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The College of Aeronautics

DEPARTMENT OF ELECTRICAL AND CONTROL ENGINEERING

Explicit formulae for ladder 2-ports

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Summary

Explicit formulae are obtained for the network functions of ladder 2-ports.

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Department of Electrical and Control Engineering

Explicit formulae for ladder 2-ports

By S. R. Deards

Consider the tandem chain of n identical bilateral L-sections represented in Fig. 1. Each section has transfer matrix

$$A = \begin{bmatrix} 1 + ZY & Z \\ Y & 1 \end{bmatrix} \quad (1)$$

hence the tandem chain has transfer matrix

$$A_c = A^n = \phi(A) \quad (2)$$

By Sylvester's interpolation formula, if a square matrix M has order m and distinct latent roots $\lambda_1, \lambda_2, \dots, \lambda_m$ then

$$\phi(M) = \sum_{r=1}^m \phi(\lambda_r) \prod_{\substack{1 \leq k \leq m \\ k \neq r}} \frac{I\lambda_k - M}{\lambda_k - \lambda_r} \quad (3)$$

where I is the unit matrix of order m . Thus, the transfer matrix A_c of the tandem chain in Fig. 1 has the representation

$$A_c = A^n = \frac{A(\lambda_2^n - \lambda_1^n) - I\lambda_1\lambda_2(\lambda_2^{n-1} - \lambda_1^{n-1})}{\lambda_2 - \lambda_1} \quad (4)$$

The trace of A is $a_{11} + a_{22}$ and the determinant of A is unity. Since the trace and determinant of A are preserved under a similarity transformation which converts A into the diagonal matrix with components λ_1 and λ_2 we have

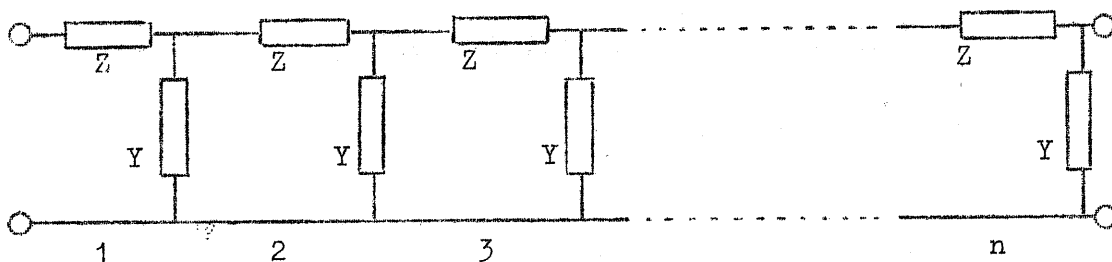


Fig. 1

$$\lambda_1 + \lambda_2 = a_{11} + a_{22} \quad (5)$$

and

$$\lambda_1\lambda_2 = 1 \quad (6)$$

Let

$$\left. \begin{aligned} \lambda_1 &= e^{j\theta} \\ \lambda_2 &= e^{-j\theta} \end{aligned} \right\} \quad (7)$$

so that (4) can be written

$$A_c = A \frac{\sin n\theta}{\sin\theta} - I \frac{\sin(n-1)\theta}{\sin\theta} \quad (8)$$

In view of (5) and (7)

$$a_{11} + a_{22} = 2\cos\theta \quad (9)$$

If we put

$$\mu = \cos \theta \quad (10)$$

then

$$\frac{\sin n \theta}{\sin \theta} = \frac{\sin n \theta}{\sqrt{1 - \cos^2 \theta}} = \frac{\sin(n \arccos \mu)}{\sqrt{1 - \mu^2}} = U_{n-1}(\mu) \quad (11)$$

which is the Chebyshev function of the second kind. Thus, (8) has the representation

$$\begin{aligned} A_c &= A \cdot U_{n-1}(\mu) - I \cdot U_{n-2}(\mu) \\ &= \begin{bmatrix} (1 + ZY) \cdot U_{n-1}(\mu) - U_{n-2}(\mu) & Z \cdot U_{n-1}(\mu) \\ Y \cdot U_{n-1}(\mu) & U_{n-1}(\mu) - U_{n-2}(\mu) \end{bmatrix} \end{aligned} \quad (12)$$

$$\text{where} \quad \mu = 1 + \frac{1}{2}ZY \quad (13)$$

Let us represent the Chebyshev function in the form

$$U_{n-1}(\mu) = \sum_{r=0}^{n-1} \binom{n+r}{2r+1} 2^r (\mu-1)^r \quad (14)$$

or, in view of (13),

$$U_{n-1}(\mu) = \sum_{r=0}^{n-1} \binom{n+r}{2r+1} Z^r Y^r \quad (15)$$

whence follows

$$\begin{aligned} U_{n-1}(\mu) - U_{n-2}(\mu) &= \sum_{r=0}^{n-1} \binom{n+r}{2r+1} Z^r Y^r - \sum_{r=0}^{n-2} \binom{n+r-1}{2r+1} Z^r Y^r \\ &= \sum_{r=0}^{n-2} \left[\binom{n+r}{2r+1} - \binom{n+r-1}{2r+1} \right] Z^r Y^r + Z^{n-1} Y^{n-1} \\ &= \sum_{r=0}^{n-2} \binom{n+r-1}{2r} Z^r Y^r + Z^{n-1} Y^{n-1} \\ &= \sum_{r=0}^{n-1} \binom{n+r-1}{2r} Z^r Y^r \end{aligned} \quad (16)$$

Furthermore

$$\begin{aligned}
 (1 + ZY) \cdot U_{n-1}(\mu) - U_{n-2}(\mu) &= U_{n-1}(\mu) - U_{n-2}(\mu) + ZY \cdot U_{n-1}(\mu) \\
 &= \sum_{r=0}^{n-1} \binom{n+r-1}{2r} Z^r Y^r + \sum_{r=0}^{n-1} \binom{n+r}{2r+1} Z^{r+1} Y^{r+1} \\
 &= \binom{n-1}{0} + \sum_{r=1}^{n-1} \binom{n+r-1}{2r} Z^r Y^r + \sum_{r=0}^{n-2} \binom{n+r}{2r+1} Z^{r+1} Y^{r+1} + \binom{2n-1}{2n-1} Z^n Y^n \quad (17)
 \end{aligned}$$

Consider the second and third terms in (17)

$$\begin{aligned}
 \sum_{r=1}^{n-1} \binom{n+r-1}{2r} Z^r Y^r + \sum_{r=0}^{n-2} \binom{n+r}{2r+1} Z^{r+1} Y^{r+1} &= \sum_{r=0}^{n-2} \left[\binom{n+r}{2r+2} + \binom{n+r}{2r+1} \right] Z^{r+1} Y^{r+1} \\
 &= \sum_{r=0}^{n-2} \binom{n+r+1}{2r+2} Z^{r+1} Y^{r+1} \quad (18)
 \end{aligned}$$

Thus, (17) may be written

$$\begin{aligned}
 (1 + ZY) \cdot U_{n-1}(\mu) - U_{n-2}(\mu) &= 1 + \sum_{r=0}^{n-2} \binom{n+r+1}{2r+2} Z^{r+1} Y^{r+1} + Z^n Y^n \\
 &= \sum_{r=0}^n \binom{n+r}{2r} Z^r Y^r \quad (19)
 \end{aligned}$$

By substituting (15), (16), and (19) in (12) we obtain the explicit form of the transfer matrix of the n-section ladder 2-port, thus

$$A_c = \begin{bmatrix} \sum_{r=0}^n \binom{n+r}{2r} Z^r Y^r & \sum_{r=0}^{n-1} \binom{n+r}{2r+1} Z^{r+1} Y^r \\ \sum_{r=0}^{n-1} \binom{n+r}{2r+1} Z^r Y^{r+1} & \sum_{r=0}^{n-1} \binom{n+r-1}{2r} Z^r Y^r \end{bmatrix} \quad (20)$$

The components of A_c for $n=1$ to 12 are given in the tables below.

Coefficients of a_{11}

| n | ZY | Z ² Y ² | Z ³ Y ³ | Z ⁴ Y ⁴ | Z ⁵ Y ⁵ | Z ⁶ Y ⁶ | Z ⁷ Y ⁷ | Z ⁸ Y ⁸ | Z ⁹ Y ⁹ | Z ¹⁰ Y ¹⁰ | Z ¹¹ Y ¹¹ | Z ¹² Y ¹² |
|----|----|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|---------------------------------|---------------------------------|---------------------------------|
| 1 | 1 | | | | | | | | | | | |
| 2 | 3 | 1 | | | | | | | | | | |
| 3 | 6 | 5 | 1 | | | | | | | | | |
| 4 | 10 | 15 | 7 | 1 | | | | | | | | |
| 5 | 15 | 35 | 28 | 9 | 1 | | | | | | | |
| 6 | 21 | 70 | 84 | 45 | 11 | 1 | | | | | | |
| 7 | 28 | 126 | 210 | 165 | 66 | 13 | 1 | | | | | |
| 8 | 36 | 210 | 462 | 495 | 286 | 91 | 15 | 1 | | | | |
| 9 | 45 | 330 | 924 | 1287 | 1001 | 455 | 120 | 17 | 1 | | | |
| 10 | 55 | 495 | 1716 | 3003 | 3003 | 1820 | 680 | 153 | 19 | 1 | | |
| 11 | 66 | 715 | 3003 | 6435 | 8008 | 6188 | 3060 | 969 | 190 | 21 | 1 | |
| 12 | 78 | 1001 | 5005 | 12870 | 19448 | 18564 | 11628 | 4845 | 1330 | 231 | 23 | 1 |

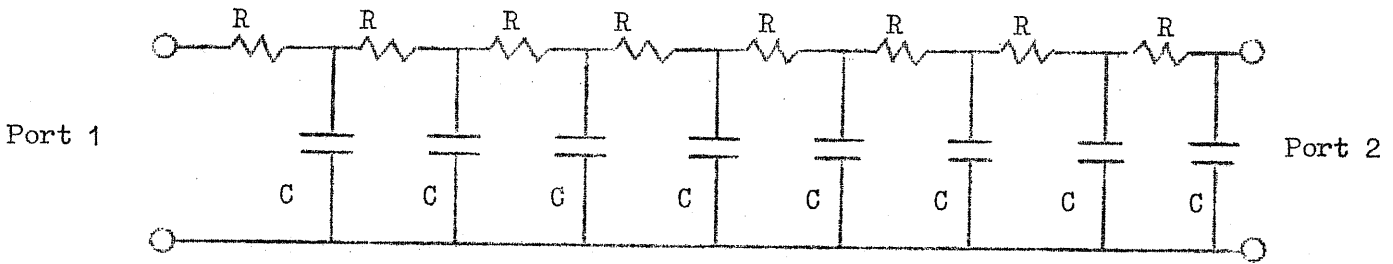
Coefficients of a_{12} and a_{21}

| a_{12} | Z | Z^2Y | Z^3Y^2 | Z^4Y^3 | Z^5Y^4 | Z^6Y^5 | Z^7Y^6 | Z^8Y^7 | Z^9Y^8 | $Z^{10}Y^9$ | $Z^{11}Y^{10}$ | $Z^{12}Y^{11}$ |
|----------|----|--------|----------|----------|----------|----------|----------|----------|----------|-------------|----------------|----------------|
| n | | | | | | | | | | | | |
| 1 | 1 | | | | | | | | | | | |
| 2 | 2 | 1 | | | | | | | | | | |
| 3 | 3 | 4 | 1 | | | | | | | | | |
| 4 | 4 | 10 | 6 | 1 | | | | | | | | |
| 5 | 5 | 20 | 21 | 8 | 1 | | | | | | | |
| 6 | 6 | 35 | 56 | 36 | 10 | 1 | | | | | | |
| 7 | 7 | 56 | 126 | 120 | 55 | 12 | 1 | | | | | |
| 8 | 8 | 84 | 252 | 330 | 220 | 78 | 14 | 1 | | | | |
| 9 | 9 | 120 | 462 | 792 | 715 | 364 | 105 | 16 | 1 | | | |
| 10 | 10 | 165 | 792 | 1716 | 2002 | 1265 | 560 | 136 | 18 | 1 | | |
| 11 | 11 | 220 | 1287 | 3432 | 5005 | 4368 | 2380 | 816 | 171 | 20 | 1 | |
| 12 | 12 | 286 | 2002 | 6435 | 11440 | 12376 | 8568 | 3876 | 1140 | 210 | 22 | 1 |
| a_{21} | Y | ZY^2 | Z^2Y^3 | Z^3Y^4 | Z^4Y^5 | Z^5Y^6 | Z^6Y^7 | Z^7Y^8 | Z^8Y^9 | Z^9Y^{10} | $Z^{10}Y^{11}$ | $Z^{11}Y^{12}$ |

Coefficients of a_{22}

| n | ZY | Z ² Y ² | Z ³ Y ³ | Z ⁴ Y ⁴ | Z ⁵ Y ⁵ | Z ⁶ Y ⁶ | Z ⁷ Y ⁷ | Z ⁸ Y ⁸ | Z ⁹ Y ⁹ | Z ¹⁰ Y ¹⁰ | Z ¹¹ Y ¹¹ | |
|----|----|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|---------------------------------|---------------------------------|---|
| 1 | 1 | | | | | | | | | | | |
| 2 | 1 | 1 | | | | | | | | | | |
| 3 | 1 | 3 | 1 | | | | | | | | | |
| 4 | 1 | 6 | 5 | 1 | | | | | | | | |
| 5 | 1 | 10 | 15 | 7 | 1 | | | | | | | |
| 6 | 1 | 15 | 35 | 28 | 9 | 1 | | | | | | |
| 7 | 1 | 21 | 70 | 84 | 45 | 11 | 1 | | | | | |
| 8 | 1 | 28 | 126 | 210 | 165 | 66 | 13 | 1 | | | | |
| 9 | 1 | 36 | 210 | 462 | 495 | 286 | 91 | 15 | 1 | | | |
| 10 | 1 | 45 | 330 | 924 | 1287 | 1001 | 455 | 120 | 17 | 1 | | |
| 11 | 1 | 55 | 495 | 1716 | 3003 | 3003 | 1820 | 680 | 153 | 19 | 1 | |
| 12 | 1 | 66 | 715 | 3003 | 6435 | 8008 | 6188 | 3060 | 969 | 190 | 21 | 1 |

Example:



In the RC ladder 2-port shown, $n = 8$; $ZY = sCR = sT$ if $T = CR$. We have at once, from the tables, the forward voltage transfer function

$$\frac{1}{a_{11}} = \frac{1}{1+36sT+210s^2T^2+462s^3T^3+495s^4T^4+286s^5T^5+91s^6T^6+15s^7T^7+s^8T^8}$$

and the short-circuit impedance function at port 1

$$\frac{a_{12}}{a_{22}} = R \frac{8+84sT+252s^2T^2+330s^3T^3+220s^4T^4+78s^5T^5+14s^6T^6+s^7T^7}{1+28sT+126s^2T^2+210s^3T^3+165s^4T^4+66s^5T^5+13s^6T^6+s^7T^7}$$

Similarly we may find

$$\frac{a_{11}}{a_{21}} = \text{open-circuit impedance at port 1}$$

$$\frac{a_{12}}{a_{11}} = \text{short-circuit impedance at port 2}$$

$$\frac{a_{22}}{a_{21}} = \text{open-circuit impedance at port 2}$$

$$\frac{1}{a_{21}} = \text{open-circuit transfer impedance}$$

$$a_{12} = \text{short-circuit transfer impedance}$$

With $s = j\omega$,

$$\frac{1}{2a_{21}} \left[(a_{11} - a_{22}) + \sqrt{(a_{11} + a_{22})^2 - 4} \right] = \text{forward iterative impedance}$$

$$\frac{1}{2a_{21}} \left[(a_{22} - a_{11}) + \sqrt{(a_{11} + a_{22})^2 - 4} \right] = \text{reverse iterative impedance}$$

$$\text{arc cosh } \frac{a_{11} + a_{22}}{2} = \text{iterative propagation function}$$

$$\sqrt{\frac{a_{11}a_{12}}{a_{22}a_{21}}} = \text{image impedance at port 1}$$

$$\sqrt{\frac{a_{22}a_{12}}{a_{11}a_{21}}} = \text{image impedance at port 2}$$

$$\ln(\sqrt{a_{11}a_{22}} + \sqrt{a_{12}a_{21}}) = \text{image propagation function}$$

$$\Re \ln \frac{a_{11}Z_2 + a_{21}Z_2Z_1 + a_{12} + a_{22}Z_1}{Z_1 + Z_2} = \text{insertion loss phase}$$

where Z_k is the external impedance at port k.