A long period grating based directional flow sensor

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ABSTRACT

A chirped long period grating (LPG) is used as a directional flow sensor by monitoring the change in the transmission spectrum upon immersion in an oil of refractive index higher than that of the fibre cladding. The change in profile of an attenuation band is shown to depend on the direction of immersion, indicating the possibility of using such devices in applications such as resin flow sensing in the manufacture of fibre reinforced plastic composite structures.

Keywords: Chirped long period grating, directional flow sensor

INTRODUCTION

The sensitivity of long period gratings (LPGs) to external perturbation has been reported previously and has been exploited for sensing parameters such as temperature, strain and refractive index¹. The refractive index response of an LPG has been exploited to has been used to demonstrate a liquid level sensor². Khaliq *et al* demonstrated the use of a uniform period LPG as a liquid level sensor by monitoring the change in the transmission spectrum when the LPG was partially immersed in a liquid of refractive index lower than that of the cladding. The LPG attenuation bands were observed to split as a different phase matched resonant condition existed for the section of the fibre immersed in the liquid as compared to the section in air. The relative transmission depth for the split attenuation bands was shown to be a function of the proportion of the LPG immersed in the liquid. Here the concept of the LPG based liquid level sensor is developed further by demonstrating a sensor which also provides information on the direction of immersion, by exploiting the properties of a chirped LPG.

A chirped long period grating has a periodicity that varies as a function of position along the axial length of the LPG, which results in a broadening of the bands and a decrease in attenuation, compared with that of a uniform period LPG of the same length³. The spectrum of a chirped LPG may be explained by considering it as a composite of separate LPGs of differing but closely matched periodicity. A representation of this is shown in figure 1. The separate period LPGs, $\Lambda_1, \Lambda_2, \Lambda_3$, all form attenuation bands of differing central wavelengths. The composite band resulting from the chirped LPG is shown in figure 1 (a) and illustrates the broadening effect on the band. The reduction in attenuation is a result of the dependence of the depth of the attenuation band on the length of the LPG⁴.





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19th International Conference on Optical Fibre Sensors, edited by David Sampson, Stephen Collins, Kyunghwan Oh, Ryozo Yamauchi, Proc. of SPIE Vol. 7004, 70045P, (2008) 0277-786X/08/\$18 doi: 10.1117/12.786558 If a section of the LPG is covered, e.g. Λ_1 of figure 1 (b), with an oil of refractive index higher than that of the cladding, the composite band period experiences a slight decrease in attenuation and a positive shift of the lower wavelength edge (because, when exposed to a refractive index higher than that of the cladding, the LPG has low sensitivity to the surrounding refractive index, the wavelength shift may be neglected). This may be explained by the coupling to leaky cladding modes⁵, which results in a decrease in the extinction ratio of the attenuation band corresponding to section Λ_1 . The expected result for covering section Λ_3 is shown in figure 1 (c). This demonstrates the potential for the use of such devices as directional flow sensors. The discussion is concerned with the refractive indices higher than that of the cladding, as this is representative of the refractive index of resin systems used for structural components.

EXPERIMENT

An LPG of length 40 mm was fabricated in hydrogen loaded single mode fibre of cut of wavelength 650nm (Fibercore SM750). The fibre was placed behind a Vernier calliper with a fixed slit width of 200µm that was illuminated by a UV laser beam at a wavelength of 266nm, provided by a frequency quadrupled Nd:YAG laser. A computer controlled translation stage was used to move the fibre behind the slit to create a linearly chirped period, from 395µm to 405µm. The LPG was subsequently annealed at 100°C for 24 hours to ensure that the hydrogen had diffused out and that the spectrum was stable⁶.



Figure 2. Transmission spectrum of a chirped LPG of length 40mm and linearly chirped period 395μm - 405μm, fabricated in Fibercore SM750. Band 6 is highlighted and shown compared with a band in the same spectral location (b) of an LPG of uniform period 400μm (dashed).



Figure 3. Experimental setup for chirped long period grating flow sensor (a) orientation of the chirped LPG for the flow sensing experiments (b).

The transmission spectrum of the chirped LPG, shown in figure 2, was monitored by coupling the output from a tungsten-halogen white light source into the fibre and coupling the transmitted light to a CCD spectrometer (OceanOptics S2000). The experimental setup is shown in figure 3 (a). A feed syringe allowed a test syringe, graduated

with 0.01ml marks, to be gradually filled with a Cargille refractive index oil of 1.56 ± 0.0002 . The fibre was held in place with rubber grommets to prevent the fibre from bending, which is known to distort the transmission spectrum⁸. The rubber grommets also provided a seal to ensure that there was no loss of liquid. The needle from the feed syringe was placed close to the wall of the test syringe to ensure there was no contact during feeds between oil and LPG before the oil reached the bottom of the test syringe. The experiment was repeated with the orientation of the chirp reversed to simulate the effect of the liquid flowing over the LPG from the opposite direction, as illustrated in figure 3 (b).

RESULTS

As the test syringe was filled with the oil, the transmission spectrum of the LPG was recorded for each 2.7mm increment in the depth of the oil. Figure 4 shows the response of band 6 to the gradual covering of the LPG by the oil for the different test orientations. With the LPG oriented with decreasing period relative to the oil, experiment 1, (figure 4(a)), an apparent negative wavelength shift is measured. This is caused by a reduction of the extinction at longer wavelengths due to the cladding/oil structure of the covered section no longer supporting propagating cladding modes. The result for experiment 2 is shown in figure 4(b).



Figure 4. Change in shape of band 6 for gradual immersion in 1.56 Cargille index oil. Experiment 1 (a) and experiment 2 (b). 0% is no coverage, 50% half and 100% total coverage.

Figures 5 (a) and (b) show the wavelength shift of the central wavelength of attenuation band 6 and the minimum transmission value at that wavelength for the different test orientations. The band minimum was calculated by fitting a 6^{th} order polynomial to the spectra. For both experiments, an apparent wavelength shift of ~1nm is observed, with directional information given by the direction of shift. In experiment 1 (figure 5 (a)) the wavelength shift is negative while experiment 2, (figure 5 (a)) the wavelength shift is positive. The transmission change is similar (10%) for both orientations.



Figure 5. Wavelength shift (\blacklozenge) of band 6 and minimum transmission value (\Box) against LPG coverage with Cargille index oil (1.56) for LPG arranged with decreasing period (a) and increasing period (b). Grey lines are shown only as a visual aid.

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DISCUSSION

The results presented in figures 4 and 5 show the wavelength shift and change in transmission of band 6 for the gradual immersion of the grating in the Cargille oil. The apparent wavelength shift of the band is shown to be dependant on the direction of flow of the oil surrounding the fibre. The change in the extinction of the band is shown to have no directional dependency. When the oil covers 75% of the LPG the results for both orientations of the LPG indicate a change in direction for wavelength shift as the coupling to leaky cladding modes begins to dominate. When the LPG is fully immersed in the high index oil the cladding/oil structure no longer supports propagating cladding modes but leaky cladding modes exist due to Fresnel reflections from the cladding oil interface. Coupling to such modes is weak when the index difference between the cladding and oil is small and results in attenuation bands with a poor extinction ratio. This effect and the broad bands exhibited by chirped LPGs may contribute to errors in determining the wavelength of the band minimum.

5. CONCLUSION

A directional flow sensor using a chirped LPG is demonstrated with an oil of refractive index higher than that of the silica fibre,. An attenuation band is shown to have directional dependence on immersion in the oil leading to the possibility of a flow sensor with directional sensing capability. As epoxy resin used in the fabrication of composite structural components typically have a refractive index in the range 1.5 - 1.6, the results indicate the potential for the use of chirped LPGs as directional flow sensors to monitor the infusion of resins into reinforcing fibre layups.

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