

The effect of nanoclay on dust generation during drilling of PA6 nanocomposites

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ABSTRACT

During the past decade, polymer nanocomposites have emerged as a novel and rapidly developing class of materials and attracted considerable investment in research and development worldwide. However, there is currently a lack of information available in the literature on the nano and ultrafine particle emission rates from these materials. In this study, influence of nanoclay on mechanical drilling of PA6 composites, in terms of dust generation has been reported. With the help of real-time characterization, submicrometer-sized particles (5.6-512 nm) size distribution and number concentration emitted from polyamide 6/nanoclay composites during mechanical drilling is studied. Total particle concentration for the PA6/nanoclay composites was 20,000 cm⁻³, while unreinforced panel measured a total concentration of approximately 400,000 cm⁻³. While the airborne particle concentration for the PA6/ nanoclay composites was 20 times lower than for the PA6 matrix, the concentration of deposited nanoparticles doubled for the nanocomposite. The results clearly shows that more particles in the size range between 175-350 nm are generated, during drilling of the nanocomposites and this particles deposit in a shorter time. It is likely that the presence of nanoclay in some way retains the formation of high quantity of airborne particles and promotes particle deposition.

KEYWORDS *Nanocomposite, nanoclay, thermal properties, nanoscale dust particles*

INTRODUCTION

Nanoreinforced polymers have focused the attention, because of their potential to exhibit impressive enhancements of material properties compared to the pure polymers. For light weight constructions, among various nanocomposites, much attention has been paid to polymer/layered silicate nanocomposites, because of their enhanced mechanical properties, high thermal stability and high flame retardants [1-7]. Nanoclays account approximately 70% of the total volume of nanomaterials commercially used [8]. In the automotive and packaging sector nanoclays were introduced, mainly due to their low cost and availability. Poly(methyl methacrylate) –epoxy–nanoclay composites [9], polypropylene–nanoclay composites [10], polyvinylidene fluoride–nanoclay nanocomposites [11] and nanoclay modified rigid polyurethane foam [12] exhibit improved properties when compared to their bulk polymer constituents and conventional macro composite counterparts. Numerous studies have reported the improvement of energy absorption of nanoclay/polymer nanocomposites [13-15]. For example, John et al. [16] have shown that the incorporation of 2 and 4 vol. % of nanoclay respectively improves the tensile modulus of cyanate ester syntactic foams by 60 and 80%, respectively.

On the other hand, only little attention has been paid to the behaviour of these materials on the emission of free nanofiller as ultrafine airborne particles during their life time. Shear forces during different mechanical processes such as milling, grinding, turning, boring, and drilling may detach free nanofiller as ultrafine airborne particles. Due to their size, these particles are able to remain airborne for a longer period [17] and are suspected to enter the human cells more easily via respiratory, dermal or oral absorption [18]. The high biological activity can be explained by the large surface-to-volume ratio; hence many types of nanoparticles have shown toxic impact [19-22].

In the current work, airborne particles emitted by nanoclay filled polyamide 6 nanocomposites during mechanical drilling, in a controlled environment, were investigated. The particle number concentration and size distribution were measured continuously in real time using a particle sizer. In addition, the particles emission rates were evaluated, as this information could be useful in assessing the particle exposure to air. Further, deposited particles were collected and investigated utilising a nanoparticle tracking analysis and electron microscopy, for assessing the emission of particles to soil and water.

EXPERIMENTAL

Materials

Polyamide 6 (PA-6) Tarnamid T30, Azoty Tarnów, Poland (melt volume flow rate 25.0 g/10 min (275°C/5.0 kg), due to its respectable mechanical properties, was chosen as an appropriate matrix material. As filler materials 5wt. % of montmorillonite (Laviosa/Dellite 43B) was used, which has been surface-modified with N,N-dimethyl-N-benzyl-N-octadecyl ammonium utilization as filler material. The montmorillonite (MMT) was first dispersed in hot distilled water at a concentration of max. 5 wt % and mixed at 70°C for 2h. Subsequently, a water solution of cationic surfactant (R= alkyl chain C₁₆–C₁₈) was slowly added in an adequate quantity for cation exchange of MMT. The mixture was stirred for 3h to enable complete sodium cation exchange. Then the precipitate was filtered and washed with hot distilled water until no chloride ions were detected in the filtrate after addition of 0.1 mol AgNO₃. Finally, the filtered cake was dried, grounded into fine powder and size-graded with a 50 µm sieve.

Manufacturing of polyamide 6/nanoclay composites panels

Compounding of the composite material was conducted in a twin-screw extruder (ZMK/116/10, ZAMAK - Cable Machinery Plant, Poland). The PA6 and 5 wt. % of organically modified montmorillonite were premixed and batched by the main feeder to the first barrel zone. The extruder was equipped as followed; screw diameter 24mm, length/diameter ratio 32, conventional screw configuration, and 6 barrel zones with two high-shearing zones. This granulate was then used for nanocomposite manufacturing by compression moulding.

The mould temperature was kept at 250°C over the compression time of 5 min. Due to the high dimensions of the panels, cooling of the polymer melt was completed in the mould in order to avoid material warping.

Drilling experiment

Drilling of the nanoreinforced panels was conducted in a controlled environment, with just one small opening for the drill bit (10mm diameter) as shown in Figure 1. This chamber was designed to reduce the possible influence of the drilling engine, as background noises, on the measurement results. Inside the chamber the composite panels were mounted on a fixture. A sampling tray helped collecting the turnings which were produced during drilling. The measurement equipment and the chamber were connected with help of an antistatic silicon tube. An angle drill (Makita BDA351Z 18V LXT Angle Drill) was used for drilling with a maximum speed of 1800 min⁻¹. Before the drilling experiment, the chamber was purged with laboratory air for about 20 min. Each sampling cycle

comprised a 60 min background air monitoring in the chamber, 14min. of active drilling, and a 60 min postdrilling period. The experiment was repeated 3 times for each material composition.

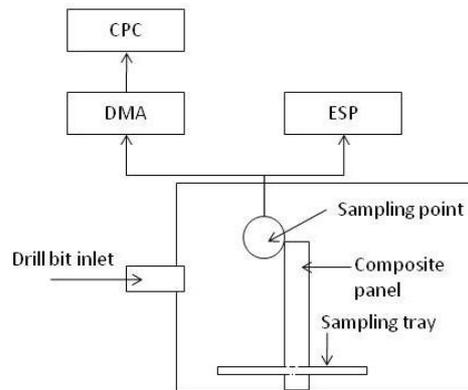


Figure 1 Apparatus and setup for the chamber experiments

Airborne particle size distributions were measured with help of a SMPS+C (Condensation Particle Counter "CPC" 5.403 with Classifier "Vienna"-DMA 5.5-U, Grimm Aerosol, Germany). An Electrostatic Precipitator (Model 5.561 Grimm Aerosol, Germany) was utilized to sample the generated airborne particles. A high voltage (5000V) was applied to the central electrode to attract the charged particles onto a sampling plate. The particles on the sampling plate were then studied in further scanning electron microscope analysis.

Fracture particles were sampled in a dry state and analysed by suspending them in solution. Particle size distribution and quantity were measured by nanoparticle tracking analysis (NTA) provided by the Nanosight equipment (Model LM20, NanoSight Ltd.). A defined mass of fracture particles (0.30g) were suspended in 20 ml of deionised water, this solution was then introduced to the Nanosight equipment using a disposable syringe. For the TEM images, 30mg of fracture particles were suspended in 1ml. After sonification, 0.5ml of this suspension was used for TEM study.

Material Characterisation

The morphology of the nanocomposites was investigated by using a FEI XL30 field emission scanning electron microscope (SEM). The operating voltage was in the range of 10–20 kV and the specimens were gold sputtered to minimize charging of the sample.

Crystalline structure of the manufactured nanocomposites was studied with help of powder X-ray diffraction (XRD). XRD studies were performed between 3° and 60° scattering angle, using a Philips X-Pert diffractometer, with graphite monochromator placed in the front of detector - $\lambda_{Cu} = 1.5418 \text{ \AA}$.

RESULTS AND DISCUSSION

Morphology of nanocomposite panels

Microscopical investigation of the nanoadditive panels did not show microscopic agglomerates of filler as shown in Figure 2a. The PA6/ nanoclay composites showed formation of a net of inclusions (brighter areas) nanometric dimensions (Figure 2a). The various shapes of inclusions (both anisometric and isometric) reflect limited orientation of nanoparticles in the core region of the moulded sample and an anisotropic structure. The observations of structure and morphology of PA6/ nanoclay composites by SEM technique enabled to confirm the uniform distribution of nanoparticles in polymer matrix. The morphology of the PA6 panels has shown dendrite structures in some areas. One reason for this dendritic growth was caused from growth instabilities that occurred when the growth rate was limited by the rate of diffusion of solute atoms to the interface [23].

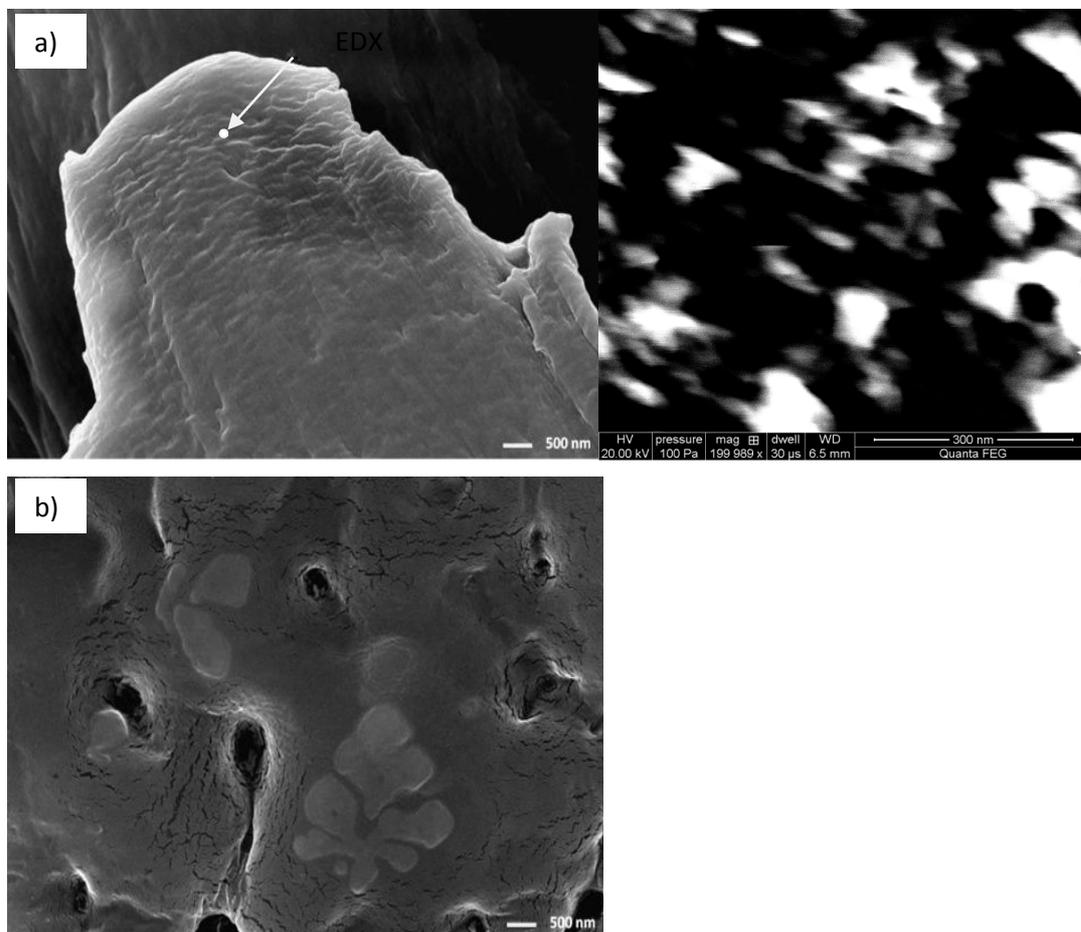


Figure 2 SEM micrographs of bulk a) nano reinforced composites and b) virgin material

WAXD diffractogram of the neat material reflected a strong diffraction peak with a maximum at 21.5° , which corresponded to the γ crystalline phase, and small peak at 37.9° . The main diffraction peak observed on WAXD diffractogram of the PA6/nanoclay composites panels occurred at the same value of 2θ degree as for neat PA6 matrix (Figure 3a). Therefore, no significant changes in the

matrix's crystallographic structure were induced by nanofiller in the prepared panels. The formation of a nanostructure was additionally confirmed by SAXD method (Figure 3b). The characteristic peaks for organically modified MMT disappeared completely in the nanocomposite indicating significant alteration of the original parallel arrangement of nanoclay layers.

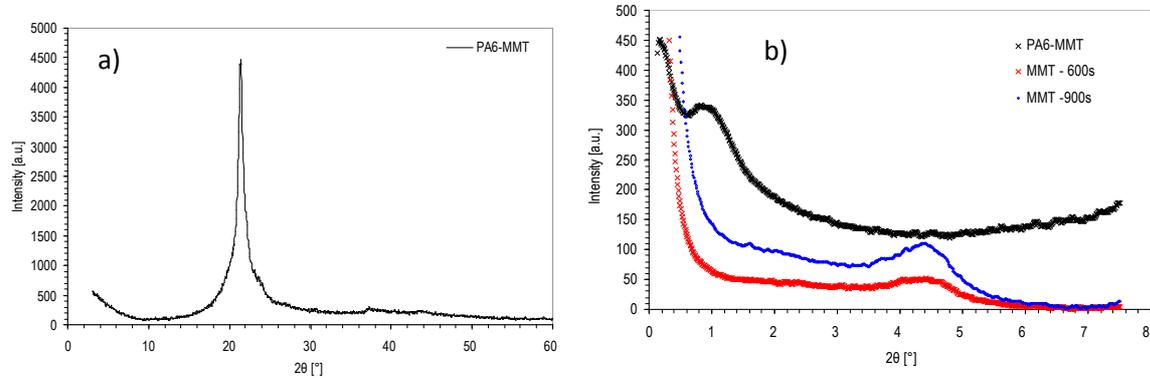


Figure 3 a) WAXD diffractogram of PA6/nanoclay composites b) SAXD PA6/nanoclay composites and organically modified MMT

Nanoscale dust particles during drilling

The sequential alteration of the total number concentration of airborne particles, for a typical sampling cycle is shown in Figure 6. The total number concentration was essentially constant with an average of 1000 (particles/cm³) before drilling. As soon as drilling started the number concentration increased rapidly. The maximum number concentration was reached for the virgin material as soon as drilling was terminated and after approx. 30min for the PA6/nanoclay composites panel. Subsequently, the particle decay was observed with the concentration falling back to the original background level approximately after a post drilling period of 2h. In significant research studies [24-29] the influence of the machining engines as "background noises" on the results has been reported. As the drilling was conducted in a controlled environment, the influence of the machining engine could be reduced to a minimum. Compared with the total particle concentration the particles generated by the drill are minimal and therefore were neglected. The total concentration was around 20,000 cm⁻³ for the nanoclay filled panel, while the unreinforced panel measured a total concentration of approximately 400,000 cm⁻³. As the total concentration was 20 times lower for the reinforced panel, it is likely that the presence of nanoclay in some way retains the formation of high quantity of airborne particles.

Diffusion, gravitational deposition, convection, impaction, and coagulation are some of the complex processes which influence formation and removal of particles in the chamber. Removal of small particles is primary dominated by diffusion while larger particles are mainly affected by gravitation. During diffusion, small particles collide with one another and form larger particles. This process is

known as coagulation and strongly depended on particle size and concentration. An indication of the coagulation rate can be stated identified by the half-life of an individual particle, which is introduced into an atmosphere embracing a defined concentration of such particles [30]. However, coagulation can be neglected for laboratory experiments if the particle concentration was less the $1 \times 10^{12} \text{m}^{-3}$. As the maximum concentration measured in this study did not exceed $3.86 \times 10^{11} \text{m}^{-3}$, coagulation could be neglected [31].

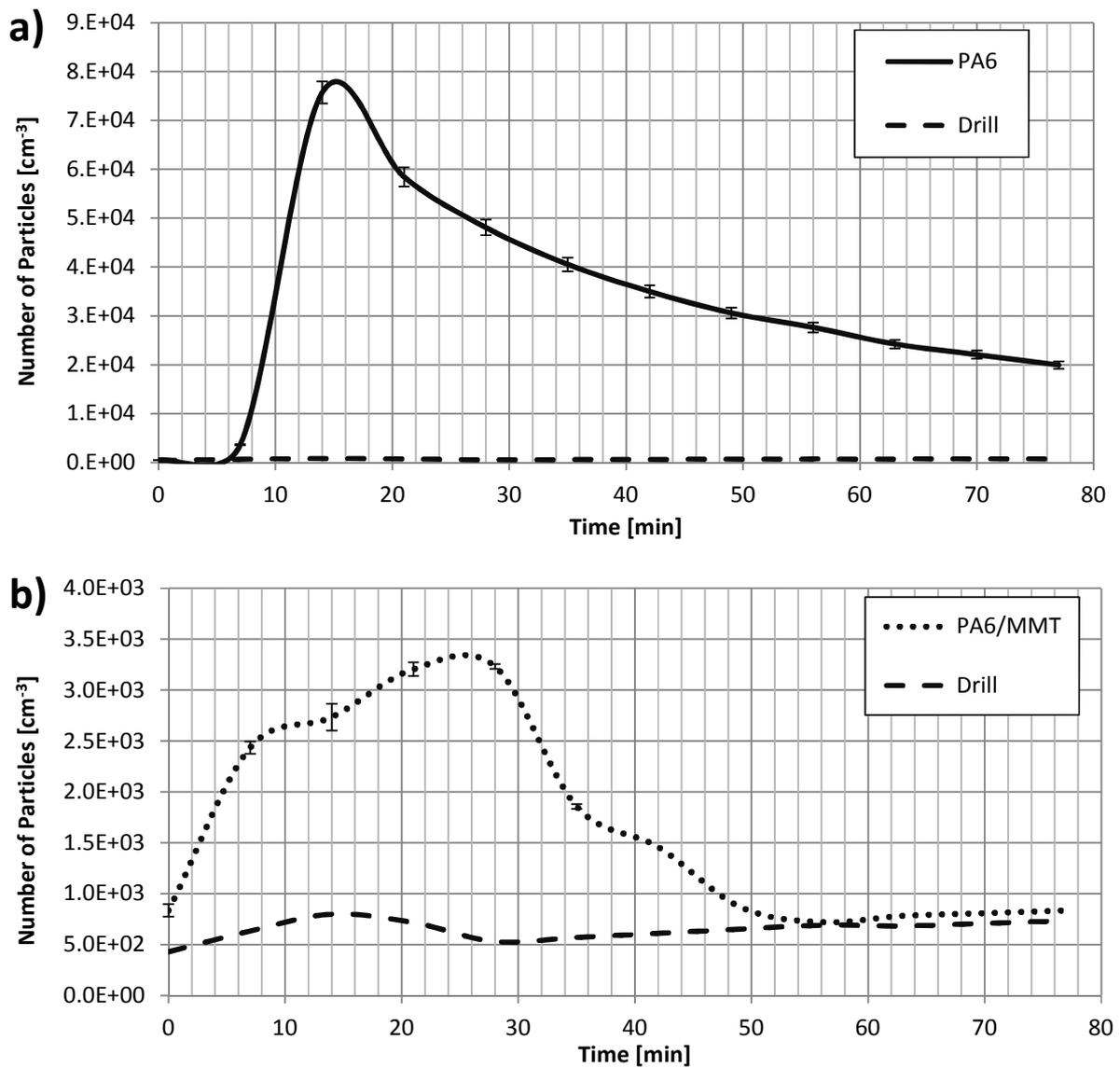


Figure 4 Sequential alteration of number concentration of a typical sampling cycle for neat PA6 (a) and PA6/MMT composite (b)

The particle size distributions of drilling into different material systems are shown in Figure 5. The plots reflected particle size distributions at the time particle concentration reached its maximum and drilling was terminated. The plots presented the normalized distribution with $\Delta N/\Delta \ln d_p$ versus the

particle diameter d_p , where ΔN is the concentration of particles within a specified size interval and $\Delta \ln d_p$ is the difference in the natural logarithm of the largest and smallest particle sizes of that interval. From visual inspection of the graph, it could be noted that the modal diameters was the same for unreinforced and reinforced composite panel. Similar results were obtained by Wohlleben et al. [26], while comparing nanocomposites with their reference materials without nanofillers, that the differences are insignificant in the actual size distribution of aerosols during normal abrasion use. However, they [26] also reported no significant changes between reference materials without nanofillers in the number concentrations, which could not be confirmed by the results we obtained.

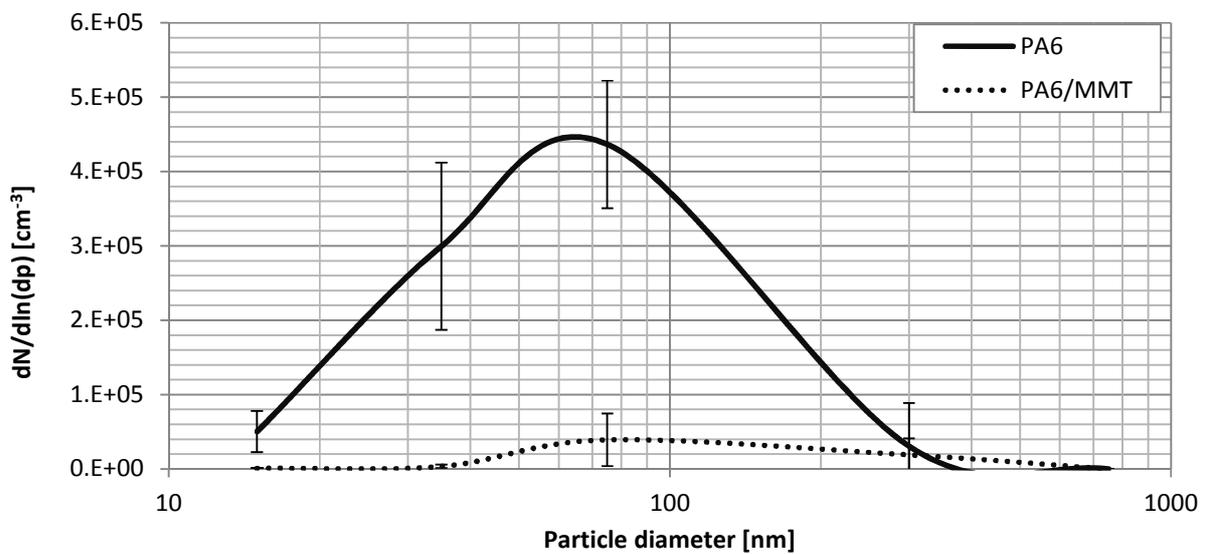
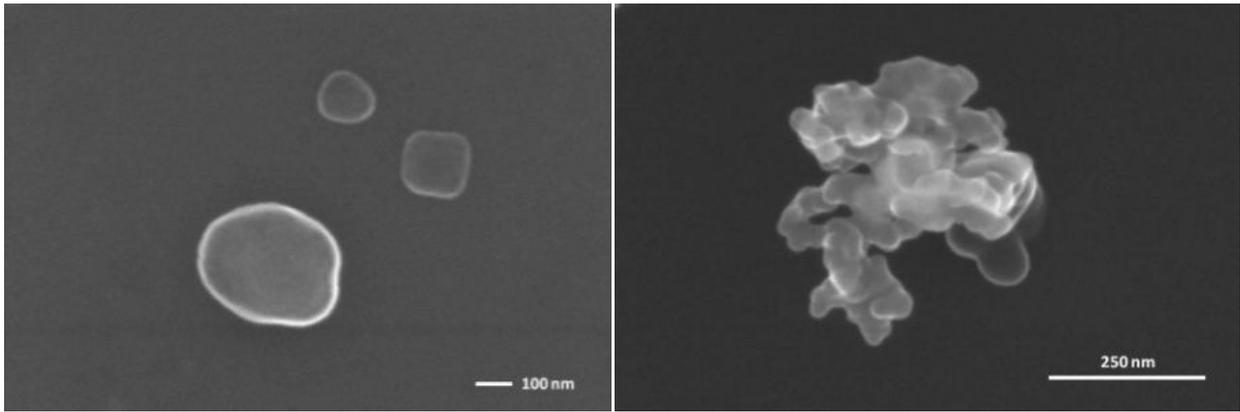


Figure 5 Normalized particle size distributions at ending of the drilling cycles

To support the measurements obtained by SMPS+C, particles were sampled via electrostatic precipitators (ESPs, Grimm Aerosols, Germany) and subjected to JFEI XL30 field emission scanning electron microscope. The scanning electron micrographs of the particles generated during drilling of different composites are represented in Figure 6. Micrographs of the particles generated from PA6 panels showed coagulation of small particles (80nm) to larger particles (300nm). Microscopic investigation of the particles obtained from drilling PA6/nanoclay composites were scattered over the sampling plate and no coagulation could be found. According to Grassian et al. [30] the half time of particles in the size range of 10-200nm in the measured concentration would be between 16-83 min, therefore coagulates of particles are natural for a sampling period of 2h.



a) PA6/nanoclay -particle

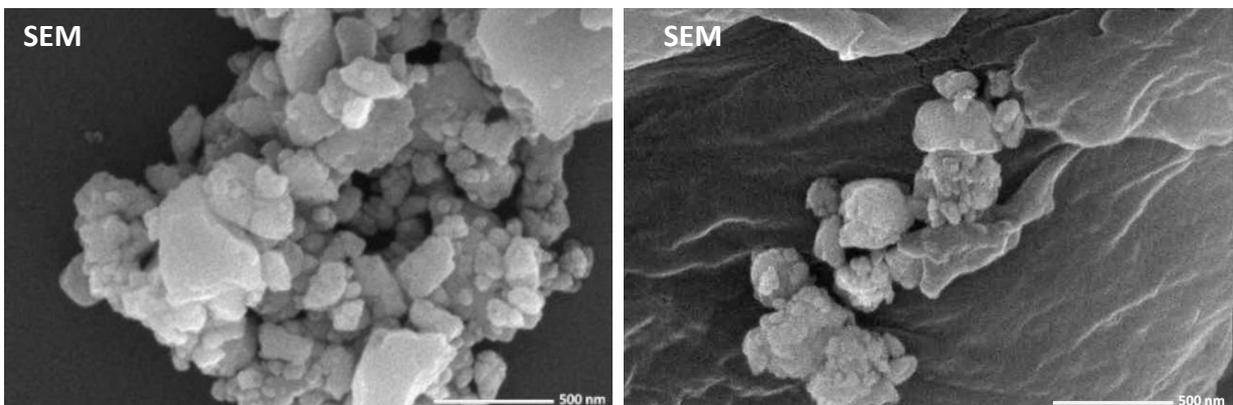
b) PA6-particle

Figure 6 SEM micrographs of a) PA6/nanoclay-particle and b) PA6-particle collected by ESP

As there was a major difference between the particles emitted during drilling of nano filled PA6 and virgin PA6, particles which deposited on the sampling tray inside the chamber were investigated.

Total deposited particles concentration and geometric mean size were measured by Nanosight, after suspending the dry collected particles in deionised water nanoclay filled PA6 specimen, which was double the concentration of the un-filled PA6. This meant that PA6/nanoclay composites generated more particles that deposited, compared to the unreinforced material especially in the size range between 175-350 nm.

The scanning and transmission electron microscopy micrographs confirmed the Nanosight results, as shown in Figure 7. The airborne nanoscale particle concentration of the PA6/nanoclay composites was lower than for the virgin matrix material, and the deposited concentration was higher. An increase in the aerodynamic diameter of particle size results in an increase in the rate of deposition due to gravitational effects.



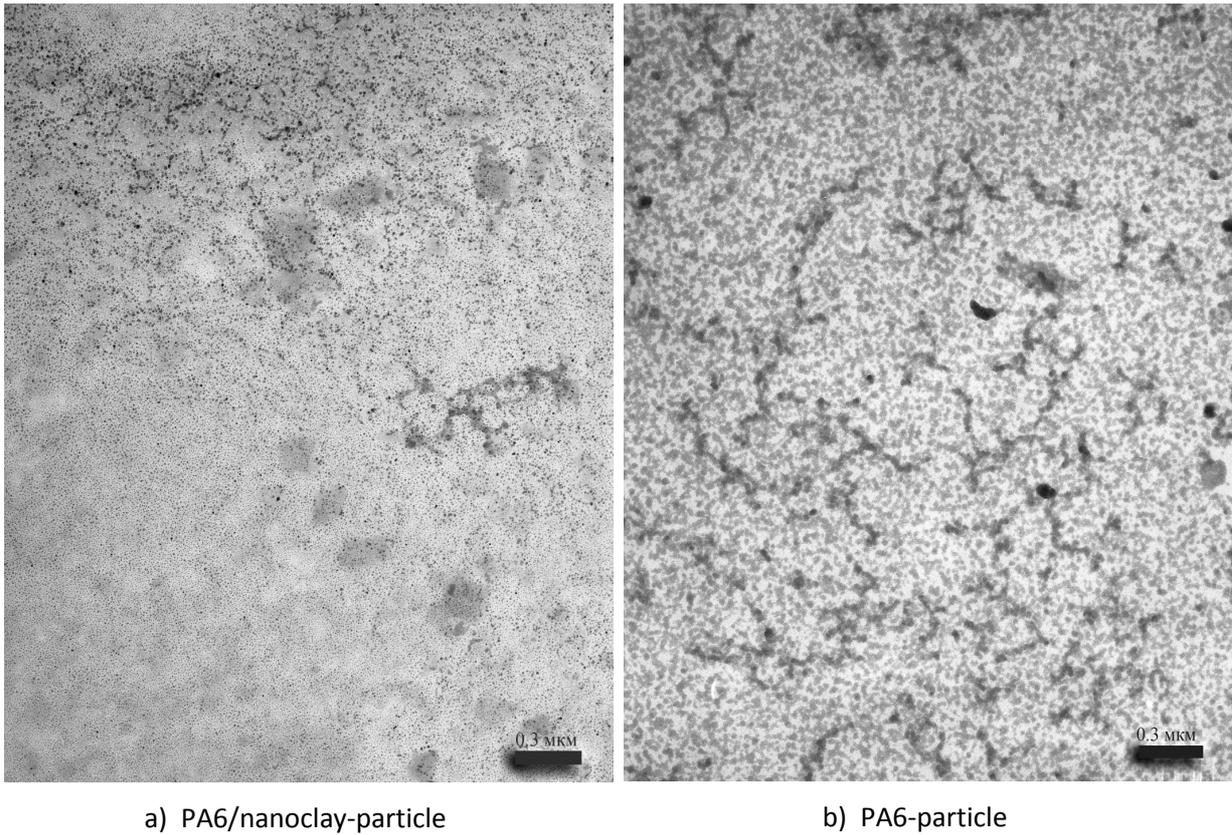


Figure 7 SEM/TEM micrographs of a) PA6/nanoclay-particle and b) PA6-particle

The diffraction pattern of PA6 in a bulk form and a powder are presented in Figure 8. Clearly the polymorphic structure were formed under the action of mechanical force since one strong peak corresponding to the γ crystalline phase of PA6 in bulk form was weakened after drilling an additional peaks at 20.05° and 23.35° occur showing the formation of α -crystal phase of PA6. Recrystallization of polymer matrix may be facilitated by the heat evolved during mechanical drilling of the polymer materials.

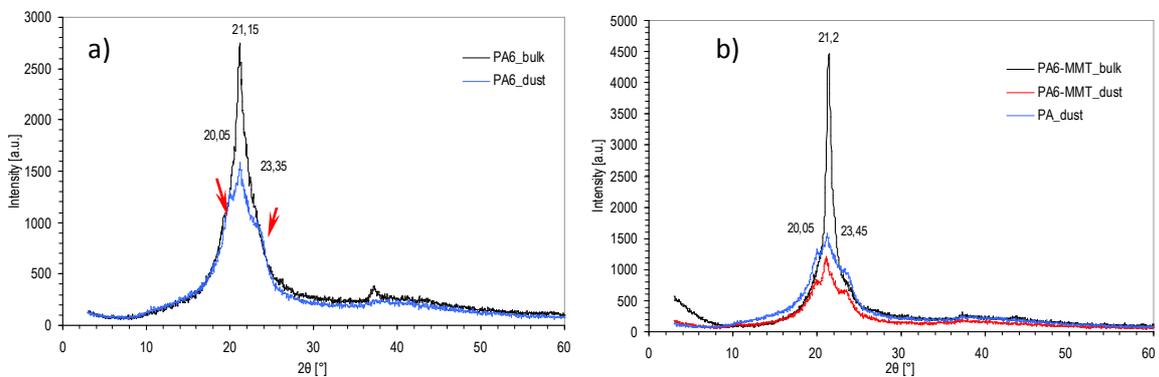


Figure 8 WAXD diffractograms of a) PA6 bulk panel and generated particles and b) PA6/nanoclay bulk panel and generated particles

CONCLUSIONS

Nanoclay filled PA6 nanocomposites were manufactured through direct compounding and compression moulding process. Microscopic analysis of the nanocomposites morphology revealed that the nanoclay was dispersed homogeneously throughout the PA6 matrix. Additional WAXD analysis showed a high degree of exfoliation of the nanoclay in the polymeric matrix. The investigating particle released from PA6 and PA6/nanoclay composites during drilling demonstrated that the airborne particle concentration was decreased by integration of nanofillers in the matrix.

However, while the airborne particle concentration for the PA6/ nanoclay composites was 20 times lower than for the PA6 matrix, the concentration of deposited nanoparticles doubled for the nanocomposite. The results showed that more particles in the size range between 175-350 nm are generated and this particles deposit in a shorter time. The results showed that drilling of nanocomposites generates nanoparticles; therefore, this should be considered and assessed while dealing with machining of nanocomposites. However, it could also be shown that by integration of nanoclay into the PA6 matrix airborne particle quantity can be reduced.

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