

# IMPERIAL

# High-Rate Fracture Testing Methods

Fixed Energy Input (Pendulum) vs. Speed Controlled (Servo-hydraulic) Experimental Procedures

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DSDS 24 – Cranfield University, Museum of the Great Western Railway

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# Standard 'Rapid' Fracture Methods

Toughness changes with Speed

ASTM E1820-*Ap.14&17*

ASTM E399-*Ap.10*

BS 7448-3-*Ap.A*

BS ISO 26834:2015

Same equations as static: Assume Negligible Inertia

Charpy preferred - mature technology

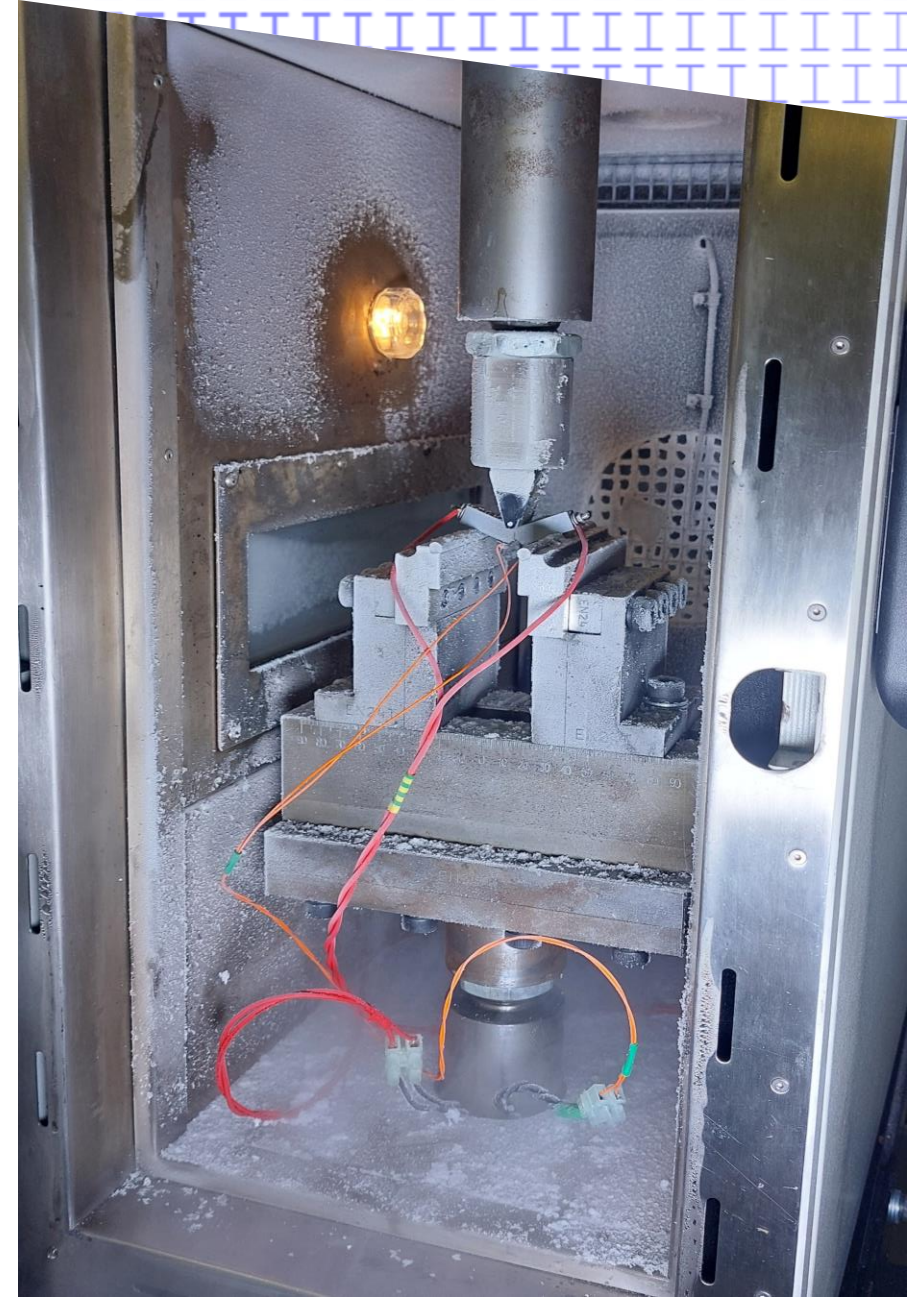
Charpy Samples 10x10x55mm, notch and ½ Pre-crack

**Prone to Plastic Collapse**

*“such tests do not comply to valid specimen sizes but can be used as part of research and quality control”* ASTM-E1820-23b

High uncertainty ∴ Large safety factors

Excessive conservatism



# Standard 'Rapid' Fracture Methods

Charpy (Pendulum) vs. VHS INSTRON (Servo-hydraulic)

Readily Available

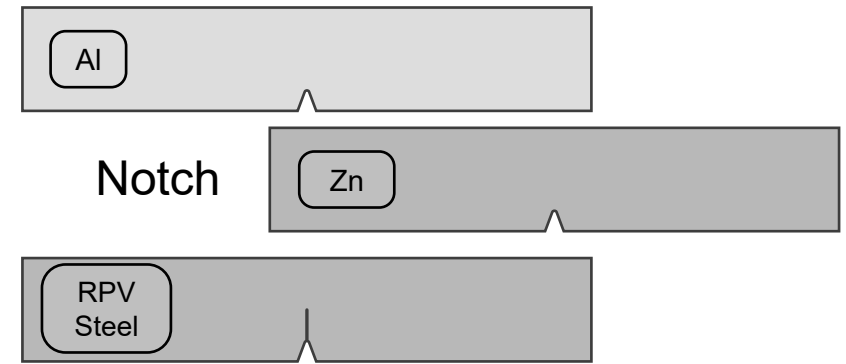
Little Discussion

Fixed Energy Input

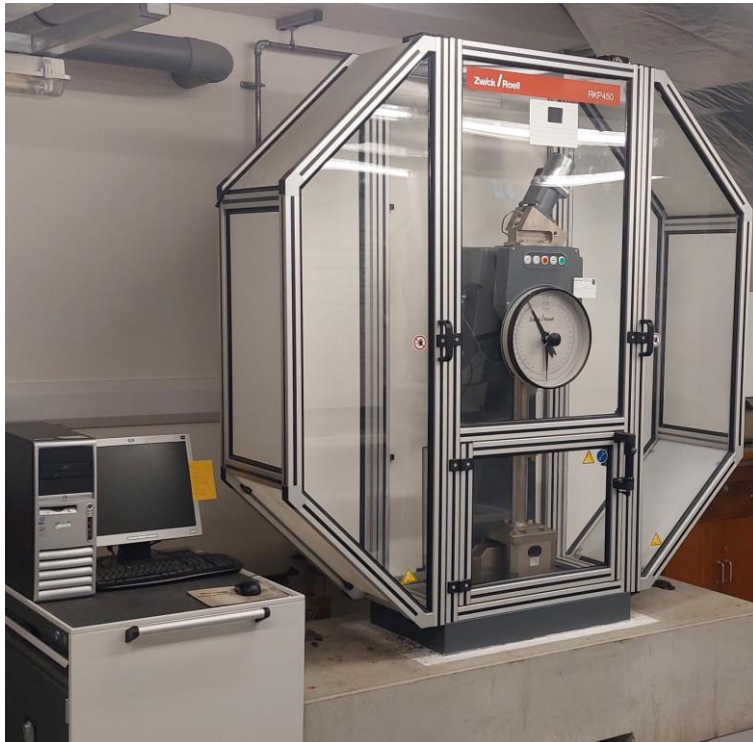
Active Energy Input

Loose Speed during Test

Maintain Speed



Pre-crack

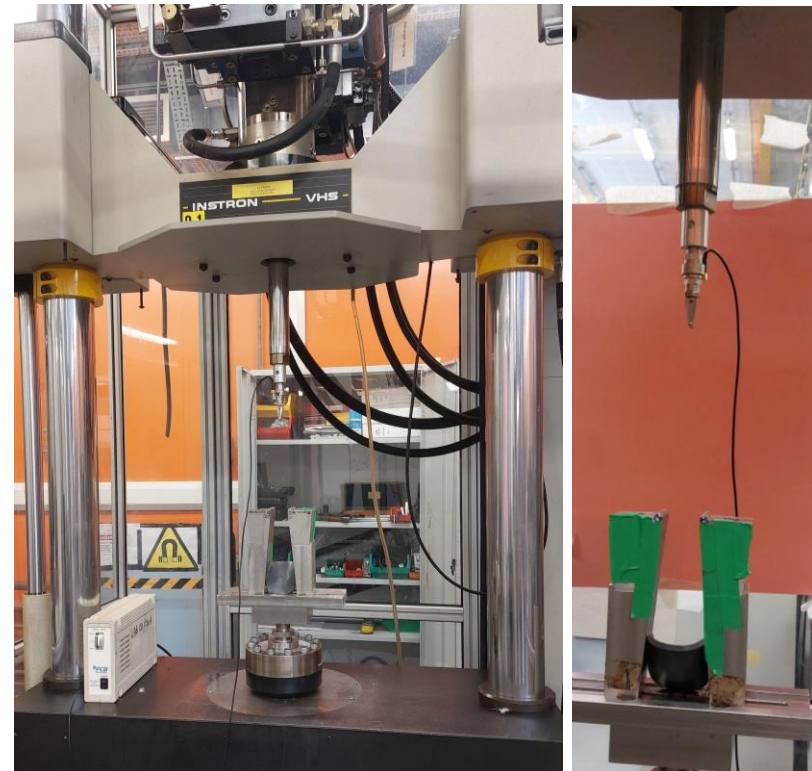


Instrumented Charpy

5.24 m/s  
~310 strain/s

Fixed 450J input

Active Energy input



VHS INSTRON

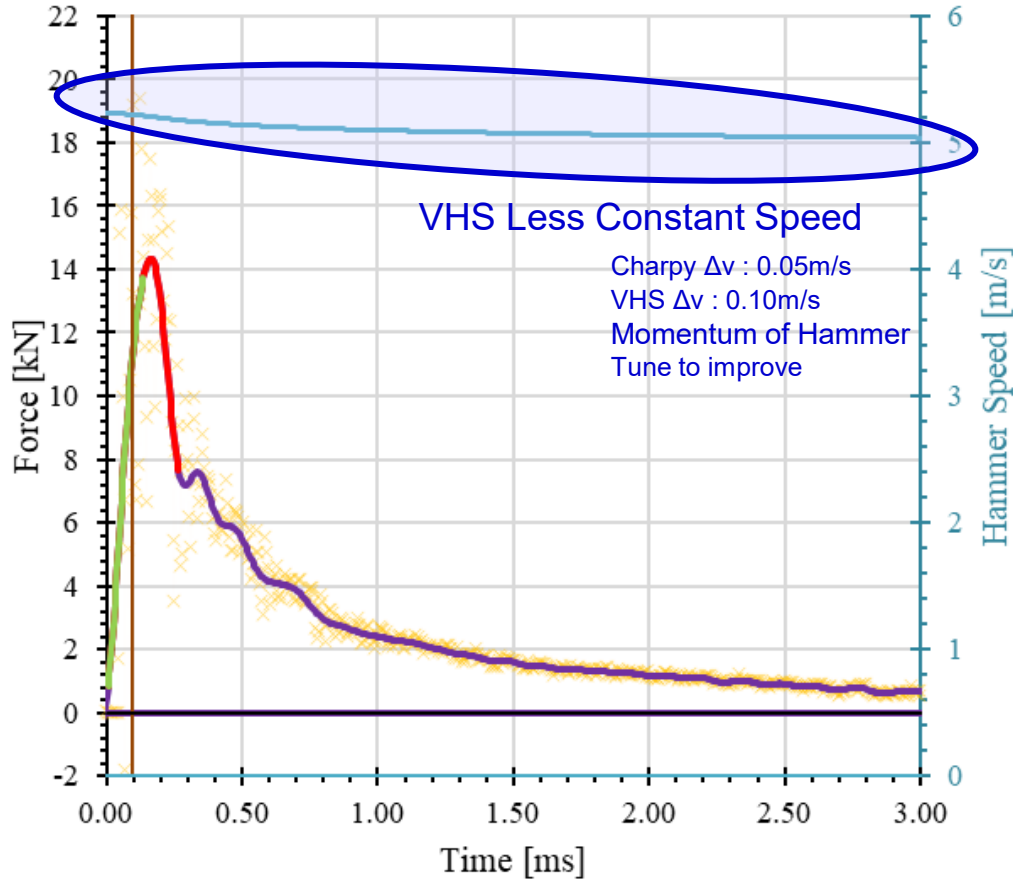
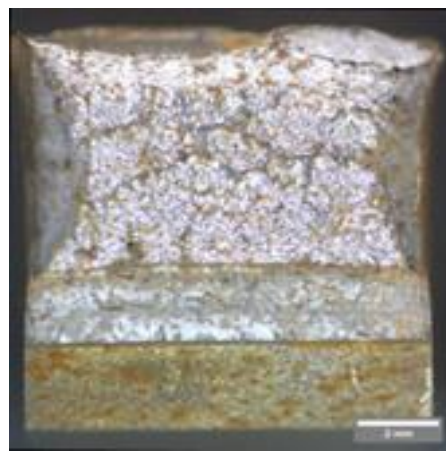
Does speed control alter fracture response

# Results

## RPV Steel – Pre-Crack

### Charpy

- × Std. Load (Peak 19.4 kN)
- Filtered Load
- Test Range
- Linear Range
- Valid Data: 92.8  $\mu$ s
- Speed 5.23 to 5.18 m/s



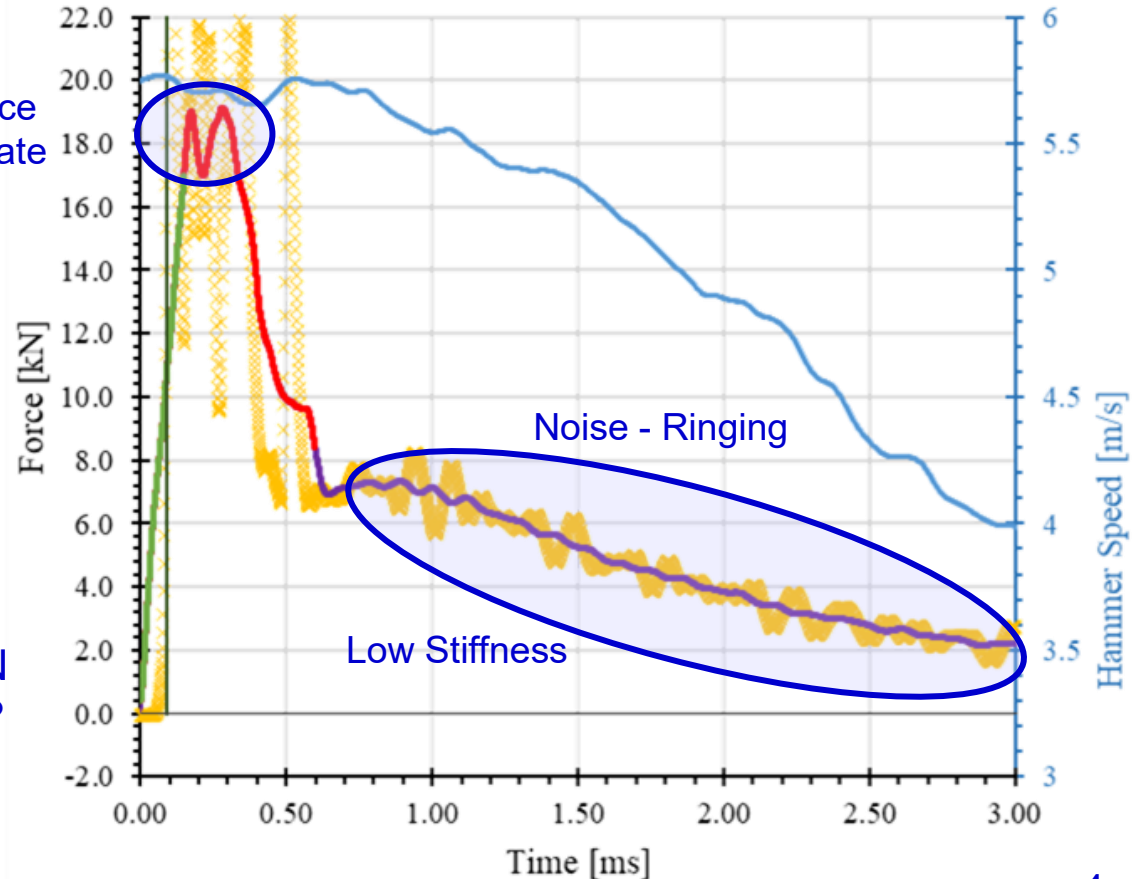
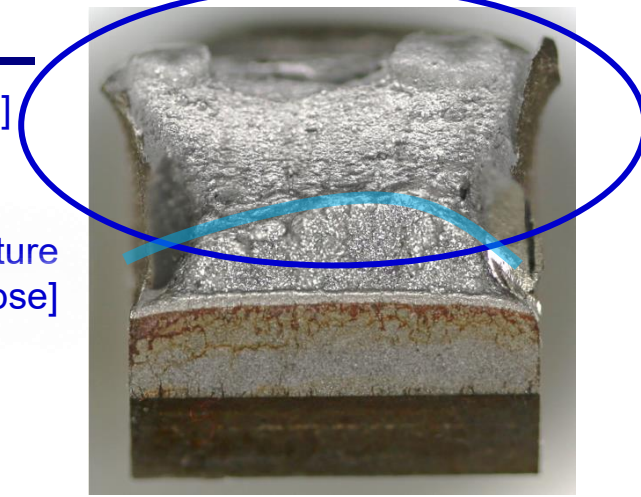
Higher Peak Force  
Higher Sample rate

Similar Profile  
Collapse 7.5 kN  
Charpy Faster?  
Compliance delay?

### VHS

- × Std. Load (Peak 19.4 kN)
- Smoothed Load
- Test Range
- Linear Range
- Valid Data: 88.8  $\mu$ s
- Speed 5.75 to 5.65 m/s

5mm  
More ductile end [Post-collapse]



# Results

## Dynamic Validity

### Use of Static Equations

Assume Inertia effects are negligible

Nakamura [1986] SEN(B) – Time **93µs**

$$\tau = DS \frac{H}{C_0} \cong 23.8 \frac{H}{C_0}$$

### Standards

minimum time of test ( $t_m$ )

ASTM E39 **1,000µs**

ASTM E1820  $t_m > 2 \cdot \frac{D}{C_0}$  **68µs**

BS **140µs**

### Stress Equilibrium

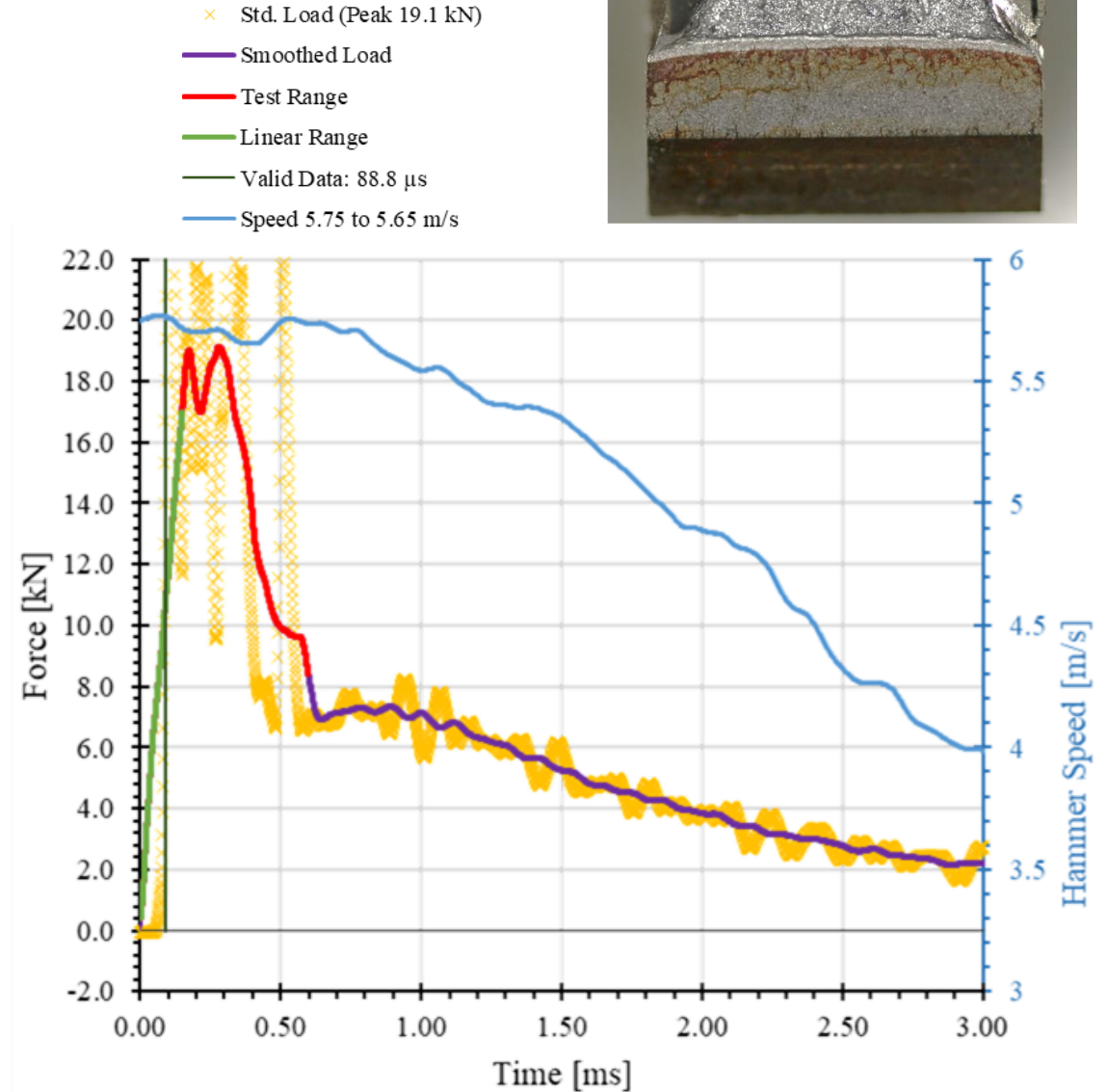
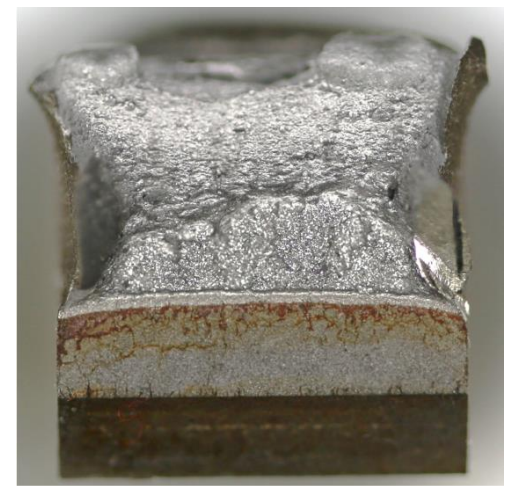
3x reflections

$$3 \cdot \frac{D}{C_0}$$

Charpy **12µs**

VHS **10µs**

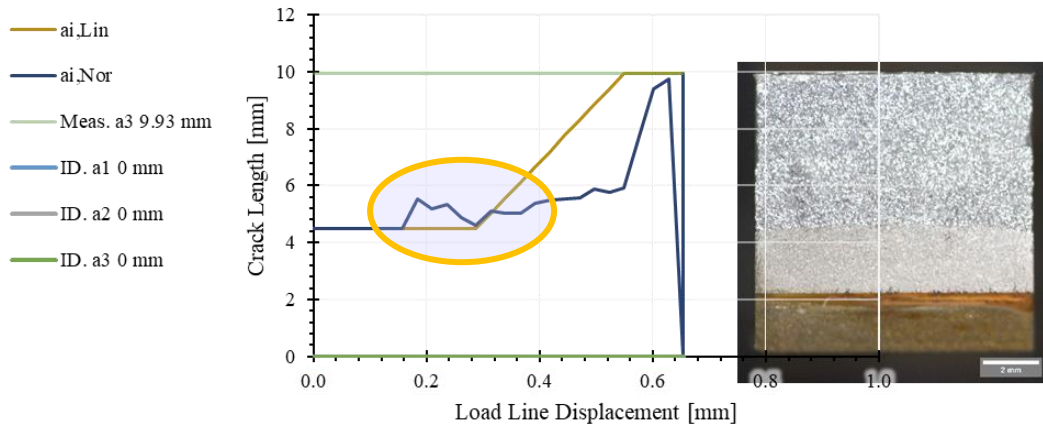
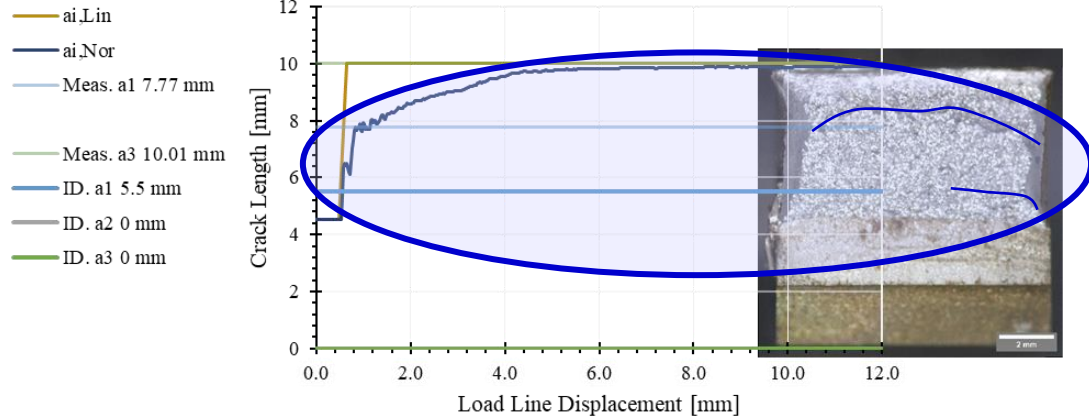
5mm



# Results

## Crack Length Monitoring

### Charpy

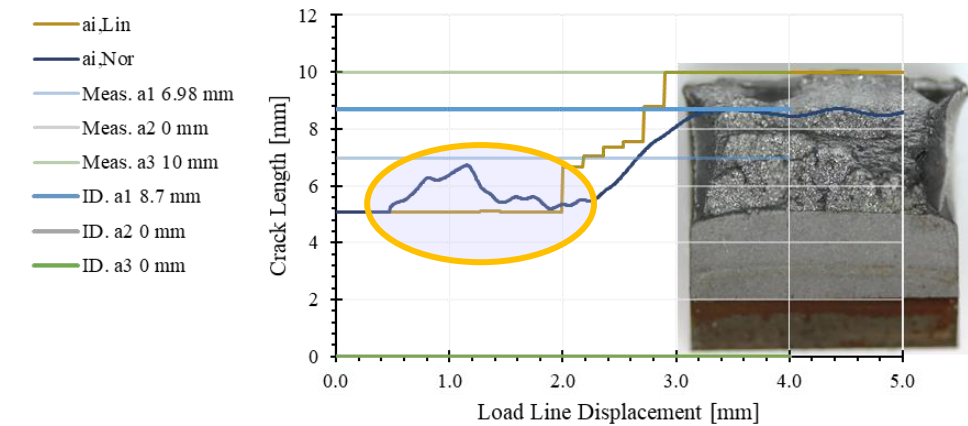
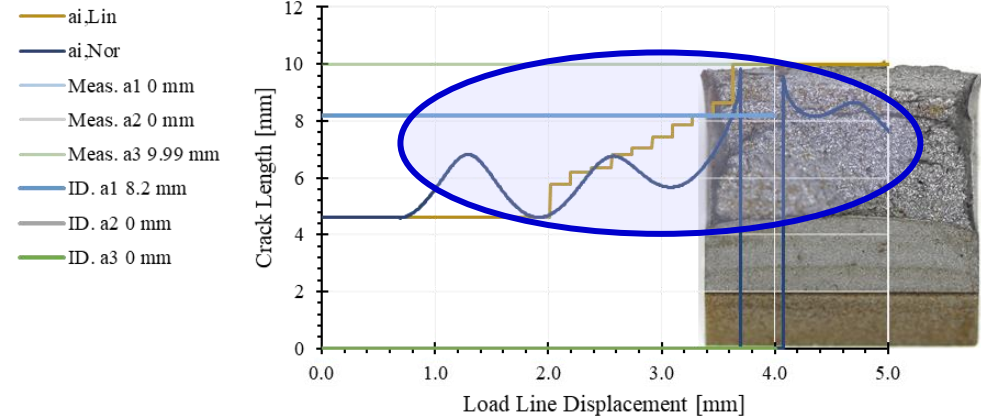


**Linear** – Similar Initiation  
 Norm. suggests earlier.  
 Blunting? Settling on supports?

**Normalisation** – Adjusted fit to normalised load history

**Normalisation** – Fits well  
 Features show from load history

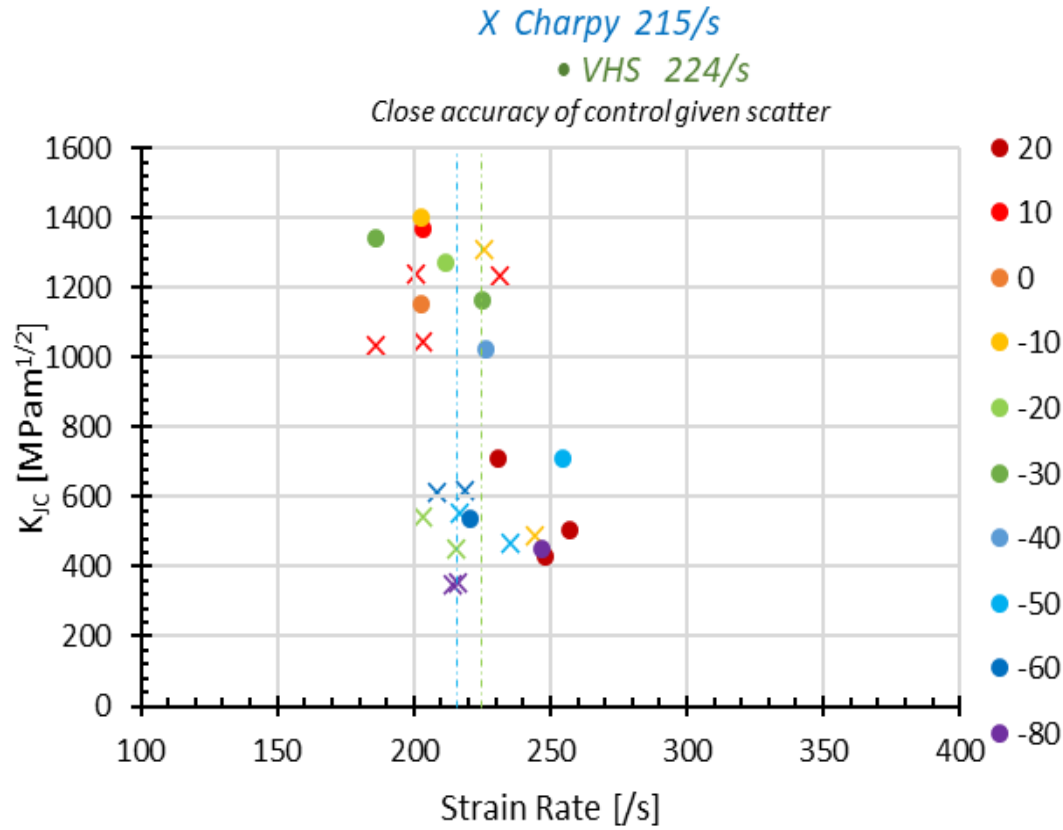
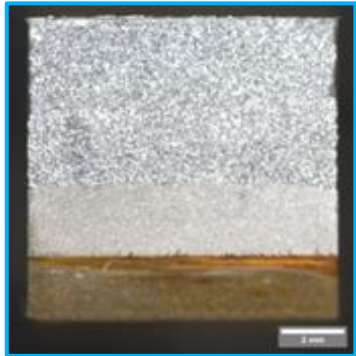
### VHS



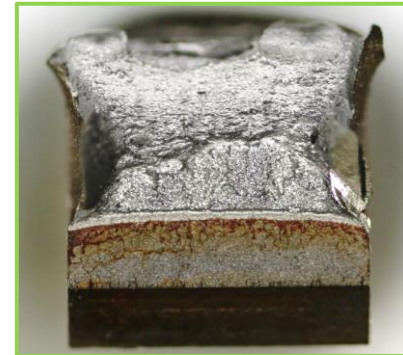
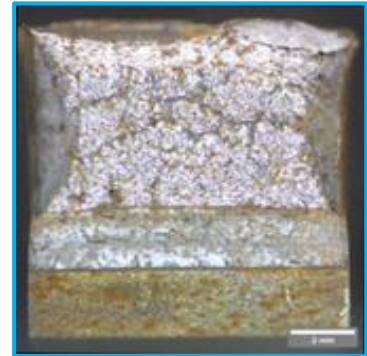
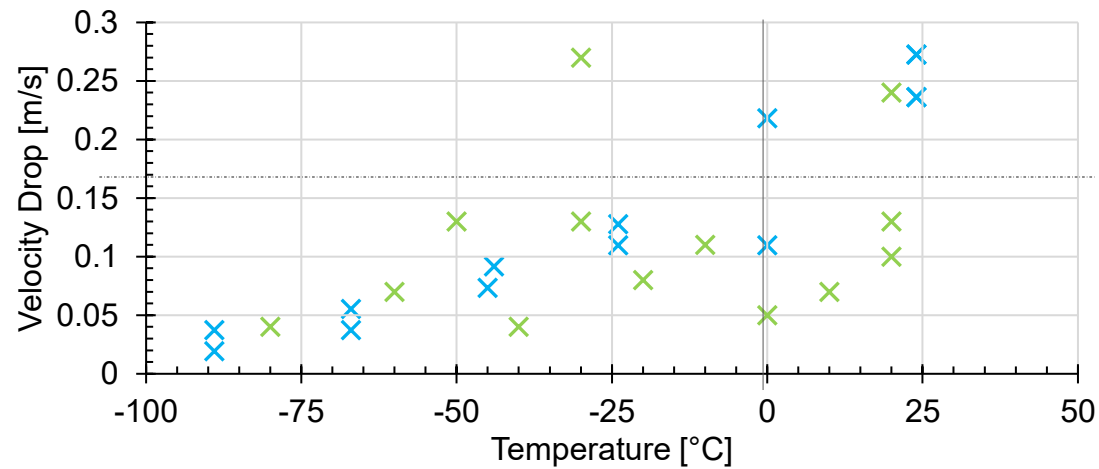
**Linear** – Assume crack growth from Max load to end of test  
 Generally seen as conservative but acceptable

# Pre-Crack

## The Good



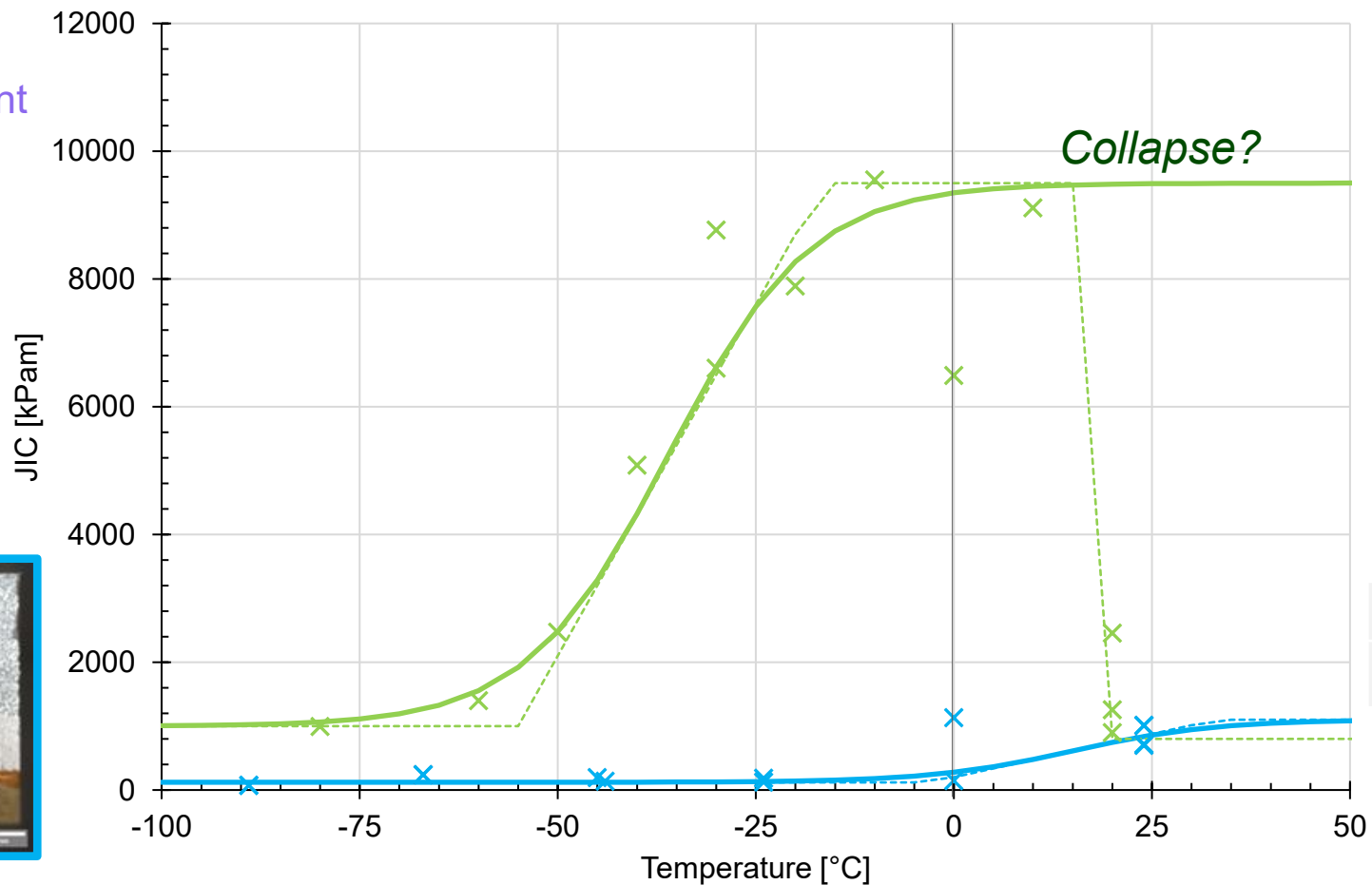
$\Delta v_{ave} = 0.11 \text{ m/s}$   
 $\pm 0.12$   
Good Speed Control  
~ Proportional to energy absorbed



# Pre-Crack

*Charpy more reasonable values.  
Better data analysis needed in VHS to effectively compare.*

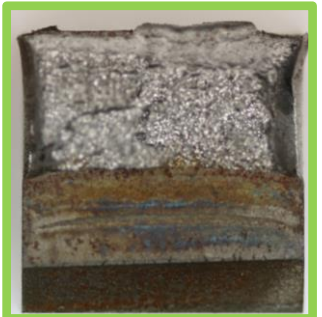
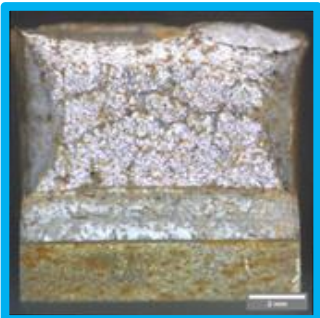
The Bad  
Very Different



- × Charpy
- - - Charpy Linear Trend
- Charpy Hypobolic Fit
- × VHS
- - - VHS Linear Trend
- VHS Hypobolic Fit

BDTT	-36	15 °C
~T <sub>0</sub>	-135	-65 °C

Charpy Results compare well with previous work

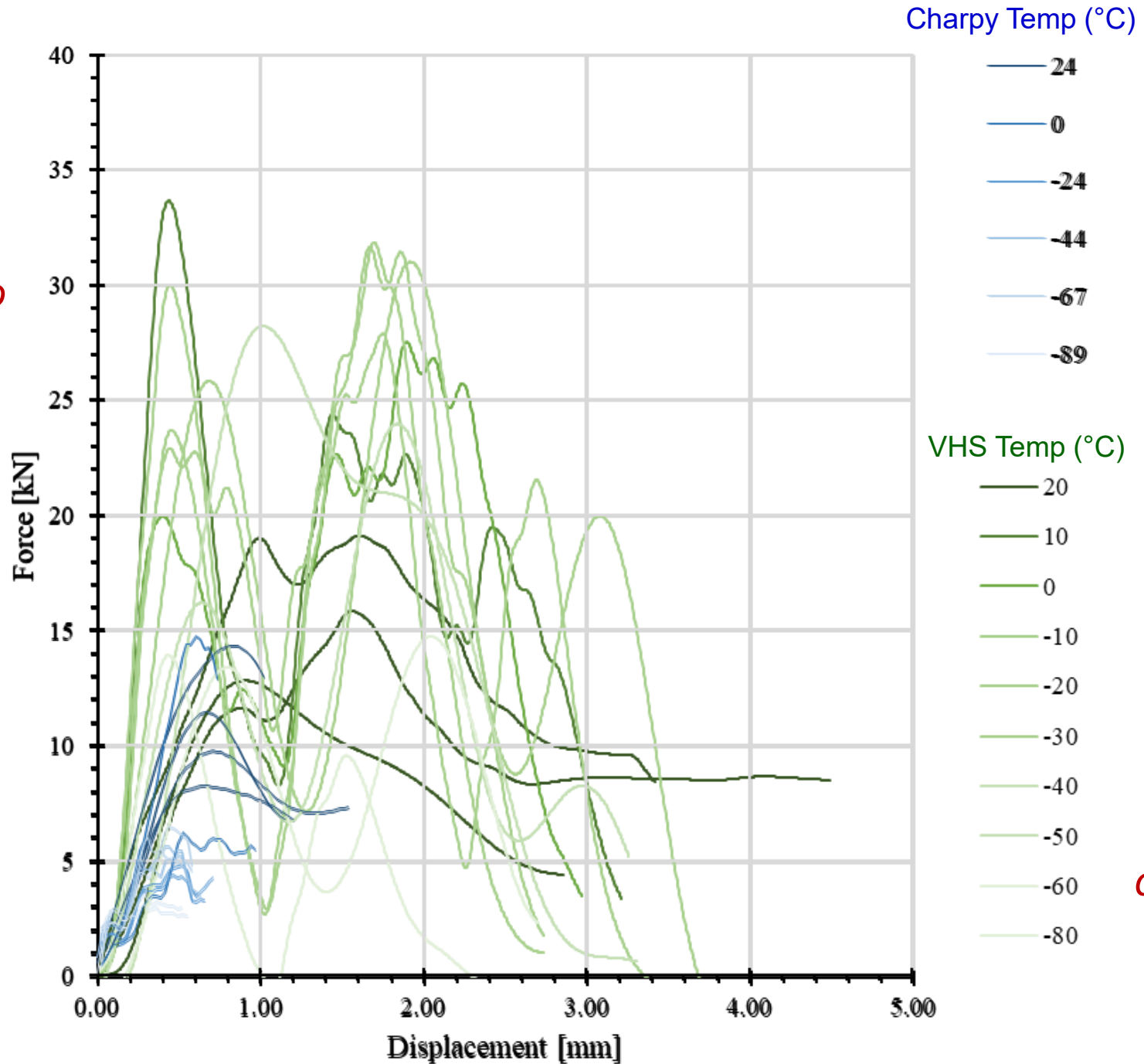




# Pre-Crack

The Ugly

*Impact ringing adding to initial load – artificially raising peak load*



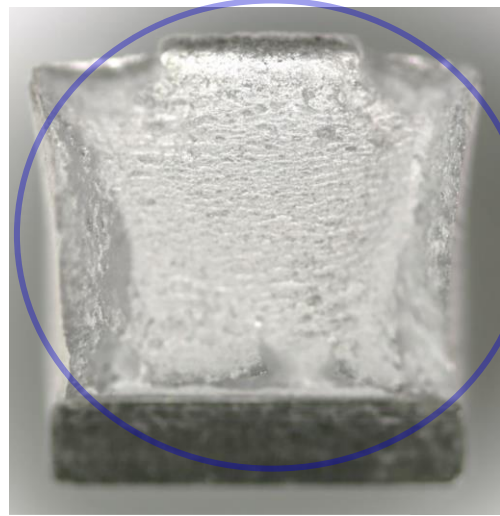
*Ringings makes end of fracture difficult to identify*

# Results

Aluminium – Ductile

## Charpy

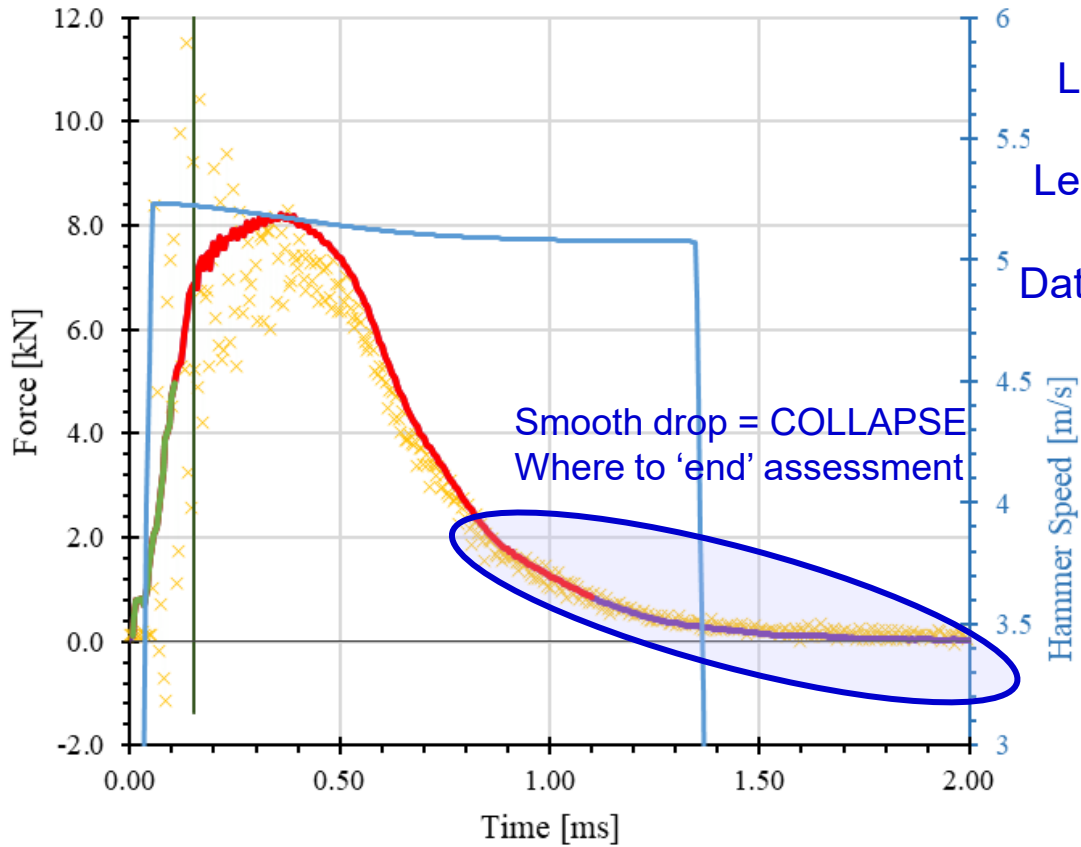
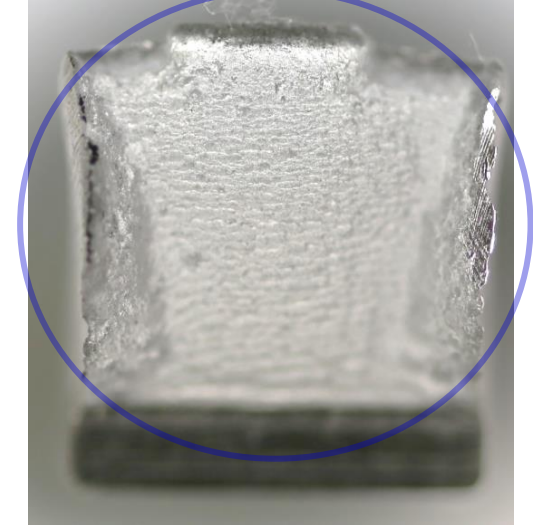
- × Std. Load (Peak 8.2 kN)
- Smoothed Load
- Test Range
- Linear Range
- Valid Data: 150.7  $\mu$ s
- Speed 5.23 to 5.08 m/s



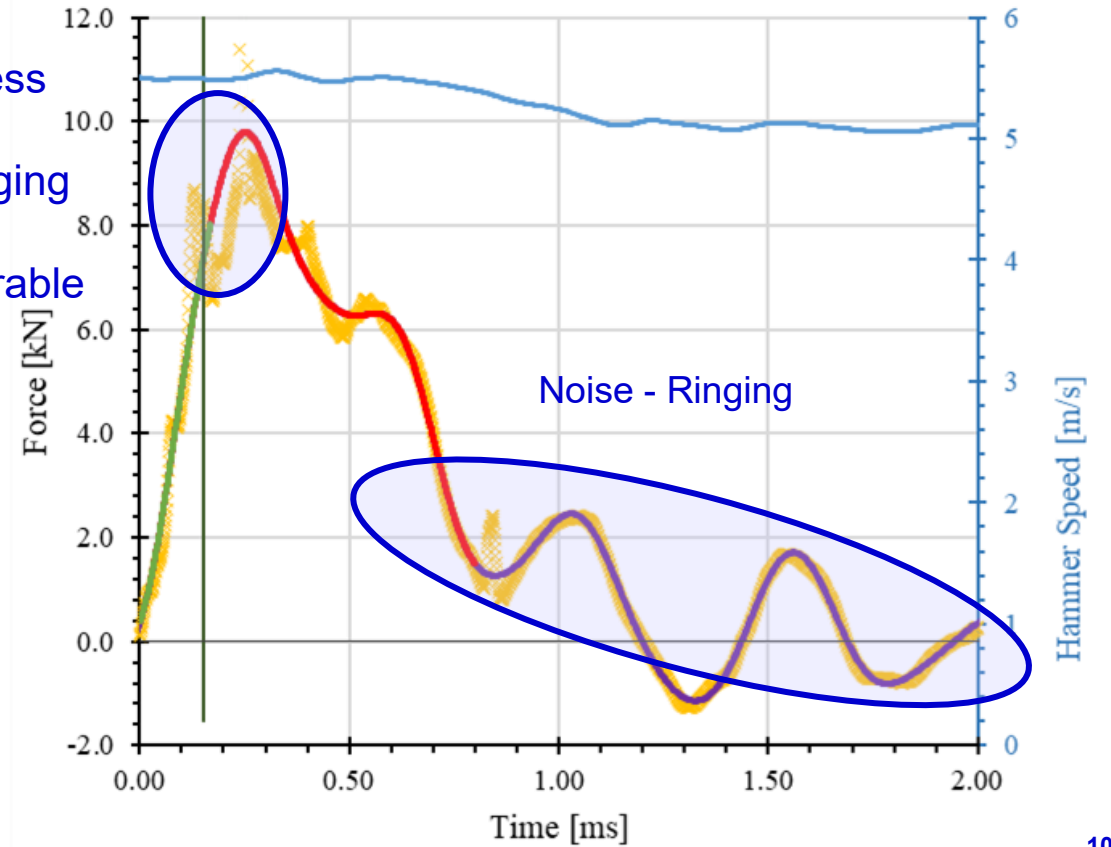
## VHS

Same Feature  
[Collapse]

- × Std. Load (Peak 9.8 kN)
- Smoothed Load
- Test Range
- Linear Range
- Valid Data: 151  $\mu$ s
- Speed 5.56 to 5.4 m/s



Lower Stiffness  
Less initial ringing  
Data is comparable

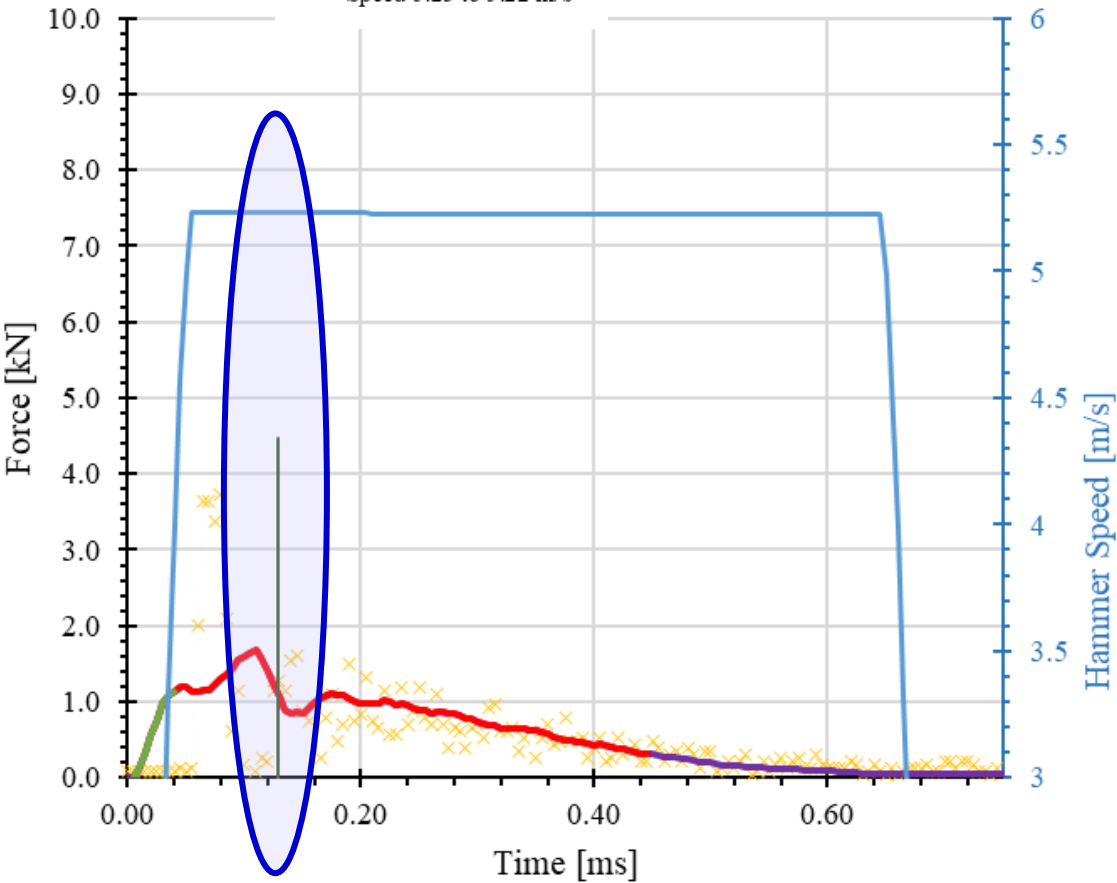


# Results

Zinc – Very Brittle

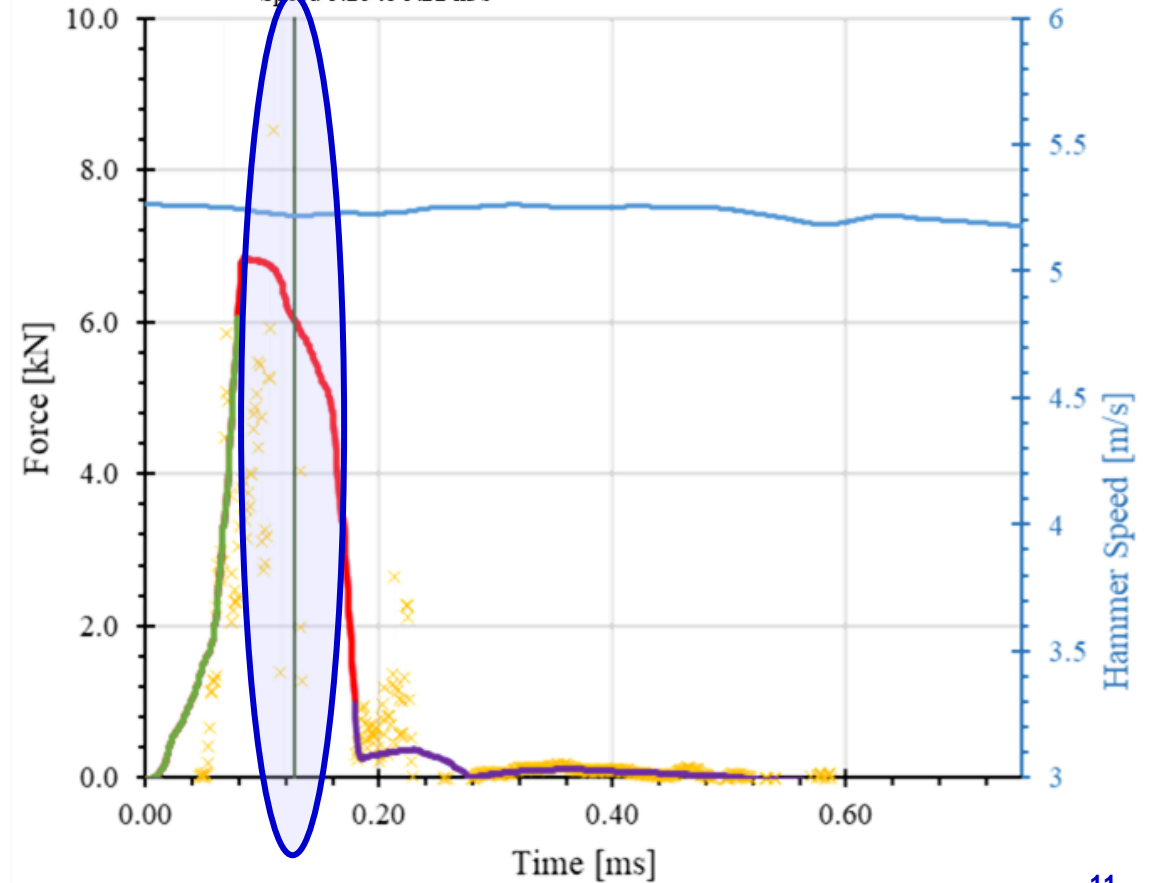
## Charpy

- × Std. Load (Peak 1.7 kN)
- Smoothed Load
- Test Range
- Linear Range
- Valid Data: 128.9  $\mu$ s
- Speed 5.23 to 5.22 m/s



## VHS

- × Std. Load (Peak 6.8 kN)
- Filtered Load
- Test Range
- Linear Range
- Valid Data: 127.1  $\mu$ s
- Speed 5.26 to 5.22 m/s



5mm

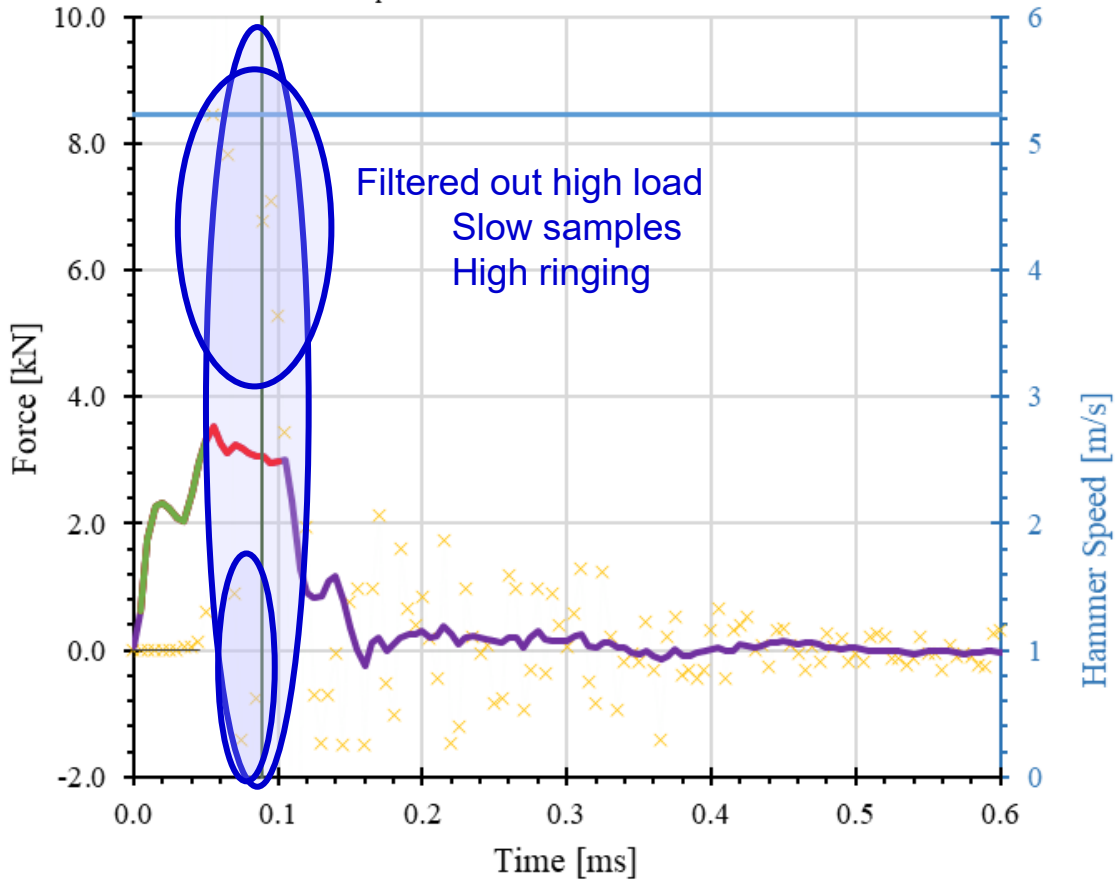
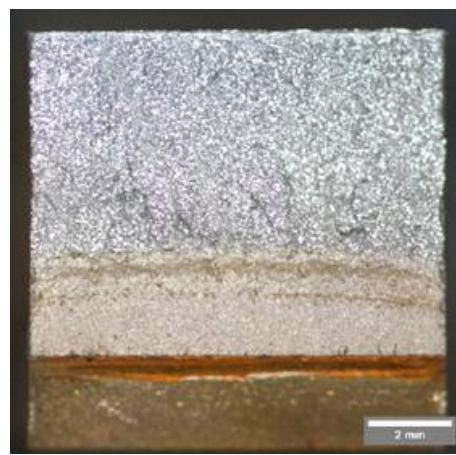


# Results

Low Temp Steel – Very Brittle

## Charpy

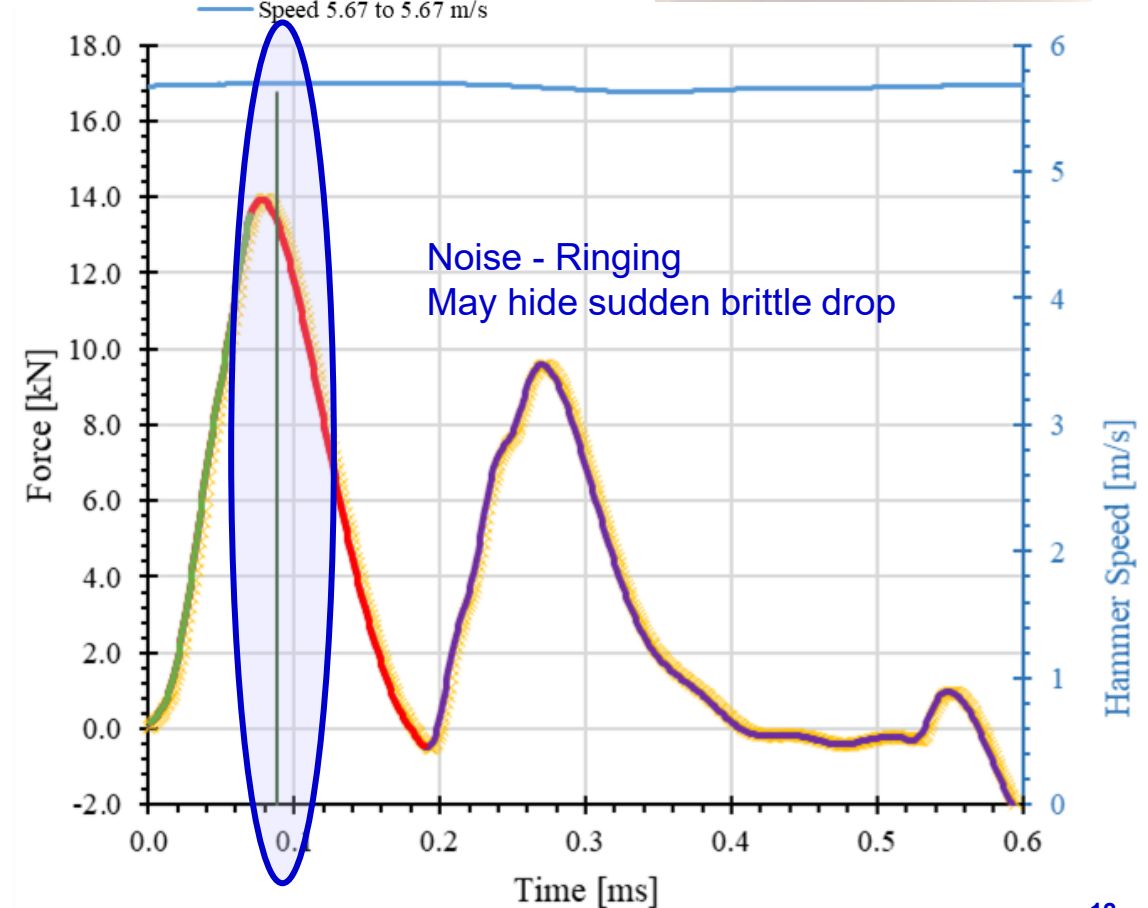
- × Std. Load (Peak 3.5 kN)
- Smoothed Load
- Test Range
- Linear Range
- Valid Data: 88.8  $\mu$ s
- Speed 5.23 to 5.22 m/s



## VHS

- × Std. Load (Peak 13.9 kN)
- Smoothed Load
- Test Range
- Linear Range
- Valid Data: 88.5  $\mu$ s
- Speed 5.67 to 5.67 m/s

5mm



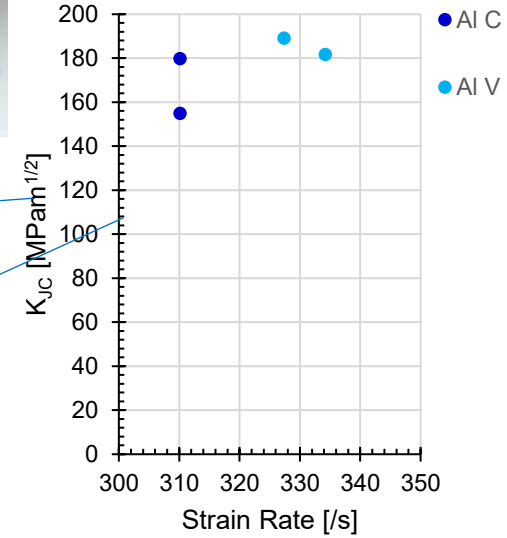
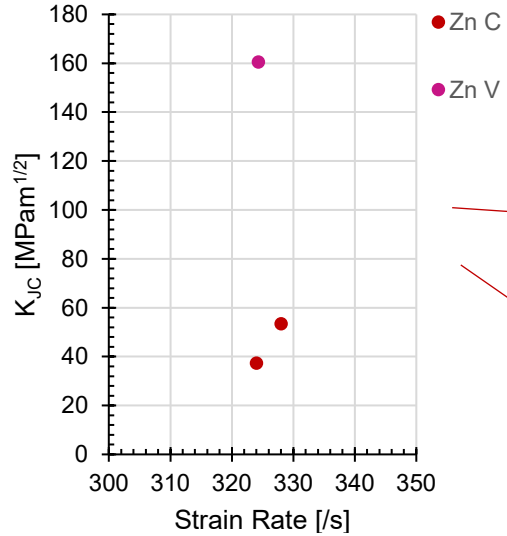
**Brittle Snaps too fast  
Dynamically Invalid**



# Zinc & Aluminium

Brittle vs. Ductile  
Charpy vs. VHS

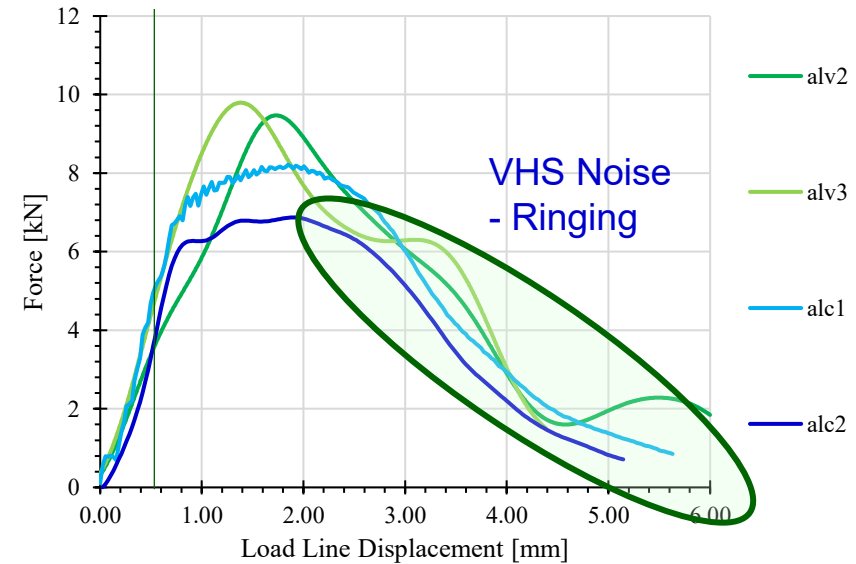
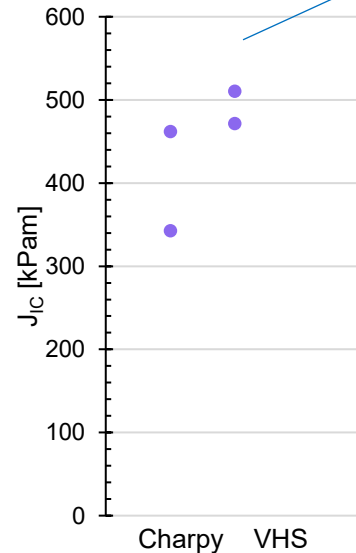
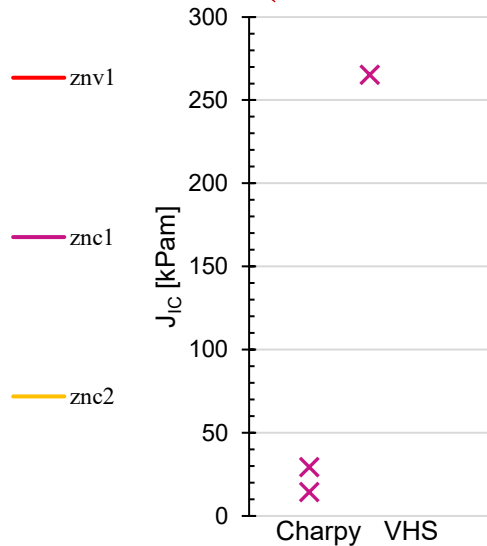
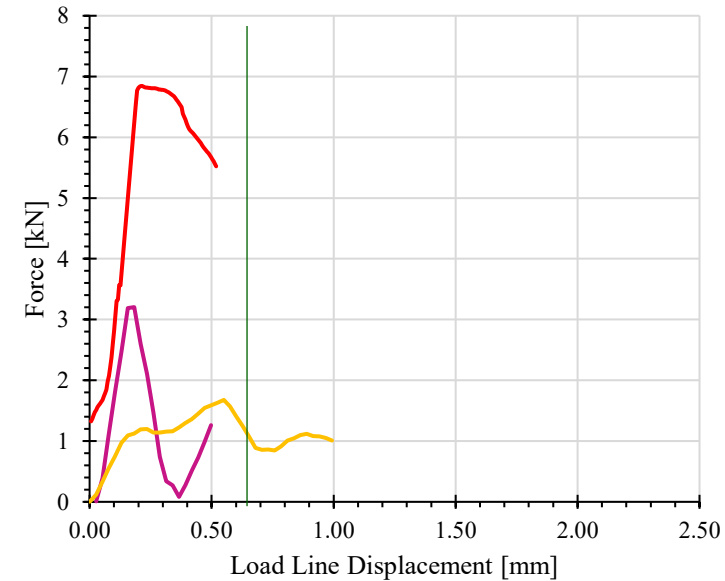
Ave $\dot{\epsilon}_0$ :	327.8	/s		
Ave				
$\Delta v$ :	0.08	m/s	$\pm 0.25$	



*Similar strain rate on both machines*

**Big Difference in Brittle  
CHARPY Slow Sample rate  
VHS Initial Shock Ramp-up**

**Similar in Ductile  
More time to sample and  
less effect by uncertain  
rise time**



# Conclusion

## Both Function for Ductile

Brittle tests are all Dynamically invalid for Fracture

Both methods require **low stiffness ductile metal** to be effective. When too stiff...

CHARPY loses highest loads from slow sampling

VHS overloads from shock ringing

Smooth collapse makes end of test difficult to identify

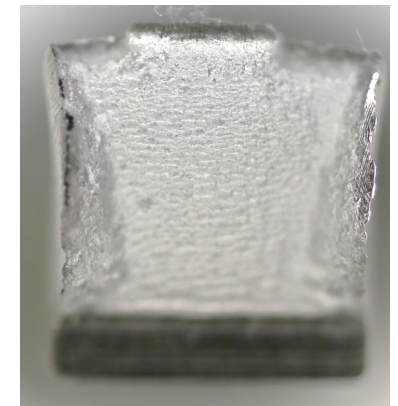
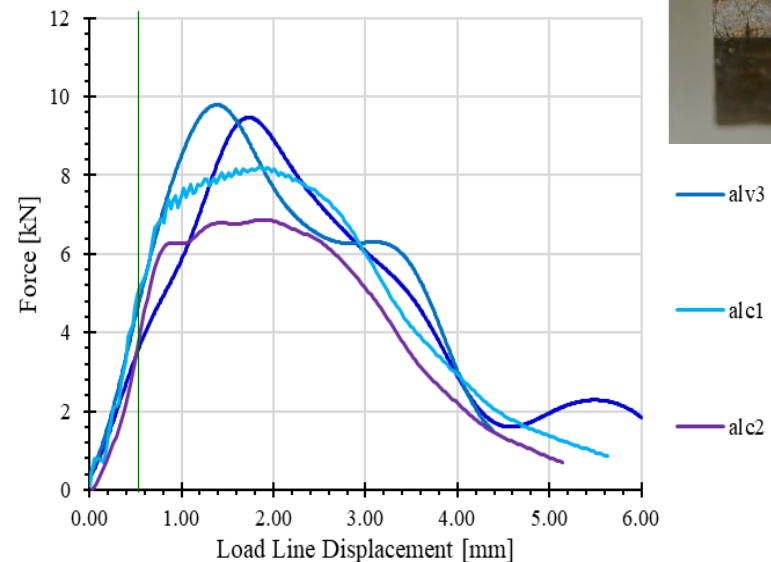
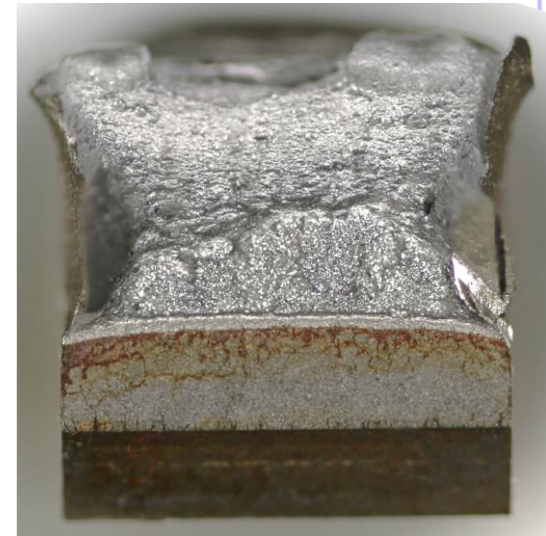
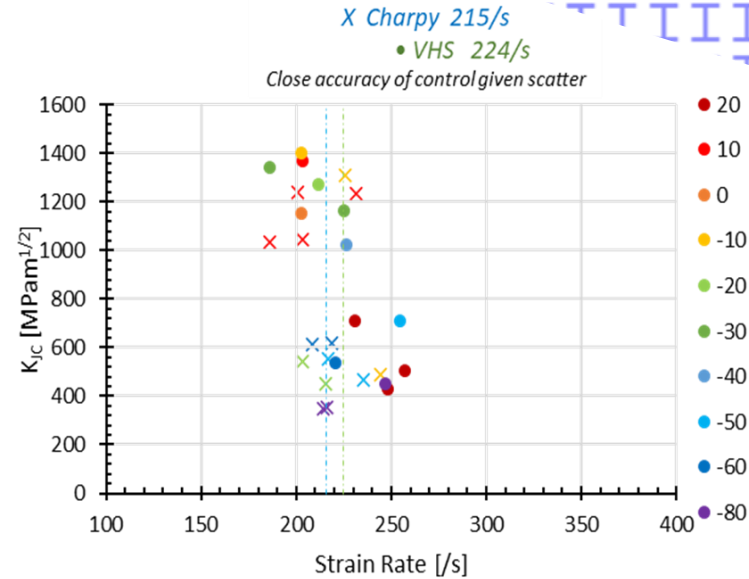
Good strain rate control

Charpy has advantage of momentum and stiffness

VHS system can be improved and tuned

Crack growth monitoring (norm. & linear) compare well

Similar profiles with equal benefits and draw-backs



# Conclusion

Effect of Fixed energy Input vs. Speed control testing

No observable difference

Rig rigidity and data acquisition lead to larger difference.

Next – Improve Procedures

VHS – More ridged system to reduce ringing

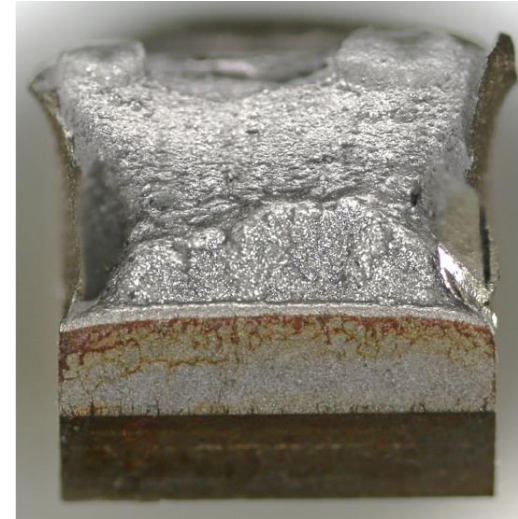
Crack growth by Potential Drop

Next - Interrupted testing

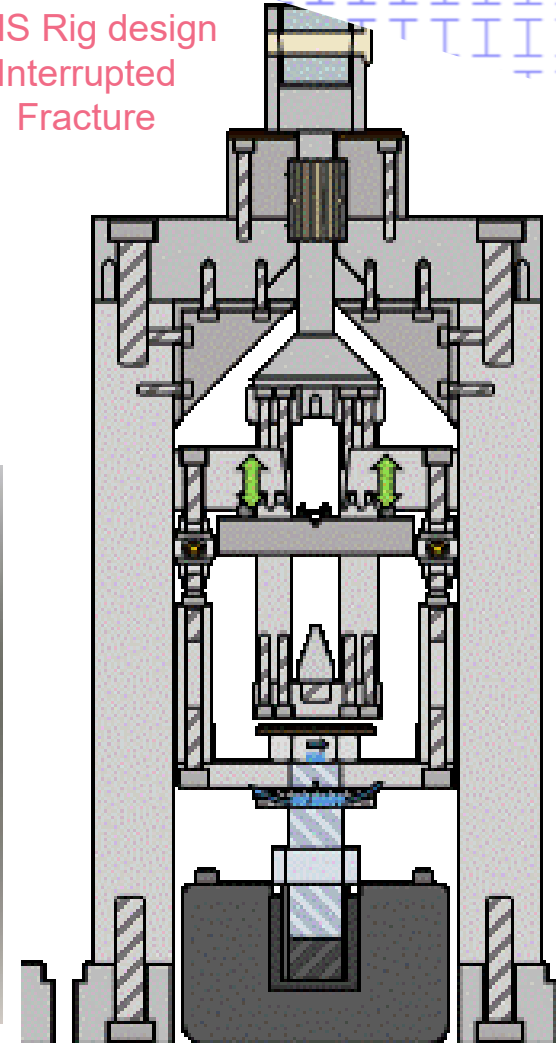
Chapry ‘low-blow’

VHS – Novel test rig

Project sponsorship acknowledged to the Nuclear Energy Futures CDT (EPSRC ref. EP/S023844/1) and Nuclear Security Technologies



VHS Rig design  
Interrupted  
Fracture



**IMPERIAL**

**Thank You**