considerably reduces the computational complexity.

Let us first separately rewrite the received signal vector into the real and imaginary parts as

$$\underbrace{\begin{bmatrix} \mathcal{R}\{\mathbf{y}\} \\ \mathcal{I}\{\mathbf{y}\} \end{bmatrix}}_{\bar{\mathbf{y}}} = \underbrace{\begin{bmatrix} \mathcal{R}\{\mathbf{H}\} & -\mathcal{I}\{\mathbf{H}\} \\ \mathcal{I}\{\mathbf{H}\} & \mathcal{R}\{\mathbf{H}\} \end{bmatrix}}_{\bar{\mathbf{H}}} \underbrace{\begin{bmatrix} \mathbf{x}^I \\ \mathbf{x}^Q \end{bmatrix}}_{\bar{\mathbf{x}}} + \underbrace{\begin{bmatrix} \mathcal{R}\{\mathbf{n}\} \\ \mathcal{I}\{\mathbf{n}\} \end{bmatrix}}_{\bar{\mathbf{n}}}. \quad (8)$$

We then calculate the weight metric of (8) by equalization as

$$w_\varphi = \bar{\mathbf{h}}_\varphi^H \bar{\mathbf{y}} / (\bar{\mathbf{h}}_\varphi^H \bar{\mathbf{h}}_\varphi), \quad (9)$$

where $\varphi \in \{1, 2, \dots, 2N_t\}$ and $\bar{\mathbf{h}}_\varphi$ denotes the φ th column of $\bar{\mathbf{H}}$. The resulting sum of weight metrics for the real and imaginary parts containing the α th (I_α^I) and β th (I_β^Q) AAPs is obtained by

$$g_\alpha = \sum_{\mu=1}^p |w_{i_\alpha^I(\mu)}|, \text{ and } f_\beta = \sum_{\mu=1}^p |w_{i_\beta^Q(\mu)+N_t}|, \quad (10)$$

where $1 \leq \alpha, \beta \leq L$. Let $\mathbf{g} = [g_1, g_2, \dots, g_L]$ and $\mathbf{f} = [f_1, f_2, \dots, f_L]$, the sequential AAPs for the real and imaginary parts are separately estimated by sorting \mathbf{g} and \mathbf{f} as

$$[a_1, a_2, \dots, a_L] = \text{sort}\{\mathbf{g}\}, \quad (11)$$

and

$$[b_1, b_2, \dots, b_L] = \text{sort}\{\mathbf{f}\}, \quad (12)$$

where a_1 and b_1 denote the positions of maximal values among \mathbf{g} and \mathbf{f} , respectively, and a_L and b_L denote the positions of minimal values among \mathbf{g} and \mathbf{f} . After obtaining the sorted AAPs, the modulated signals for the real part with the a_α th AAP and the imaginary part with the b_β th AAP can be obtained by the zero-forcing (ZF) approach as

$$[\hat{\mathbf{s}}_{a_\alpha}^I, \hat{\mathbf{s}}_{b_\beta}^Q] = \text{demod}((\mathbf{H}_{\text{new}}^H \mathbf{H}_{\text{new}})^{-1} \mathbf{H}_{\text{new}}^H \bar{\mathbf{y}}), \quad (13)$$

where $1 \leq \alpha, \beta \leq L$; $\mathbf{H}_{\text{new}} = [\bar{\mathbf{H}}_{I_{a_\alpha}^I}, \bar{\mathbf{H}}_{I_{b_\beta}^Q}]$, $\bar{\mathbf{H}}_{I_{a_\alpha}^I}$ and $\bar{\mathbf{H}}_{I_{b_\beta}^Q}$ denote the submatrices of $\bar{\mathbf{H}}$ including the

$I_{a_\alpha}^I$ th and $I_{(b_\beta+N_t)}^Q$ th columns of $\bar{\mathbf{H}}$, respectively. The resulting Euclidean distances of AAPs via $\{a_\alpha\}_{\alpha=1}^L$ and $\{b_\beta\}_{\beta=1}^L$ can be sequentially calculated by

$$\epsilon_{(a_\alpha, b_\beta)} = \left\| \bar{\mathbf{y}} - \mathbf{H}_{\text{new}} \begin{bmatrix} \hat{\mathbf{s}}_{a_\alpha}^I \\ \hat{\mathbf{s}}_{b_\beta}^Q \end{bmatrix} \right\|^2. \quad (14)$$

It should be noted that it still leads to high detection complexity by searching all L^2 possible Euclidean distances, especially for large L . In order to further mitigate this problem, we present a detection threshold η and stop calculating the Euclidean distances in (14) once $\epsilon_{(a_\alpha, b_\beta)} < \eta$, which rapidly results in the estimated AAPs $[\hat{I}_{a_\alpha}^I, \hat{I}_{b_\beta}^Q]$ and modulated symbols $[\hat{\mathbf{s}}_{a_\alpha}^I, \hat{\mathbf{s}}_{b_\beta}^Q]$.

After obtaining $\hat{I}_{a_\alpha}^I, \hat{I}_{b_\beta}^Q, \hat{\mathbf{s}}_{a_\alpha}^I, \hat{\mathbf{s}}_{b_\beta}^Q$, the transmitted signal, including the real and imaginary parts, are directly obtained, and the corresponding input bits can be recovered by the demapping of the AAPs and the demodulation of the constellation symbols.

C. Performance Analysis

According to (7), the conditional pairwise error probability (PEP) of detecting $\hat{\mathbf{x}}$ when \mathbf{x} is transmitted on \mathbf{H} is given by

$$\begin{aligned} \Pr \{ \mathbf{x} \rightarrow \hat{\mathbf{x}} | \mathbf{H} \} &= \Pr \left\{ \|\mathbf{y} - \mathbf{H}\mathbf{x}\|^2 > \|\mathbf{y} - \mathbf{H}\hat{\mathbf{x}}\|^2 \right\} \\ &= Q \left(\sqrt{\frac{\|\mathbf{H}(\mathbf{x} - \hat{\mathbf{x}})\|}{2N_0}} \right). \end{aligned} \quad (15)$$

Applying the Q -function approximation [48]

$$Q(x) \cong \frac{1}{12} e^{-\frac{x^2}{2}} + \frac{1}{4} e^{-\frac{2x^2}{3}}, \quad (16)$$

the unconditional PEP can be approximated as

$$\begin{aligned} \Pr \{ \mathbf{x} \rightarrow \hat{\mathbf{x}} \} &= E_{\mathbf{H}} \{ \Pr \{ \mathbf{x} \rightarrow \hat{\mathbf{x}} | \mathbf{H} \} \} \\ &= \frac{1/12}{(\det(\mathbf{I}_{N_t} + q_1 \mathbf{K}\mathbf{A}))^{N_r}} + \frac{1/4}{(\det(\mathbf{I}_{N_t} + q_2 \mathbf{K}\mathbf{A}))^{N_r}}, \end{aligned} \quad (17)$$

where $\mathbf{A} = (\mathbf{x} - \hat{\mathbf{x}})^*(\mathbf{x} - \hat{\mathbf{x}})^T$, $\mathbf{K} = E\{\mathbf{H}\mathbf{H}^H\}$ is the covariance matrix of \mathbf{H} , $q_1 = 1/(2N_0)$ and $q_2 = 2/(3N_0)$. After obtaining the unconditional PEP, an upper bound on BER can be derived according to the union bounding technique as [49]

$$P_e \leq \frac{1}{m2^m} \sum_{\mathbf{x}} \sum_{\hat{\mathbf{x}} \neq \mathbf{x}} d(\mathbf{x} \rightarrow \hat{\mathbf{x}}) \Pr \{ \mathbf{x} \rightarrow \hat{\mathbf{x}} \}, \quad (18)$$

where $d(\mathbf{x} \rightarrow \hat{\mathbf{x}})$ measures the number of bits in error between \mathbf{x} and $\hat{\mathbf{x}}$.

At high SNR (*i.e.*, $\{q_1, q_2\} \gg 1$), (18) can be approximated as

$$\begin{aligned} P_e^I &\approx \frac{1}{m2^m} \sum_{\mathbf{x}} \sum_{\hat{\mathbf{x}} \neq \mathbf{x}} \left(\frac{1}{12q_1^{rN_r}} + \frac{1}{4q_2^{rN_r}} \right) \\ &\quad \times \left(\prod_{\varpi=1}^d \lambda_{\varpi} \right)^{-N_r} d(\mathbf{x} \rightarrow \hat{\mathbf{x}}), \end{aligned} \quad (19)$$

where λ_{ϖ} with $\varpi = 1, \dots, r$ are the non-zero eigenvalues of $\mathbf{K}\mathbf{A}$ and $r = \text{rank}\{\mathbf{A}\}$. The diversity order provided by

GQSM is $N_r r_{\min} = N_r \{\min \text{rank}\{\mathbf{A}\}\}$, which depends on the number of receiver antennas N_r and the minimal rank of \mathbf{A} . Recall that $\mathbf{A} = (\mathbf{x} - \hat{\mathbf{x}})^*(\mathbf{x} - \hat{\mathbf{x}})^T$ and the minimal rank of \mathbf{A} equals one with only one modulated symbol error. Therefore, it is concluded that the diversity order provided by GQSM is N_r , which only depends on the number of receive antennas. Interestingly, the diversity order provided by GQSM is irrelevant to the number of transmit antennas N_t , the number of activated transmit antennas p , and the cardinality of the constellation M .

III. APPLICATION OF GQSM IN COOPERATIVE VEHICULAR NETWORKS WITH NOMA

In this section, we propose two novel schemes, namely C-OMA-GQSM and C-NOMA-GQSM, which apply the GQSM scheme to the vehicular networks utilizing the OMA and NOMA techniques.

We consider a multi-vehicle single-relay cooperative downlink vehicular communication network, comprising one BS with N_t transmit antennas, vehicle 1 and vehicle 2 both with N_r receive antennas, and one DF relay with N_t transmit and N_r receive antennas operating in the half-duplex mode, where the BS aims to transmit two GQSM signal vectors \mathbf{x}_1 and \mathbf{x}_2 generated by m^1 and m^2 bits to vehicle 1 and vehicle 2, respectively. For simplicity, we assume that $m^1 = m^2 = \lceil \log_2 C(N_t, p) \rceil + p \log_2 M$. Note that the vehicle 1 can directly receive the signal from the BS due to the near location, while there is no direct transmission link between the BS and vehicle 2 because of the severe propagation attenuation (long distance). Therefore, one DF relay is assumed to be located between the BS and vehicle 2, which leads to two phases for transmission from the BS to vehicle 1 and vehicle 2. To enable this two-phase transmission, we investigate two relaying transmission schemes, C-OMA-GQSM and C-NOMA-GQSM, in this paper.

A. Proposed C-OMA-GQSM

We first propose the C-OMA-GQSM scheme in Fig. 2, where the BS transmits two $N_t \times 1$ signal vectors \mathbf{x}_1 and \mathbf{x}_2 to vehicle 1 and vehicle 2 in two orthogonal phases (two time slots). The $N_t \times N_r$ channel matrices between BS-to-Vehicle 1, BS-to-Relay, Relay-to-Vehicle 1, and Relay-to-Vehicle 2 links are defined as \mathbf{H}_{BV_1} , \mathbf{H}_{BR} , \mathbf{H}_{RV_1} , and \mathbf{H}_{RV_2} , respectively, where all entries of \mathbf{H}_{BV_1} , \mathbf{H}_{BR} , \mathbf{H}_{RV_1} , and \mathbf{H}_{RV_2} follow the complex Gaussian distribution with $\mathcal{CN}(0, \sigma_{\text{BV}_1}^2)$, $\mathcal{CN}(0, \sigma_{\text{BR}}^2)$, $\mathcal{CN}(0, \sigma_{\text{RV}_1}^2)$, $\mathcal{CN}(0, \sigma_{\text{RV}_2}^2)$, respectively.

Specifically, the BS first transmits \mathbf{x}_2 to the relay in the first phase, and the $N_r \times 1$ received signal vector at the relay can be expressed as

$$\mathbf{y}_{\text{BR}}^{\text{OMA}} = \mathbf{H}_{\text{BR}}\mathbf{x}_2 + \mathbf{n}_{\text{BR}}, \quad (20)$$

where \mathbf{n}_{BR} denotes the $N_r \times 1$ noise vector following the distribution $\mathcal{CN}(0, \sigma_{\text{BR}}^2)$. After receiving $\mathbf{y}_{\text{BR}}^{\text{OMA}}$, the DF relay performs the ML detection to estimate the transmitted signal vector as

$$\hat{\mathbf{x}}_2 = \arg \min_{\mathbf{x}_2} \|\mathbf{y}_{\text{BR}}^{\text{OMA}} - \mathbf{H}_{\text{BR}}\mathbf{x}_2\|^2. \quad (21)$$

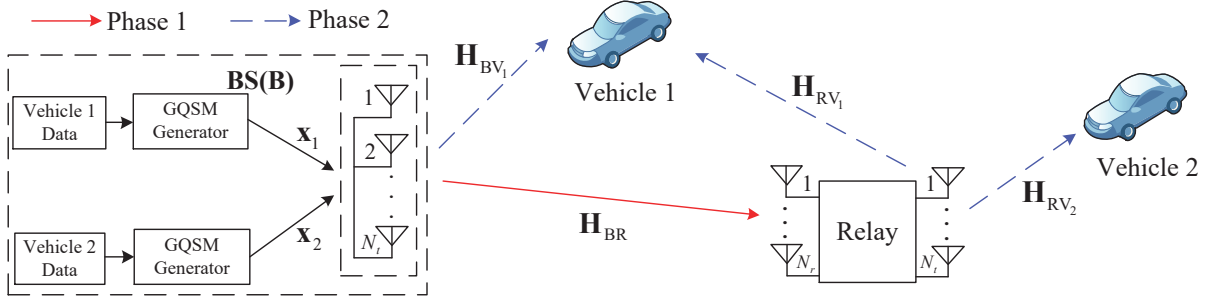


Fig. 2. System model for C-OMA-GQSM.

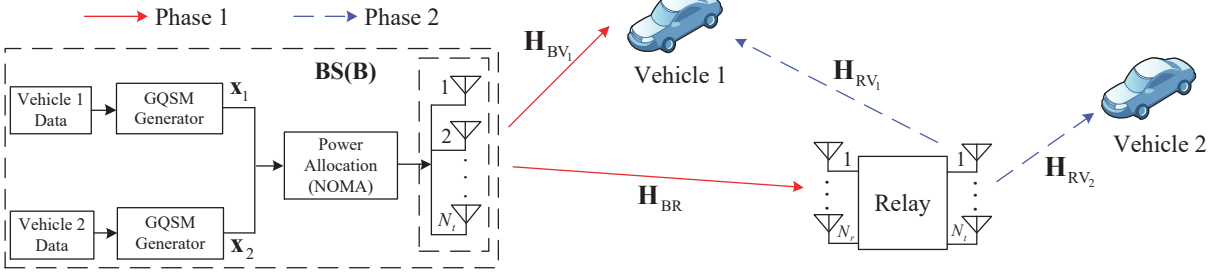


Fig. 3. System model of C-NOMA-GQSM.

In the second phase, the DF relay broadcasts the estimated signal vector $\hat{\mathbf{x}}_2$ to both vehicle 1 and vehicle 2. At the vehicle 2, the $N_r \times 1$ signal vector is obtained by

$$\mathbf{y}_{RV_2}^{\text{OMA}} = \mathbf{H}_{RV_2} \hat{\mathbf{x}}_2 + \mathbf{n}_{RV_2}, \quad (22)$$

where \mathbf{n}_{RV_2} denotes the $N_r \times 1$ noise vector following the distribution $\mathcal{CN}(0, \sigma_{RV_2}^2)$. The transmitted signal vector for vehicle 2 is finally estimated by the ML detection as

$$\hat{\mathbf{x}}_2' = \arg \min_{\mathbf{x}_2} \|\mathbf{y}_{RV_2}^{\text{OMA}} - \mathbf{H}_{RV_2} \mathbf{x}_2\|^2. \quad (23)$$

Meanwhile, vehicle 1 simultaneously receives the signals transmitted from both of the BS and the DF relay, which yields the $N_r \times 1$ signal vector as

$$\mathbf{y}_{U_1}^{\text{OMA}} = \mathbf{H}_{BV_1} \mathbf{x}_1 + \mathbf{H}_{RV_1} \hat{\mathbf{x}}_2 + \mathbf{n}_{U_1}, \quad (24)$$

where \mathbf{n}_{U_1} denotes the $N_r \times 1$ noise vector following the distribution $\mathcal{CN}(0, \sigma_{U_1}^2)$. The transmitted signal vector for vehicle 1 is similarly estimated by the ML detection as

$$\mathbf{x}_1 = \arg \min_{\mathbf{x}_1} \|\mathbf{y}_{U_1}^{\text{OMA}} - \mathbf{H}_{BV_1} \mathbf{x}_1\|^2. \quad (25)$$

It is worth noting that although the detection on \mathbf{x}_2 in (23) is sufficiently reliable, the estimation on \mathbf{x}_1 is very inaccurate due to the non-erasable interference from the DF relay, which results in catastrophic BER performance of vehicle 1. Therefore, the C-OMA-NOMA scheme might not be suitable for certain practical applications, which need to guarantee the average BER performance of all vehicles. Therefore, to relieve this problem, we further propose a more practical scheme in the next subsection.

B. Proposed C-NOMA-GQSM

The system model for the C-NOMA-GQSM scheme is shown in Fig. 3, which still needs two phases to complete the whole transmission. It should be noted that vehicle 1 is near to the BS, and the DF relay is relatively far from the BS, which leads to $\sigma_{BV_1}^2 > \sigma_{BR}^2$. Due to the NOMA principle, the BS will combine two signal vectors by $\mathbf{x}_{\text{ALL}} = \sqrt{\zeta_1} \mathbf{x}_1 + \sqrt{\zeta_2} \mathbf{x}_2$, where ζ_1 and ζ_2 denote the power allocation factors for vehicle 1 and vehicle 2, respectively, and $\zeta_1 + \zeta_2 = 1$ as the transmit power constraint. Since vehicle 1 is near to the BS and vehicle 2 as well as the relay are far from the BS, the BS will allocate more power to user 2 (\mathbf{x}_2) and less power to vehicle 1 (\mathbf{x}_1) by NOMA, which leads to $\zeta_1 < \zeta_2$.

By C-NOMA-GQSM, the BS first broadcasts the combined signal \mathbf{x}_{ALL} to both vehicle 1 and the relay in the first phase. The $N_r \times 1$ received signal vectors at vehicle 1 and the relay can be expressed as

$$\begin{aligned} \mathbf{y}_{BV_1}^{\text{NOMA}} &= \mathbf{H}_{BV_1} \mathbf{x}_{\text{ALL}} + \mathbf{n}_{BV_1} \\ &= \mathbf{H}_{BV_1} (\sqrt{\zeta_1} \mathbf{x}_1 + \sqrt{\zeta_2} \mathbf{x}_2) + \mathbf{n}_{BV_1}, \end{aligned} \quad (26)$$

and

$$\begin{aligned} \mathbf{y}_{BR}^{\text{NOMA}} &= \mathbf{H}_{BR} \mathbf{x}_{\text{ALL}} + \mathbf{n}_{BR} \\ &= \mathbf{H}_{BR} (\sqrt{\zeta_1} \mathbf{x}_1 + \sqrt{\zeta_2} \mathbf{x}_2) + \mathbf{n}_{BR}, \end{aligned} \quad (27)$$

respectively, where \mathbf{n}_{BV_1} and \mathbf{n}_{BR} denote the $N_r \times 1$ noise vectors following the distribution $\mathcal{CN}(0, \sigma_{BV_1}^2)$ and $\mathcal{CN}(0, \sigma_{BR}^2)$, respectively. Vehicle 1 retains the received signal $\mathbf{y}_{BV_1}^{\text{NOMA}}$ and waits for another upcoming signal in the second phase for detection purposes. With the help of the relay, the transmitted signal vector to vehicle 2 can be easily detected

$$\hat{\mathbf{x}}_2 = \arg \min_{\mathbf{x}_2} \|\mathbf{y}_{\text{BR}}^{\text{NOMA}} - \sqrt{\zeta_2} \mathbf{H}_{\text{BR}} \mathbf{x}_2\|^2. \quad (28)$$

In the second phase, the DF relay broadcasts the estimated signal $\hat{\mathbf{x}}_2$ to vehicle 1 and vehicle 2, where the $N_r \times 1$ received signal vectors at vehicle 1 and vehicle 2 are given by

$$\mathbf{y}_{\text{RV}_1}^{\text{NOMA}} = \mathbf{H}_{\text{RV}_1} \hat{\mathbf{x}}_2 + \mathbf{n}_{\text{RV}_1}, \quad (29)$$

and

$$\mathbf{y}_{\text{RV}_2}^{\text{NOMA}} = \mathbf{H}_{\text{RV}_2} \hat{\mathbf{x}}_2 + \mathbf{n}_{\text{RV}_2}, \quad (30)$$

respectively, where \mathbf{n}_{RV_1} and \mathbf{n}_{RV_2} denote the the $N_r \times 1$ noise vectors following the distribution $\mathcal{CN}(0, \sigma_{\text{RV}_1}^2)$ and $\mathcal{CN}(0, \sigma_{\text{RV}_2}^2)$, respectively. Vehicle 2 then performs the ML detection

$$\hat{\mathbf{x}}_2' = \arg \min_{\mathbf{x}_2} \|\mathbf{y}_{\text{RV}_2}^{\text{NOMA}} - \mathbf{H}_{\text{RV}_2} \mathbf{x}_2\|^2. \quad (31)$$

On the other hand, since the signal vector \mathbf{x}_2 transmitted to vehicle 2 has larger transmit power than \mathbf{x}_1 to vehicle 1 ($\zeta_1 < \zeta_2$), the SIC process should be implemented by incorporating the received signal in the first phase $\mathbf{y}_{\text{BV}_1}^{\text{NOMA}}$ before detecting \mathbf{x}_1 at vehicle 1, which is given by

$$\hat{\mathbf{x}}_2'' = \arg \min_{\mathbf{x}_2} \{ \|\mathbf{y}_{\text{RV}_1}^{\text{NOMA}} - \mathbf{H}_{\text{RV}_1} \mathbf{x}_2\|^2 + \|\mathbf{y}_{\text{BV}_1}^{\text{NOMA}} - \sqrt{\zeta_2} \mathbf{H}_{\text{BV}_1} \mathbf{x}_2\|^2 \}. \quad (32)$$

After estimating the signal vector $\hat{\mathbf{x}}_2''$ of vehicle 2, the received signal vector at vehicle 1 is updated by eliminating the interference from vehicle 2 as

$$\mathbf{y}_{\text{BV}_1}^{\text{Update}} = \mathbf{y}_{\text{RV}_1}^{\text{NOMA}} - \sqrt{\zeta_2} \mathbf{H}_{\text{BV}_1} \hat{\mathbf{x}}_2''. \quad (33)$$

The transmitted signal vector to vehicle 1 can be finally estimated by

$$\hat{\mathbf{x}}_1 = \arg \min_{\mathbf{x}_1} \|\mathbf{y}_{\text{BV}_1}^{\text{Update}} - \sqrt{\zeta_1} \mathbf{H}_{\text{BV}_1} \mathbf{x}_1\|^2. \quad (34)$$

Note that the BER performance of vehicle 2 is limited due to the signal detection criterion given in (28) at the DF relay, which suffers from the non-erasable multi-vehicle interference from vehicle 1, so as to bring the error floor on BER of vehicle 2. However, unlike the catastrophic BER performance of vehicle 1 in C-OMA-GQSM, vehicle 1 in C-NOMA-GQSM achieves comparable BER performance with the aid of the DF relay in (32) and the SIC process in (33), which successfully suppress the interference from vehicle 2 to some degree. Despite of the existence of error floor, the BER performance of vehicle 1 in C-NOMA-GQSM systems is significantly improved compared with that of vehicle 1 in C-OMA-NOMA systems. Therefore, it is concluded that the C-OMA-NOMA scheme has better BER performance of vehicle 2, while the C-NOMA-GQSM scheme achieves better overall average BER performance, which makes C-NOMA-GQSM more suitable for practical applications.

IV. SIMULATION RESULTS

In this section, we present computer simulation results to evaluate the BER performance of GQSM systems under the

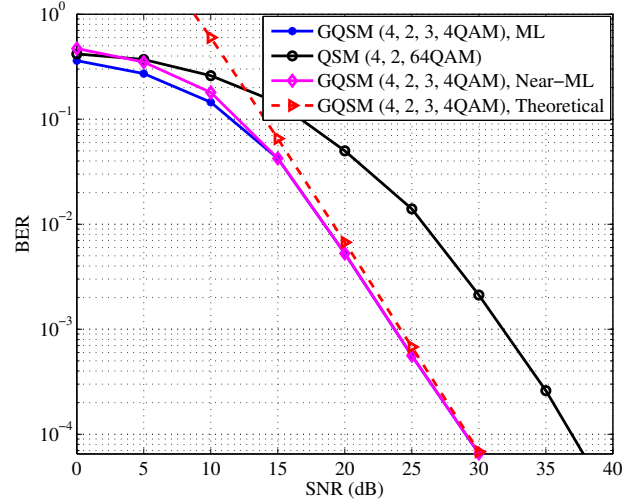


Fig. 4. Performance comparison between GQSM and QSM with $N_t = 4$, $N_r = 2$, and $m = 10$.

assumptions of Rayleigh fading channels and perfect channel estimation. For the sake of simplicity, we denote “GQSM ($N_t, N_r, p, MQAM$)” as the GQSM scheme with N_t transmit antennas, N_r receive antennas, p activated transmit antennas and M -ary QAM constellation, and “QSM ($N_t, N_r, MQAM$)” as the QSM scheme with N_t transmit antennas, N_r receive antennas, and M -ary QAM constellation. The detection threshold η is set to be $2N_r\sigma^2$ for the proposed low-complexity detection.

In Fig. 4, we compare the BER performance between GQSM and QSM schemes with $N_t = 4$, $N_r = 2$. It can be seen that GQSM (4, 2, 3, 4QAM) achieves a large performance gain than QSM (4, 2, 64QAM) both with 10 input bits in the entire SNR region. Specifically, compared to QSM (4, 2, 64QAM), GQSM (4, 2, 3, 4QAM) obtains almost 6 dB SNR gain at $\text{BER}=10^{-2}$ and obtains up to 8dB SNR gain at $\text{BER}=10^{-4}$. This is because GQSM significantly increases the length of index bits, which improves the system performance. From Fig. 4, it can also be seen that the theoretical curves perfectly match the simulation results in the high SNR region, which validates our analysis in Section II. C. Moreover, we can see that the proposed low-complexity detection (near-ML) closely approaches the optimal ML detection for GQSM (4, 2, 3, 4QAM). To be more specific, the BER curve of the low-complexity detection is close to that of the ML detection with a trivial performance loss in the low SNR region, while the BER curves of the low-complexity and ML detection almost coincide in the high SNR region.

We further compare the BER performance between GQSM and QSM schemes with $N_t = 8$, $N_r = 4$, $m = 12$ bits in Fig. 5. Similar to Fig. 4, GQSM (8, 4, 2, 4QAM) still outperforms QSM (8, 4, 64QAM) with a large performance gain, especially in the medium-to-high SNR region. At $\text{BER}=10^{-4}$, GQSM (8, 4, 2, 4QAM) acquires about 10 dB SNR gain compared with QSM (8, 4, 64QAM), which attributes to the benefit of a larger number of index bits in GQSM. It can be also seen in this figure that the theoretical curve matches

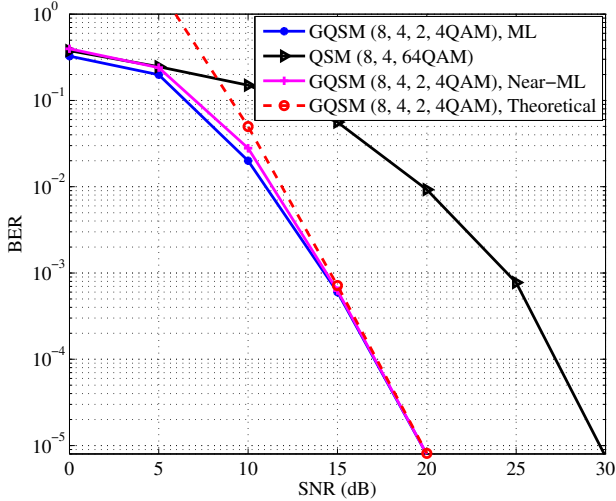


Fig. 5. Performance comparison between GQSM and QSM with $N_t = 8$, $N_r = 4$, and $m = 12$.

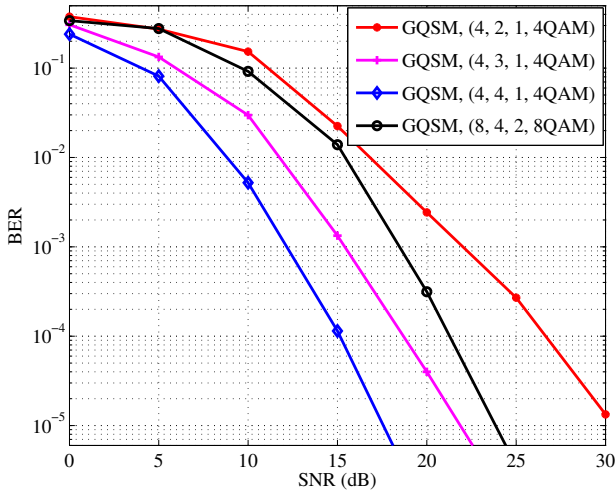


Fig. 6. Diversity comparison of GQSM with different configurations.

the simulation curve very well for GQSM (8, 4, 2, 4QAM) in the high SNR region. In addition, the low-complexity detection still tightly approaches the optimal ML detection with a negligible performance loss. It is worth noting that the BER performance of the low-complexity detection is greatly affected by the detection threshold η .

To evaluate the diversity of the proposed GQSM, we compare the BER performance of GQSM (4, 2, 1, 4QAM), GQSM (4, 3, 1, 4QAM), GQSM (4, 4, 1, 4QAM), and GQSM (8, 4, 2, 8QAM) in Fig. 6. It is shown from Fig. 6 that GQSM (4, 2, 1, 4QAM) achieves the smallest diversity order as 2 ($N_r = 2$). As only increasing N_r , GQSM (4, 3, 1, 4QAM) reaches a higher diversity order as 3 ($N_r = 3$). By keeping increasing N_r up to 4, GQSM (4, 4, 1, 4QAM) obtains the diversity order of 4 ($N_r = 4$), which indicates that the diversity order of GQSM is continuously increased by only changing the number of receive antennas N_r from 2 to 4. To further explore the diversity

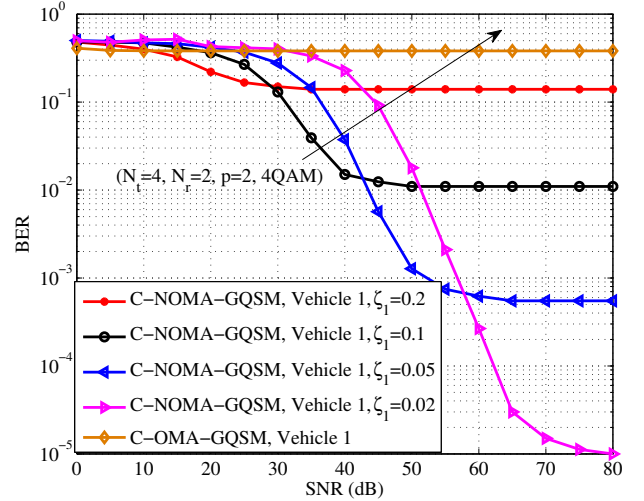


Fig. 7. Performance comparison of vehicle 1 in C-NOMA-GQSM and C-OMA-NOMA with $N_t = 4$, $N_r = 2$, $p = 2$, and 4QAM.

property, we compare the BER performance between GQSM (4, 4, 1, 4QAM) and GQSM (8, 4, 2, 8QAM), which shows that GQSM (4, 4, 1, 4QAM) achieves the same diversity order ($N_r = 4$) as that of GQSM (8, 4, 2, 8QAM) by only changing the number of transmit antennas N_t , the number of activated transmit antennas p and the cardinality of constellation M . Therefore, we can conclude that the diversity order of GQSM is only related to N_r and irrelevant to N_t , p and M , which verifies the analysis of the diversity order in Section II. B.

Fig. 7 presents the BER performance comparison of vehicle 1 between C-OMA-GQSM and C-NOMA-GQSM with $N_t = 4$, $N_r = 2$, $p = 2$, and 4QAM. It can be seen from Fig. 7 that vehicle 1 in C-OMA-GQSM has very poor performance, which leads to the constant BER=0.4 in the entire SNR region, while vehicle 1 in C-NOMA-GQSM achieves superior BER performance with different power allocation factors (ζ_1). Specifically, vehicle 1 with $\zeta_1 = 0.2$ obtains the relatively poor performance and exhibits the ineradicable error floor for $\text{SNR} > 35\text{dB}$. The performance of vehicle 1 with a smaller value of $\zeta_1 = 0.1$ becomes better and as low as the error floor of $\text{BER} = 10^{-2}$ for $\text{SNR} > 50\text{dB}$. Keeping decreasing the power allocation factor to $\zeta_1 = 0.05$, vehicle 1 obtains much better BER performance and the error floor appears only for $\text{SNR} > 65\text{dB}$. Setting $\zeta_1 = 0.02$, vehicle 1 obtains the best BER performance in Fig. 7, and the error floor appears merely in the range of $\text{SNR} > 80\text{dB}$, which can be ignored in practical situations. Based on the above results, we can observe that allocating less power to vehicle 1 will greatly improve its BER performance and postpone the occurrence of the BER error floor in the medium-to-high SNR region. This is because of the fact that allocating less power to vehicle 1 is equivalent to allocate more power to the DF relay, which is beneficial to the SIC process of vehicle 1 in the second phase so as to improve the BER performance.

Fig. 8 shows the BER performance comparison of vehicle 2 between C-OMA-GQSM and C-NOMA-GQSM with $N_t = 4$, $N_r = 2$, $p = 2$, and 4QAM. From Fig. 8, we can see that

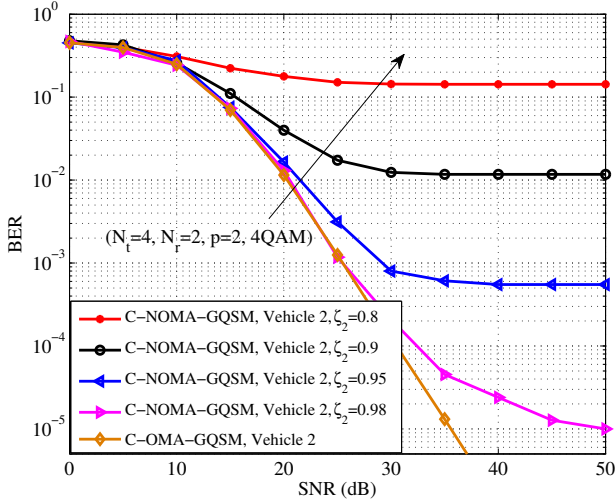


Fig. 8. Performance comparison of vehicle 2 in C-NOMA-GQSM and C-OMA-NOMA with $N_t = 4$, $N_r = 2$, $p = 2$, and 4QAM.

vehicle 2 by C-OMA-GQSM achieves the best BER performance and by C-NOMA-GQSM successively approximates to that in C-OMA-GQSM with increasing its power allocation factor ζ_2 . To be specific, vehicle 2 with $\zeta_2 = 0.8$ obtains undesirable BER performance and the error floor arises at about $\text{BER}=0.4$. Allocating more power with $\zeta_2 = 0.8$ yields better BER performance of vehicle 2 even if it is still worse than that of C-OMA-GQSM. Note that the error floor is delayed at $\text{BER}=10^2$ for $\text{SNR}>35\text{dB}$. Keeping increasing the power allocation factor up to $\zeta_2 = 0.9$, vehicle 2 obtains much better performance and the BER error floor on $\text{BER}=5 \times 10^{-4}$ appears for $\text{SNR}>40\text{dB}$. It should also be noted that the BER curve of vehicle 2 with $\zeta_2 = 0.9$ is closer to that of C-OMA-GQSM. Finally, the BER curve of vehicle 2 with a larger value of $\zeta_2 = 0.98$ obtains the best performance with the error floor of $\text{BER}=10^{-5}$, which approaches the BER curve of vehicle 2 by C-OMA-NOMA much closer. Therefore, despite of the error floor, we conclude that the BER performance of vehicle 2 in C-NOMA-GQSM tightly approaches that of vehicle 2 using C-OMA-GQSM in the medium-to-low SNR region. As can be seen from Figs. 7 and 8 that the C-OMA-GQSM scheme has the extreme situation of BER and brings consistently poor performance to vehicle 1 but the excellent performance to vehicle 2. However, the BER performance of vehicle 1 and vehicle 2 in C-NOMA-GQSM systems is gradually improved as ζ_1 (ζ_2) decreases (increases), which verifies the analysis in Section III that the C-NOMA-GQSM scheme is more suitable for practical purposes. In addition, we also find that vehicle 1 and vehicle 2 utilizing C-NOMA-GQSM finally achieve the same BER performance in the high SNR region, which guarantees the overall system performance and reliability.

To further validate our observations, we compare the BER performance of vehicle 1 and vehicle 2 in the contexts of C-OMA-GQSM and C-NOMA-GQSM with $N_t = 8$, $N_r = 4$, $p = 1$, and 4QAM in Figs. 9 and 10. Similar to Fig. 7, vehicle 1 with different values of ζ_1 employing C-NOMA-GQSM achieves better performance than that of C-OMA-

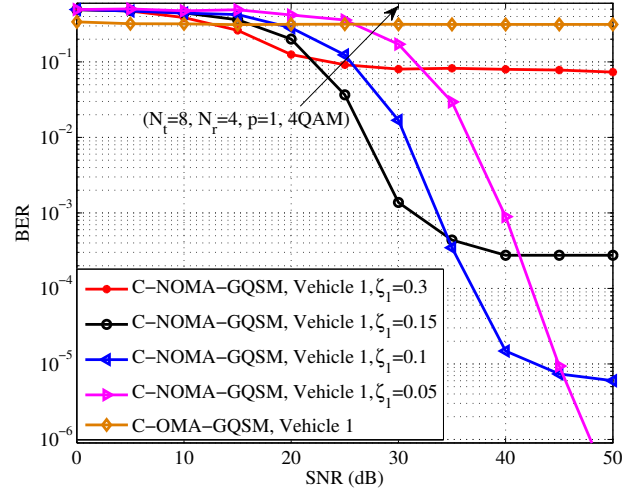


Fig. 9. Performance comparison of vehicle 1 in C-NOMA-GQSM and C-OMA-NOMA with $N_t = 8$, $N_r = 4$, $p = 1$, and 4QAM.

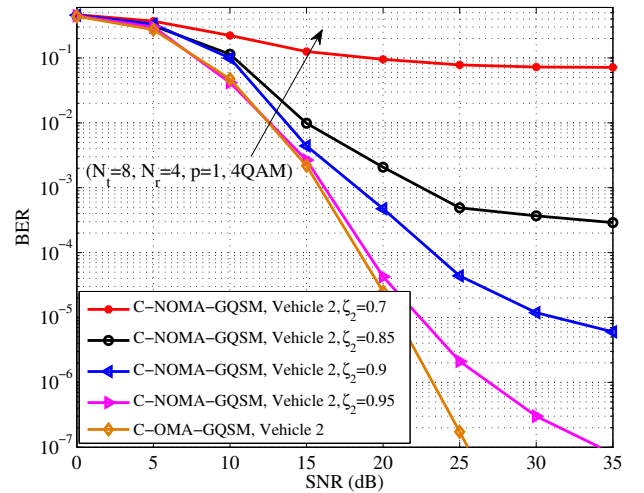


Fig. 10. Performance comparison of vehicle 2 in C-NOMA-GQSM and C-OMA-NOMA with $N_t = 8$, $N_r = 4$, $p = 1$, and 4QAM.

GQSM, where the BER of vehicle 1 employing C-NOMA-GQSM monotonously decreases when increasing ζ_1 . Note that the error floor of vehicle 1 comes out with a very small BER if ζ_1 is small enough. For example, the error floor of vehicle 1 arises at $\text{BER}=6 \times 10^{-6}$ with $\zeta_1 = 0.1$, and the error floor of vehicle 1 may arise at even a lower BER (this has not been shown in Fig. 9) with $\zeta_1 = 0.05$, which indicates that vehicle 1 utilizing C-NOMA-GQSM is able to obtain sufficiently good performance as long as ζ_1 is low enough. Meanwhile, we can figure out from Fig. 10 that the BER curves of vehicle 2 in C-NOMA-GQSM systems are able to closely approach those corresponding to C-OMA-GQSM with a larger value of ζ_2 in the medium-to-low SNR region, even if the error floor still exists. This further corroborates that the proposed C-NOMA-GQSM scheme is more suitable for large-scale multi-vehicle communication systems with large numbers of transmit and

receive antennas.

V. CONCLUSIONS

In this paper, we proposed the GQSM scheme to increase the SE of the conventional QSM scheme by allowing activating more than one active transmit antenna in in-phase and quadrature domains. By GQSM, the transmitted signals are divided into real and imaginary parts and conveyed by their corresponding active transmit antennas, which makes index bits double. A near-ML low-complexity detection was designed to greatly reduce the computational complexity of the optimal ML detection. An upper bound on BER and the diversity order were analyzed to evaluate the performance of GQSM. Moreover, we proposed the C-OMA-GQSM and C-NOMA-GQSM schemes to further investigate the practical application of GQSM by resorting to the NOMA technique. Simulation results have discovered that GQSM obtains a significant performance gain compared to QSM in the entire SNR region, and validated the effectiveness of the low-complexity detection and theoretical analysis. Besides, simulation results have also revealed that compared to C-OMA-GQSM, C-NOMA-GQSM achieves better average BER performance and is thereby more suitable for multi-vehicle communication networks, in which vehicle fairness is of key importance.

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