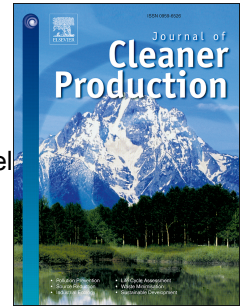


## Accepted Manuscript



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# A Technical Evaluation, Performance Analysis and Risk Assessment of Multiple Novel Oxy-Turbine Power Cycles with Complete CO<sub>2</sub> Capture

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## Abstract

In recent years there has been growing concern about greenhouse gas emissions (particularly CO<sub>2</sub> emissions) and global warming. Oxyfuel combustion is one of the key technologies for tackling CO<sub>2</sub> emissions in the power industry and reducing their contribution to global warming. The technology involves burning fuel with high-purity oxygen to generate mainly CO<sub>2</sub> and steam, enabling easy CO<sub>2</sub> separation from the flue gases by steam condensation. In fact, 100% CO<sub>2</sub> capture and near-zero NO<sub>x</sub> emissions can be achieved with this technology.

This study examines nineteen different oxy-turbine cycles, identifying the main parameters regarding their operation and development. It also analyses the use of advanced natural gas combustion cycles from the point of view of the carbon capture and storage (CCS) and considering political, legislative and social aspects of deploying this technology. Six oxy-turbine cycles which are at the most advanced stages of development (NetPower, CES, Modified Graz, E-MATIANT, AZEP100% and SCOC-CC), were chosen to conduct a Political, Environmental, Social, Technological, Legislative and Economic (PESTLE) risk analysis. This compares each technology with a conventional combined cycle gas turbine (CCGT) power plant without carbon capture as the base-case scenario. Overall, the net efficiency of the different oxy-turbine cycles ranges between 43.6% and 65%, comparable to a CCGT power plant, while providing the extra benefits of CO<sub>2</sub> capture and lower emissions.

A multi-criteria analysis carried out using DECERNS (Decision Evaluation in Complex Risk Network Systems) software determined that, depending on the specific criterion considered, one can draw different conclusions. However, in terms of technology, environment and social opinion, the most promising cycles are the NetPower and CES cycles, whereas from an economic point of view, E-MATIANT is more competitive in the energy market. Giving each factor equal importance, the NetPower cycle must be considered to be the best oxy-turbine cycle based on our analysis.

Most of the oxy-turbine cycles are still under development and only a few cycles (e.g., CES and NetPower) are progressing to the demonstration phase. In consequence, political measures such as CO<sub>2</sub> tax and emission allowances need to be implemented for oxy-turbine technologies to become the preferred option for fossil fuel power plants burning natural gas.

**Key Words:** Carbon capture and storage, oxy-turbine power cycle, air separation unit, combined cycle gas turbine, techno-economic analysis, PESTLE risk analysis

**Abbreviations**

<b>AHPS</b>	Advanced oxy-fuel Hybrid Power System
<b>ASU</b>	Air Separation Unit
<b>CCGT</b>	Combined Cycle Gas Turbine
<b>CCS</b>	Carbon Capture and Storage
<b>CES</b>	Clean Energy Systems
<b>COE</b>	Cost of Electricity
<b>CAPEX</b>	Capital Expenditure
<b>CPU</b>	Compression and Purification Unit
<b>DECERNS</b>	Decision Evaluation in Complex Risk Network Systems
<b>HICES</b>	Hybrid and Improved CES cycle
<b>HRSG</b>	Heat Recovery Steam Generator
<b>HTT</b>	High-Temperature Turbine
<b>IGCC</b>	Integrated Gasification Combined Cycle
<b>ITM</b>	Ion Transfer Membrane
<b>LCA</b>	Life Cycle Assessment
<b>MCDA</b>	Multi-Criteria Decision Analysis
<b>PESTLE</b>	Political, Environmental, Social, Technological, Legislative and Economic risk analysis
<b>ROC</b>	Renewable Obligation Certificate
<b>SCOC-CC</b>	Semi-Closed Oxy-fuel Combustion Combined Cycle
<b>STHS</b>	Solar Thermal Hybrid H <sub>2</sub> O turbine power generation System
<b>TRA</b>	Technology Readiness Assessment

**1. Introduction**

Greenhouse gas emissions from the use of fossil fuels in power generation are a major environmental problem due to their contribution to global warming. In 2013, CO<sub>2</sub> emissions represented 82% of greenhouse gas emissions in the UK and 39% of these CO<sub>2</sub> emissions were produced by the energy supply sector [1]. The use of fossil fuels is expected to continue because of their availability and economic importance. As such, technologies such as carbon capture and storage (CCS) are fundamental in reducing the severity of the greenhouse effect [2].

Oxyfuel is a promising technology for power generation with carbon capture. It consists of burning fuel with high-purity oxygen at near-stoichiometric conditions and uses flue gas recirculation (a + b) to control the combustor temperature. The process follows the global reaction shown in Equation 1.



where  $a$  is recirculated  $CO_2$  (mol) and  $b$  is recirculated  $H_2O$  (mol)

The flue gases contain mainly  $CO_2$  and steam (and low proportions of  $NO_x$ ,  $SO_x$ , CO) which can be separated by condensation of the steam [3]. Subsequently, the steam-depleted stream is normally treated to obtain high-purity  $CO_2$  for further applications.

The advantages of this technology are near elimination of  $NO_x$  by avoiding the ingress of nitrogen into the burner, and the simplicity of the  $CO_2$  sequestration process compared to other techniques since the flue gases contain few impurities. On the other hand, the technology's drawbacks are the energy penalty caused by the requirement of high-purity  $O_2$  and potentially higher materials degradation caused by the presence of excess oxygen at high temperatures and the corrosive potential of any possible fuel sulphur content.

In order to show oxyfuel combustion with carbon capture and storage is feasible, seventeen large-scale projects were initiated worldwide [4]. In most of these projects coal/biomass were the primary fuels. An important example is provided by the Callide Oxyfuel (coal) Project in Australia [5] which consists of the retrofit of a unit of 30 MW into an oxyfuel boiler for electricity generation with  $CO_2$  purification, capture and storage. When the project finished in March 2015, the oxy-combustion unit had operated for 10,000 h and the Compression and Purification Unit (CPU) for 5,500 h [6]. Four of the seventeen projects were recently cancelled or are currently moth-balled due to lack of funding or profitability. The Compostilla Phase II project located in Spain is one of these, which when it was operating showed an impressive net efficiency of 33% capturing 91% of the produced  $CO_2$  [7].

There is a growing worldwide attempt to convert coal-fired power plants to gas-fired plants due to their lower emissions. Consequently, by increasing the number of natural gas power plants,  $CO_2$  capture from gas-fired power plants (Gas-CCS) is presently receiving more attention (e.g., Gas-FACTS a CCS Research Council funded project in the UK). One of the alternatives in Gas-CCS is the oxy-combustion gas turbine cycles and, therefore, further investigations on these cycles look more promising than before.

This technical evaluation addresses a specific type of oxyfuel cycles known as oxy-turbine which are characterised by combusting natural gas or syngas with high-purity oxygen previously separated using a cryogenic air separation unit (ASU), ion transfer membrane (ITM) or other technology. Political, Environmental, Social, Technological, Legislative and Economic (PESTLE) risk analysis and a multi-criteria decision analysis carried out using DECERNS (Decision Evaluation in Complex Risk Network Systems) software have been employed to evaluate and compare different cycles.

This paper assesses nineteen different oxy-turbine power cycles which are shown with their specifications in Table 1.

Table 1: Specification review of the nineteen studied oxy-turbine power cycles

Cycle name	Developers /year	Current Status	Processes	Air Separation System	Fuel / LHV [MJ/kg]	Net power [MW]	Gross efficiency [%]	O <sub>2</sub> separation work [kWh/kg] / Efficiency considering it [%]	Net Efficiency [%]	Highest Pressure [bar]	TIT [°C]	TIP [bar]	Recirculation gas [w/w %]	Carbon Captured [%]	CO <sub>2</sub> purity [molar %]
1. CES [8]	Gou et al., 2006	Pilot scale	Combined Cycle	ASU	CH <sub>4</sub> / 50.02	400	60.94	0.24 / 50	43.6	80-100	760-927	11.6	H <sub>2</sub> O	99	100 (ideal)
2. NetPower [9]	J.R. Allam et al., 2013	Pilot scale	Regenerative Brayton	ASU	CH <sub>4</sub> / 50.02	250	-	- / 70.5	55.1	300	1150	30	CO <sub>2</sub>	100 (ideal)	100 (ideal)
3. GRAZ [10]	H. Jericha., 1985	Thermodynamic analysis (IPSEpro)	Quasi CC (Brayton and Rankine)	ASU	Syngas (0.1 CO <sub>2</sub> , 0.4 CO, 0.5 H <sub>2</sub> molar fraction)	74.75	63.30	0.25 / 55	52.5	180	1400	40	CO <sub>2</sub> + H <sub>2</sub> O – 79.26	100 (ideal)	93
4. S-GRAZ [10]	W. Sanz et al., 2005	Thermodynamic analysis (IPSEpro)	Quasi CC (Brayton and Rankine)	ASU	Syngas (0.1 CO <sub>2</sub> , 0.4 CO, 0.5 H <sub>2</sub> molar fraction)	82.75	68.60	0.25 / 60.3	57.7	180	1400	40	CO <sub>2</sub> + H <sub>2</sub> O – 81.1	100 (ideal)	94
5. Modified GRAZ [11]	H. Jericha et al., 2007	Thermodynamic analysis (IPSEpro)	Rankine + Quasi CC (Brayton and Rankine)	ASU	CH <sub>4</sub> / 50.02	400	66.55	0.25 / 54.84	53.09	180	1400	40	CO <sub>2</sub> + H <sub>2</sub> O	100 (ideal)	99
6. MATIANT [12, 13]	P. Mathieu and E. Iantovski., 1998	Thermodynamic analysis (ASPEN+ & EES)	Quasi CC (Brayton with reheat and Brayton)	ASU	NG / 42	642.5 kJ/kg CO <sub>2</sub> recirculated	49.20	0.28 / 44.2	44.2(CO <sub>2</sub> compression in cycle)	300	1300	40	CO <sub>2</sub> – 92	99.98	99
7. E-MATIANT [14]	S. Houyou, P. Mathieu and R. Nihart., 1999	Thermodynamic analysis (ASPEN+ & EES)	Regenerative Brayton with reheat	ASU	NG / 42	560 kJ/kg CO <sub>2</sub> recirculated	60	0.25 / 47	47 (CO <sub>2</sub> compression in cycle)	110	1300	60	CO <sub>2</sub>	99	99
8. CC-MATIANT [15]	S. Houyou, P. Mathieu and R. Nihart., 1999	Thermodynamic analysis (ASPEN+ & EES)	Combined Cycle with reheat	ASU	NG / 42	605 kJ/kg CO <sub>2</sub> recirculated	-	-	49.75(CO <sub>2</sub> compression in cycle)	210	1300	-	CO <sub>2</sub>	99	99
9. AZEP 100% [16, 17]	S. Sundkvist et al., 2001	Lab Scale	Combined cycle (Brayton with air)	ITM	NG / 48.43	45.7	48.40	-	47.9	20	1200	18	CO <sub>2</sub> + H <sub>2</sub> O – ≈90	100	-
10. AZEP 85% [16, 17]	S. Sundkvist et al., 2001	Thermodynamic analysis (IPSEpro)	Combined cycle (Brayton with air) with reheat	ITM	NG / 48.43	53.3	50.30	-	49.8	20	1327	-	CO <sub>2</sub> + H <sub>2</sub> O – ≈90	85	-
11. SCOC-CC [10]	W. Sanz et al., 2007	Thermodynamic analysis (IPSEpro)	Combined Cycle	ASU	CH <sub>4</sub> / 50.02	400	61.45	0.25 / 51.68	49.75	120	1400	40	CO <sub>2</sub> – 90.6	100 (ideal)	98.8
12. ZEITMOP [18]	E. Yantovsky et al., 2002	Thermodynamic analysis (ASPEN+)	Brayton with air + quasi CC (two Brayton cycles)	ITM	CH <sub>4</sub> / 50.02	25.46	50.9	-	50.9 (CO <sub>2</sub> compression in cycle)	210	1400	14	CO <sub>2</sub> - 93	100 (ideal)	-

Cycle name	Developers /year	Current Status	Processes	Air Separation System	Fuel / LHV [MJ/kg]	Net power [MW]	Gross efficiency [%]	O <sub>2</sub> separation work [kWh/kg] / Efficiency considering it [%]	Net Efficiency [%]	Highest Pressure [bar]	TIT [°C]	TIP [bar]	Recirculation gas [w/w %]	Carbon Captured [%]	CO <sub>2</sub> purity [molar %]
13. OXYF-REF [19,20]	N. Zhang and N. Lior, 2008	Thermodynamic analysis (ASPEN+)	Quasi CC (Brayton and Rankine)	ASU	NG / 46.3	404.84	64.33	- / 55.42	50.82	150	1300	15	CO <sub>2</sub> + H <sub>2</sub> O – 74.1	100 (ideal)	84
14. COOLCEP-S [21]	S Deng et al., 2002	Thermodynamic analysis (ASPEN+)	Regenerative Rankine-like	ASU	LNG / 49.2	20	59.1	0.22 / 52.29	52.29 (no CO <sub>2</sub> compression considered)	73.5	900	28	CO <sub>2</sub> - 97	100	100 (ideal)
15. Water-steam Rankine cycle with a steam-CO <sub>2</sub> recuperative-reheat cycle [22]	C. Gou, R. Cai, and H. Hong., 2006	Thermodynamic analysis (ASPEN+)	Quasi CC (Brayton with reheat and Rankine)	ASU	CH <sub>4</sub> / 50.02	67.63	-	0.25 / -	47.12	300	1300	38.8	H <sub>2</sub> O	>99	>99
16. Water-steam Rankine cycle with steam-CO <sub>2</sub> recuperative-reheat cycle and a topping Brayton cycle [22]	C. Gou, R. Cai, and H. Hong., 2006	Thermodynamic analysis (ASPEN+)	Quasi CC (Brayton with reheat and Rankine)	ASU	CH <sub>4</sub> / 50	72.56	-	0.25 / -	50.64	300	1300	38.8	H <sub>2</sub> O (COMB1) and CO <sub>2</sub> + H <sub>2</sub> O (COMB2)	>99	>99
17. Novel O <sub>2</sub> /CO <sub>2</sub> [23]	W. Cao and D. Zheng., 2006	Thermodynamic analysis (ASPEN+)	Regenerative Brayton	ASU	CH <sub>4</sub> / 50.02	24.8	59.5	0.28/51.1	48.9	10	1300	8.85	CO <sub>2</sub> - 95.6	100 (ideal)	99.5
18. LNG quasi-combined supercritical CO <sub>2</sub> Rankine cycle [24]	N. Zhang and N. Lior., 2003	Thermodynamic analysis	Quasi CC (Brayton and Rankine-like)	ASU	CH <sub>4</sub> / 50.02 (Assumed that LNG is CH <sub>4</sub> )	71.4	72.3	0.25 / 65.1	65	156	1300	29.1	CO <sub>2</sub> – 94.3	100 (ideal)	100 (ideal)
19. ZE-SOLRGT [25]	Zhang and Lior., 2012	Thermodynamic analysis (ASPEN+)	Quasi CC (Brayton and Rankine)	ASU	CH <sub>4</sub> / 50.03	496.07	61.54	0.25 / 54.27	50.7	157.5	1308	14.55	CO <sub>2</sub> + H <sub>2</sub> O - 59	100 (ideal)	87

According to Table 1, the key factors which determine the availability and performance of the oxy-turbine panorama are the current status and the net efficiency. Considering the current status, most of the cycles can be considered as being under development (e.g., at the stage of being investigated via thermodynamic analysis). In fact only AZEP, CES and NetPower can be considered to be at an advanced status given that CES and NetPower cycles have been built at the pilot scale to demonstrate their feasibility [8, 26] followed by the AZEP whose components have been tested at laboratory scale [27]. Overall, the net efficiency of the different cycles ranges between 43.6 and 65%, comparable to a combined cycle gas turbine (CCGT) power plant [28].

The core of CES's design is adapted from rocket engine technology and burns gaseous or liquid fuels with pure gaseous oxygen. The high-pressure oxy-combustor produces a steam/CO<sub>2</sub> working fluid for expansion in a turbine. NetPower, however, uses supercritical CO<sub>2</sub> as the working fluid in a radically new cycle. Carbon capture in oxy power cycles is an inherent feature of the process, not an add-on with very large parasitic loads, as with "conventional" CCS approaches. For most of these cycles compatible fuels include natural gas, syngas from coal, refinery residues, biogases, landfill gas, and oil/water emulsions. A demonstration project for the CES cycle including the design, analysis, and testing of a modified Siemens SGT-900 gas turbine was done by Clean Energy Systems (CES), with support from Siemens Energy and Florida Turbine Technologies (FTT), through a U.S. Department of Energy (DOE) funding program [29]. Component test results proved the feasibility of the gas turbine conversion to an oxy-fuel turbine; however, further testing was recommended to verify performance at higher power levels, and longer durations [30]. For demonstration of the NETPower cycle, the company is partnering with CB&I, Toshiba Corporation, and Exelon Corporation to demonstrate this new system in a 50 MWt natural gas power plant [31].

### 1.1. Classification by recirculation

Regarding the recirculation of flue gases, researchers have carried out several studies in order to determine if recirculating CO<sub>2</sub>, steam, or a mixture of both offers more thermodynamic advantages. Thus, these cycles were classified using these criteria, as shown in Table 2.

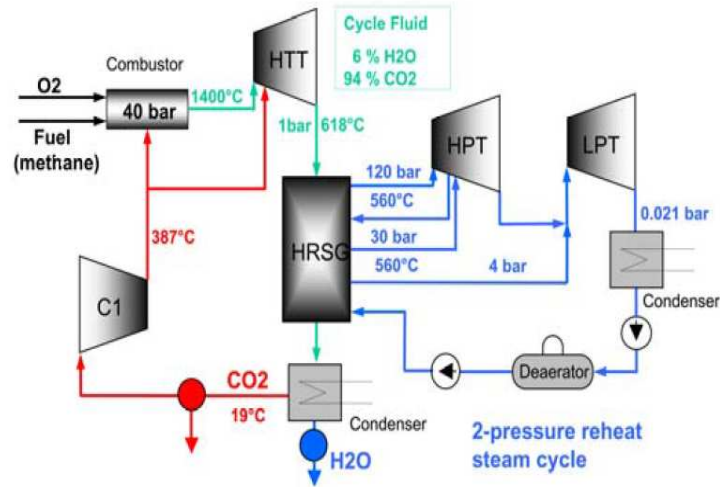
**Table 2:** Classification of oxy-turbine cycles by recirculation fluid

	Recirculated working fluid		
	CO <sub>2</sub>	H <sub>2</sub> O	CO <sub>2</sub> + H <sub>2</sub> O
NetPower		CES	Graz cycles*
MATIANT*		Water cycles*	AZEP*
SCOC-CC			OXYF-REF
ZEITMOP			ZE-SOLRGT
COOLCEP-S			
Novel O <sub>2</sub> /CO <sub>2</sub>			
LNG quasi-combined			

\* refers to all their variants

CO<sub>2</sub> is the most popular recirculation fluid for the oxy-turbine cycles reviewed. In the condenser, CO<sub>2</sub> and steam are separated by steam condensation and the remaining carbon dioxide is divided into two streams. Usually, at least 90% of the CO<sub>2</sub> produced is recirculated to the combustor, whereas the remaining part is purified and compressed for further applications [32, 33]. For example, in Semi-

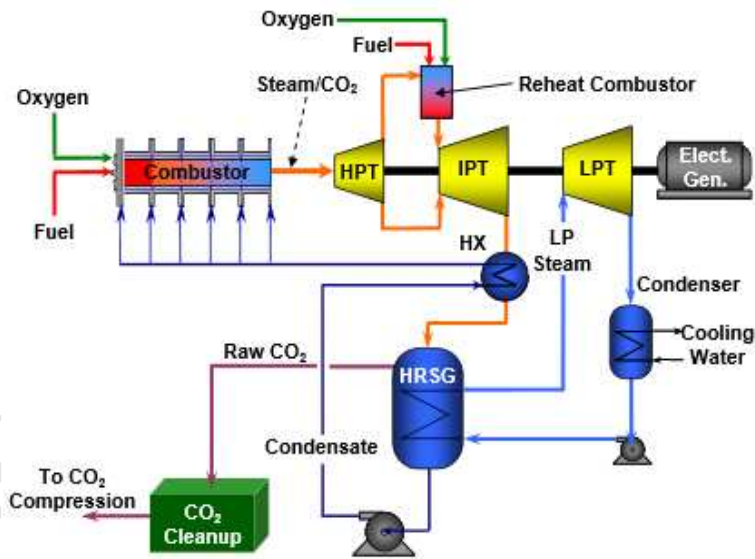
Closed Oxy-fuel Combustion Combined Cycle (SCOC-CC), recirculated  $\text{CO}_2$  is represented as a red line in the diagram shown in Figure 1.



Legend: C1 – Compressor, HTT – High-temperature turbine, HRSG – Heat recovery steam generator, HPT – High-pressure turbine, LPT – Low-pressure turbine

Figure 1: SCOC-CC schematic [10]

Another option, only seen in two of the considered oxy-turbine cycles, is to use some of the steam separated in the condenser instead of  $\text{CO}_2$ . The CES cycle illustrates the recirculation process with water, which is represented in Figure 2 as a dark blue line.

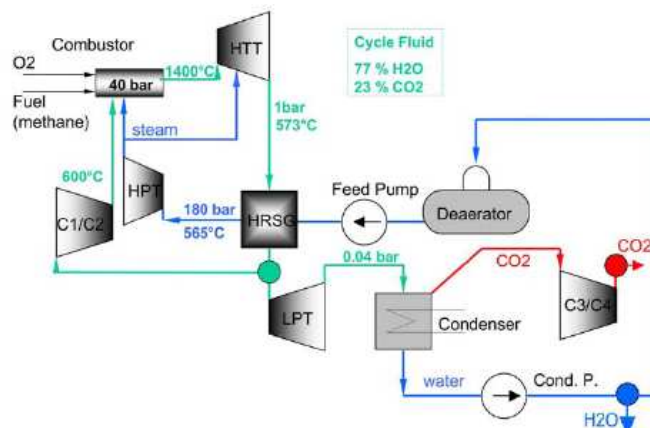


Legend: HX – Heat Exchanger, HTT – High-temperature turbine, HRSG – Heat recovery steam generator, HPT – High-pressure turbine, IPT – Intermediate-pressure turbine, LPT – Low-pressure turbine

Figure 2: CES cycle schematic [8]



The last group includes those cycles which recirculate a mixture of  $\text{CO}_2$  and  $\text{H}_2\text{O}$ . The S-Graz cycle uses this process as it is represented in Figure 3.



Legend: C1/C2 & C3/C4 – Compressor, HTT – High-temperature turbine, HRSG – Heat recovery steam generator, HPT – High-pressure turbine, LPT – Low-pressure turbine

Figure 3: S-Graz cycle schematic [11]

Depending on the recirculation of working fluid in gas turbines ( $\text{CO}_2$ ,  $\text{H}_2\text{O}$  and  $\text{CO}_2 + \text{H}_2\text{O}$ ), oxy-fuel technologies benefit or suffer depending on their cycles. First of all, recycling  $\text{CO}_2$  minimises the CCS costs by the use of almost 96% of the total  $\text{CO}_2$ ; however, the turbomachinery must be completely redesigned (gas turbine, combustor, compressor and heat exchanger) since higher temperatures and pressures are achieved [34]. In addition, the materials suffer from some limitations such as corrosion and incomplete combustion due to high levels of  $\text{CO}$ ,  $\text{H}_2$  and  $\text{OH}^\cdot$  [35]. In the second case,  $\text{H}_2\text{O}$  (steam) lowers capital costs whilst increasing the net efficiencies, since steam turbines are proven technologies; on the other hand, an extra heat recovery system and more working compressors need to be installed at considerably high pressures and temperatures ( $1300^\circ\text{C}$  and 30-50 MPa) [3]. Last but not least,  $\text{CO}_2 + \text{H}_2\text{O}$  offer a balanced approach meeting the constraints of CCS costs and energy efficiency as well as a drop in air separation costs [36]. By contrast as retrofitting, they might present lower efficiencies and low power outputs [37].

### 1.2. Classification by power generation

In order to classify the oxy-turbine power cycles from a thermodynamic point of view, the authors have suggested five different concepts relevant to power generation. Concretely, these processes modify the thermodynamic parameters of the working fluid, changing mainly its pressure and temperature to increase the efficiency of the cycle. Table 3 shows this classification:

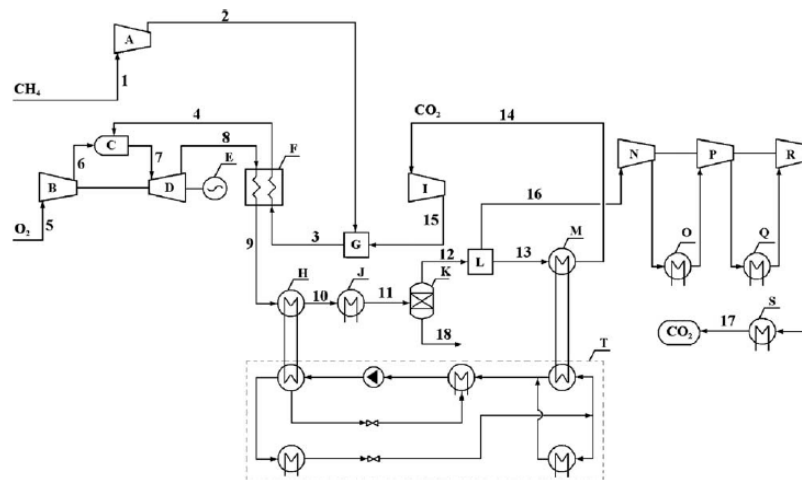
**Table 3:** Classification of oxy-turbine cycles by their power generation processes

Regenerative Brayton	Regenerative Brayton with reheat	Regenerative Rankine-like	Combined cycle	Quasi-combined cycle
NetPower	E-MATIANT	COOLCEP-S	CC-MATIANT	MATIANT
Novel O <sub>2</sub> /CO <sub>2</sub>			SCOC-CC	Graz Cycles*
			AZEP*	ZE-SOLRGT
			CES	Water Cycles*
				OXYF-REF
				LNG quasi-combined
				ZEITMOP

\* refers to all their variants

The five different groups are described as follows:

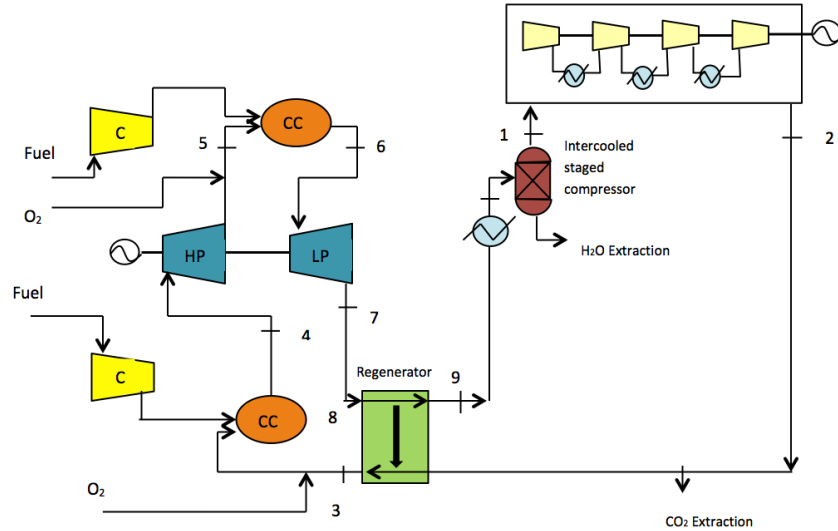
Regenerative Brayton: After the expansion of the working fluid in a gas turbine, the calorific energy of the flue gases is used to heat other parts of the working fluid. In this type of cycle, the working fluid does not suffer any phase change. One example of this is the Novel O<sub>2</sub>/CO<sub>2</sub> cycle shown in Figure 4, where the flue gases at point 8 go to a heat exchanger in order to preheat the recirculated fluid before entering the combustor.



Legend: A CH<sub>4</sub> compressor, B O<sub>2</sub> compressor, C combustor, D turbine, E generator, F CO<sub>2</sub>-NG reformer, G mixer, H heat exchanger, I CO<sub>2</sub> compressor, J cooler, O&Q intercooler, K separator, L splitter, M CO<sub>2</sub> inlet cooler, N,P,R compressor, S condenser, T ammonia absorption refrigeration

**Figure 4:** Novel O<sub>2</sub>/CO<sub>2</sub> cycle schematic [23]

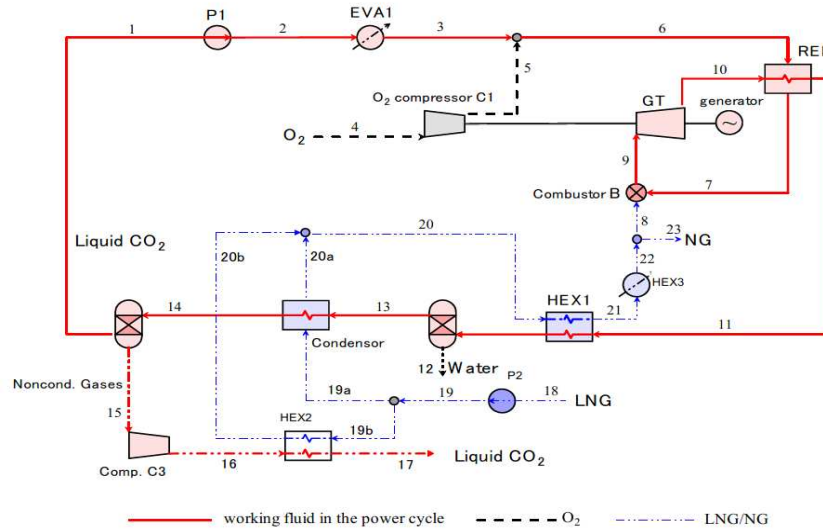
Regenerative Brayton with reheat: The cycles included in this group have a similar working principle to the first group but contain a reheat stage. In this stage and after the first expansion, the working fluid goes into another combustor and the flue gases are further expanded. The E-MATIANT, shown in Figure 5, is the only oxy-turbine cycle that belongs to this group.



Legend: C – Compressor, CC – Combustion chamber, HP – High-pressure turbine, LP – Low-pressure turbine

**Figure 5:** E-MATIANT cycle schematic [38]

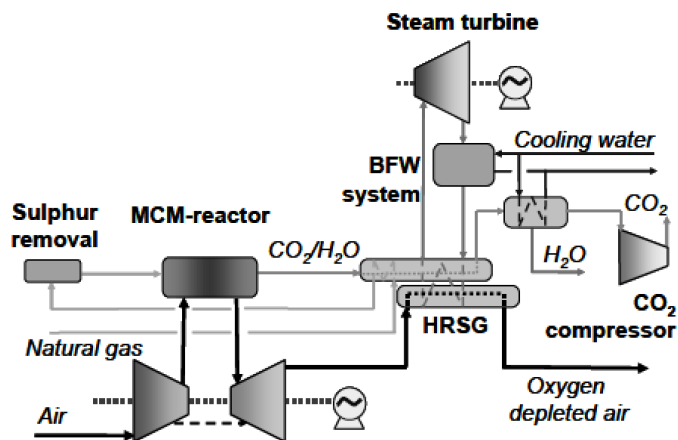
Regenerative Rankine-like: This is similar to the Regenerative Brayton but in this case the working fluid suffers phase changes (gas-liquid-gas). In Figure 6, the COOLCEP-S cycle is shown. The CO<sub>2</sub> is liquefied in the condenser (point 13) and evaporated in EVA1 (point 3).



Legend: P1 & P2 – Pump; HEX1 HEX2, HEX3 – Heat Exchanger; EVA1 - Evaporator; REP – Regenerator; GT – Gas turbine; NG – Natural gas; LNG – Liquefied natural gas

**Figure 6:** COOLCEP-S Cycle schematic [21]

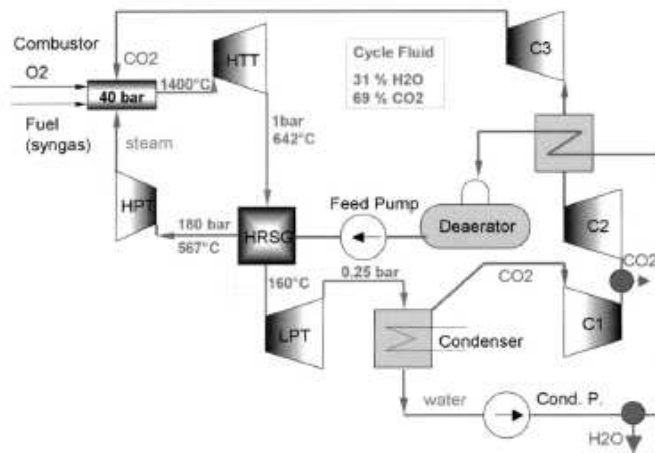
Combined Cycle: It combines two different cycles, Brayton and Rankine. The flue gases from the Brayton cycle are used to generate steam in the Rankine cycle through separated circuits. The AZEP cycle follows this principle, as seen in Figure 7.



Legend: BFW – Boiled feed water, MCM – Oxygen mixed conducting membrane, HRSG – Heat recovery steam generator

Figure 7: AZEP cycle schematic [17]

Quasi-Combined Cycle: This combines two different cycles, one high-temperature and the other low-temperature (not necessarily a Brayton linked to a Rankine), where the working fluids are in a common circuit. The Graz cycle belongs to this group, and is shown in Figure 8. The flue gases coming from the high-temperature turbine (HTT) are used as a hot sink to generate steam in the heat recovery steam generator (HRSG). After this, the water is separated by condensation and is delivered to the previously mentioned HRSG where it becomes steam.



Legend: C1, C2 & C3 – Compressor, HTT – High-temperature turbine, HRSG – Heat recovery steam generator, HPT – High-pressure turbine, LPT – Low-pressure turbine

Figure 8: Graz cycle schematic [10]

### 1.3. Cycle integration with renewables

To implement renewable energy approaches in the oxy-turbine power plant there are only three technologically and economically viable sources: solar (thermal), biomass and biofuels (liquid and gas phases). The lack of research in this field has made it impossible at present to explore other sustainable sources such as wind or geothermal in oxy-turbine power plants.

### **1.3.1. Solar**

There are several oxy-turbine technologies that back their power generation with solar thermal to heat water and optimise the HRSG system. The main technology is ZE-SOLGRT, which is an adaptation of the Graz cycle implementing solar thermal [25]. There are also three new systems that incorporate solar thermal: the Solar Thermal Hybrid H<sub>2</sub>O turbine power generation System (STHS), the Advanced oxy-fuel Hybrid Power Generation cycle (AHPS) [39] and the Hybrid and Improved CES cycle (HICES) [22].

These technologies offer the possibility of heating the working fluid and optimising the HRSG, minimising fuel and oxygen consumption. However, in general, they produce low cycle efficiency compared to the standard oxy-turbine cycles. In addition, they are highly affected by the intermittency of solar radiation due to seasonality and geographical limitations.

### **1.3.2. Biomass**

Currently, biomass is used as fuel in oxyfuel technologies by using it with different types of coal (anthracite, bituminous, peat and lignite) in a boiler to generate steam. However, the use of solid fuels in oxy-turbine cycles would damage the turbine when flue gases are expanded. The possibility of implementing solid fuels (coal) in an oxy-turbine cycle was studied by Oki et al. [40]. They concluded that it would be feasible only by integrating a gasifier into a combined cycle (IGCC). On the other hand, several thermogravimetric analyses have been conducted to study the feasibility of employing biomass in oxy-turbine cycles. These studies suggest the possibility of using several biological feedstocks such as forest residues (e.g., from poplar and switchgrass), agricultural residues (e.g., corn stover, sugarcane bagasse, pine sawdust, torrefied pine sawdust and olive pits) and waste (e.g., MSW, sewage sludge and slurry) [41, 42].

### **1.3.3. Biofuels (liquid and gaseous states)**

There are studies on the use of biofuels such as diesel, ethanol and glycerol (previously treated) in oxy-turbine power plants [43-45]. Indeed, CES offers assurances that its technology is ready to be fuelled from landfill gas, bio-digester gas and glycerine (glycerol) followed by oxyfuel combustion. Additionally, oxyfuel technologies can help third and fourth generation biofuels since both microalgae and bioengineered microbes are fed with sequestered CO<sub>2</sub> to grow and produce biofuels such as ethanol, diesel, jet fuel and gasoline [46].

## **2. Research methodology**

The evaluation of each oxy-turbine cycle is based on a PESTLE risk analysis which stands for assessments of the cycles from Political, Environmental, Social, Technological, Legislative and Economic (PESTLE) points of view [47]. The complexity of evaluating the political, legislative and social factors for each cycle has led to a general analysis of these three aspects applied to the CCS field without going into detail for each specific cycle.

A Multi-Criteria Decision Analysis (MCDA) has been carried out to evaluate the technological, economic, environmental and social factors using DECERNS software [48]. This type of analysis evaluates different alternatives attending to different factors, which have a certain weight assigned in order to decide which alternative is the most appropriate. Due to better availability of the technical information in the literature, AZEP, CES, E-MATIANT, Modified Graz, NetPower and SCOC-

CC have been chosen for this analysis. The results of this study enable the identification of the best cycle for the considered factors. Our contribution is to conduct a MCDA according to the data found in the literature, thus, a robust comparison between the most developed oxy-fuel cycles and a base case (CCGT) can be done.

### **2.1. Political and Legislative**

In general, CCS is a developing technology that has not yet been proven at large scale. It has been estimated that commercial power plants with CCS technology will not be deployed until the second tranche of units is built [49]. The first tranche will, therefore, be useful to identify the technical problems that can arise in real power plants with these technologies. Consequently, several political measures should be applied with the intention of enhancing the economic viability of this type of power plant.

The main driver that will make CCS technology profitable for investors will be some form of CO<sub>2</sub> tax. This tax will not be high enough to replace conventional fossil fuel power plants until the low-carbon technologies are as commercialised as the conventional ones and sufficiently developed to cover most of the energy demand. Therefore, until that happens, other measures are needed to promote the development and proliferation of CCS technologies. Such measures should serve as a support for building new plants with carbon capture or for retrofitting existing power plants with this technology to start capturing carbon dioxide. The measures could include either direct financing or imposing measures that restrict the amount of emissions by a plant or by a sector.

An example of an adopted measure is the one implemented first in California and later in some other states in the USA and in Europe [49]. The Electricity Emissions Performance Standards (EPSs) limits the amount of CO<sub>2</sub>/MWh that a power plant can emit. For example, in the EU the limit imposed is 350 kg CO<sub>2</sub>/MWh applicable for new and existing plants in 2020 and 2025, respectively [50]. An important consideration is that when a CCS technology is applied in a new plant, it is built to capture high degree of CO<sub>2</sub> (at least 85%). Otherwise, the limit of 350 kg CO<sub>2</sub>/MWh on the emissions amount could be equally achieved by a highly efficient power plant with no carbon capture or by retrofitting a small part of the plant leaving the rest without carbon capture. Consequently, this will help the mitigation of climate change and demonstration of these technologies at small scale, but not properly promote the construction and development of CCS technologies because it does not provide any financial support, but only imposes a legislative restriction.

Another example in terms of measures is the EU Emission Trading Scheme. In 2009 the EU set 300 million emission allowances to support CCS and innovative renewable energy projects [49]. An EU allowance permits the holder to emit 1 tonne of CO<sub>2</sub>. This incentive is similar to the Renewable Obligation Certificates (ROCs) in the UK, but unlike them, the sectoral standard market seems less likely to collapse until the CCS projects are consolidated. Overall, it appears that the EU Emission Trading Scheme provides a greater incentive than the EPS to build new CCS plants, since the less they emit the more financial support they obtain. Overall, it seems to be the most effective technique since it not only penalises CO<sub>2</sub> emissions but also finances deployment of CCS technologies.

## 2.2. Technological

To evaluate the selected cycles in terms of technological aspects, two characteristics have been considered: the net efficiency and the technical level of readiness, with 60% and 40% weight, respectively, since one of the aims of oxy-turbine cycles is to achieve efficiencies comparable to those obtained in conventional plants. A higher weight percentage is given to the net efficiency (60%) compared to the technical level of readiness (40%) because oxy-fuel technologies are looking forward to meet the net efficiency of CCGTs. Furthermore, the stage of development in most of the oxy-turbine cycles is still in the thermodynamic assessment phase and, therefore, it is important to bring the readiness level to attention if we are seeking an available practical replacement option to CCGT cycles.

The net efficiency and the level of readiness of each cycle appear in Table 4.

The level of readiness was assigned according to the stage of development of each cycle, graded from 1 to 9 following the “Technology Readiness Assessment (TRA) Guidance” for the energy supply sector [51]. Each level refers to a specific stage of development according to the literature review and reports of the oxy-fuel technologies, as shown in Table 4.

## 2.3. Economic

The two factors used for the economic evaluation are the cost of electricity (COE) which describes how much it costs to generate 1 kWh of electricity taking into account all the expenses to produce this amount of energy (e.g., fuel cost, operation, etc.) and the capital costs (CAPEX). Although the COE seems to be more significant in terms of power plant benefits, a low CAPEX will attract stakeholders to invest in it. For this reason, the same weight (50%) has been assigned to both factors.

**Table 4:** Net efficiency and level of readiness of each selected cycle

	<b>AZEP 100% [16, 17]</b>	<b>CCGT [28]</b>	<b>CES [8]</b>	<b>E-MATIANT [14]</b>	<b>Modified Graz [10]</b>	<b>NetPower [50]</b>	<b>SCOC-CC [11]</b>
<b>Net Efficiency (%)</b>	47.9	58	43.6	47	53.1	55.1*	49.8**
<b>Readiness</b>	4	9	7	5	5	6	5

\*this value is attributed by independent researchers [52] which lies between the one provided by the company [9] and Llorente [38], 58.9 and 51.9%, respectively.

\*\*this value approximates efficiencies presented in other studies [53, 54]

The economic data provided for each cycle have different assumptions depending on factors such as the power plant size, the fuel price, the discount rate, etc. Thus, in order to show the results and make them comparable, the costs for each cycle have been divided by the costs for its reference plant (CCGT), obtaining a ratio that represents their overcost. For instance, taking into account a COE of 39.5 €/MWh for the CCGT and 53.32 €/MWh for the AZEP 100% the COE overcost ratio is 1.35. The overcost ratio of each cycle is shown in Table 5.

However, it is important to take into account that these costs include the implementation and financing of these cycles as a project but R&D investment is not included, which would increase the cost considerably. This investment will depend on the complexity and novelty of the cycle and components on them but these costs cannot be estimated by the authors of this study.

**Table 5:** CAPEX and COE overcost ratio of each selected cycle

	AZEP 100% [17]	CCGT	CES [55]	E-MATIANT [56]	Modified Graz [10]	NetPower	SCOC-CC [10]
<b>CAPEX overcost</b>	1.23	1	1.36	1.1	1.69	1.27	1.64
<b>COE overcost</b>	1.35	1	1.1	1.1	1.2	1.04	1.26

#### 2.4. Environmental

The environmental aspect of the different cycles has been evaluated based on the Life Cycle Assessment (LCA). This technique assesses the environmental impacts associated with all stages of a product's life from cradle to grave. Hence, it evaluates the equivalent CO<sub>2</sub> emissions per kWh that each cycle releases during the 25 years of its life cycle including the construction of the plant, the emissions emitted during its use considering possible losses in compressors and during transport, the maintenance and repair operations and the demolition of the plant. Table 6 shows these emissions.

**Table 6:** CO<sub>2</sub> emissions for each selected cycle

	AZEP 100% [16]	CCGT [57]	CES	E-MATIANT [58]	Modified Graz	NetPower [31]	SCOC-CC
<b>gCO<sub>2</sub>eq/kWh</b>	19	366	21	29.84	26.1	8	25.33

#### 2.5. Social

With the aim of determining the social opinion related to CCS as well as the public investment in this field, the authors of this report conducted a survey which was answered by 136 people between 17-61 years of age, where most of the respondents (92%) were between 20-30 years old. Moreover, 83% of the samples are science graduates; of these 42% of the degrees are related to sustainability or environmental science. Here the sampling method is based on the convenience sampling procedure where subjects are selected because of their convenient accessibility and proximity to the researcher [59].

Although most of the respondents were science graduates, first of all a brief introduction describing the CCS process was presented in order to provide a closer picture of the topic to the respondents. The samples were not restricted only to people with a degree related with this topic and, thus, have a wider social opinion. Then, the respondents were asked some personal questions related to their



age, their educational background and where they lived (to determine whether their proximity to a power plant affected their survey responses). The survey continued with questions regarding their previous knowledge about CCS techniques and it finished with specific enquiries about their opinion on economic investment by the government for this type of technology.

The results showed that 86% of the respondents would support government investment in CCS technologies, although if they had to choose between CCS and renewable technologies, 82% would choose the latter. From this 82%, 56% claimed not to have heard about CCS before.

Of the 14% who did not support investment in CCS technologies, almost half did not know anything about CCS. The rest noted that they had heard about this concept before but 80% of them were not capable of naming any specific technique.

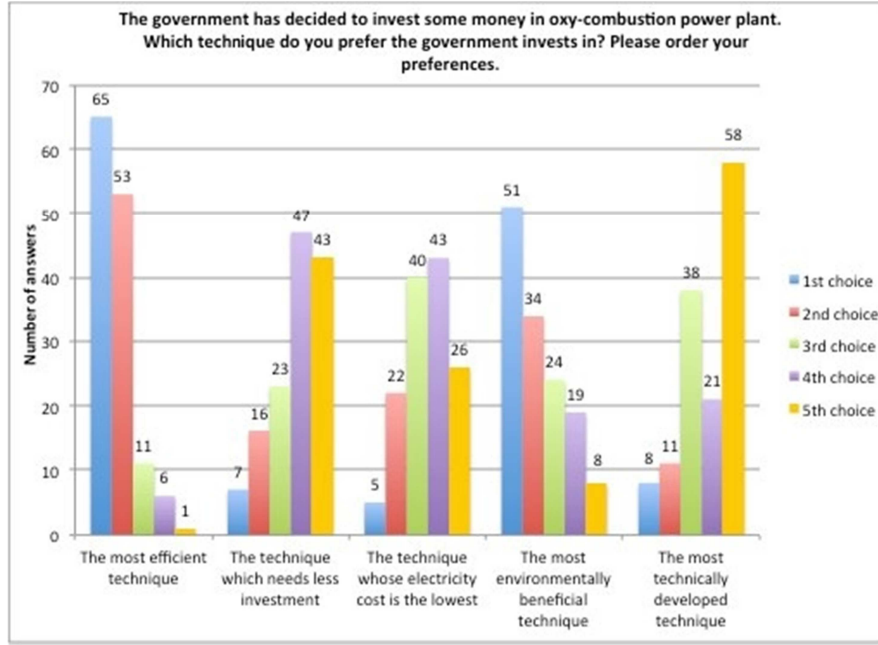
Although 36% of the respondents had some education related to sustainability or environmental science, 37.5% of this 36% had never been told about CCS. 86% of the respondents from this 36% would prefer that the government invested in renewables instead of CCS technologies.

The answers obtained from the survey were compared to the social opinion from the literature. Thus, Van Alphen et al. [60] carried out an analysis in which they state that the social opinion should be divided into two sectors: stakeholders and general public. Stakeholders are agents who have a professional interest in CCS such as the industry, the government and the non-governmental organisations (NGOs), whereas all the other opinions are included in the general public. The authors stated that it is necessary to analyse their opinion because their perception of CCS is quite different; while the stakeholders have knowledge about CCS, the public in general does not have an *a priori* point of view and in many cases its responses to questionnaires are affected by the sparse information provided by the interviewers. The stakeholders' support on CCS technologies is based on five factors: safety, temporality/partiality (it should not be a permanent technique), financial stimulation, cooperation/commitment between the different parties such as government, experts and stakeholders, and open communication with the local communities [61].

All these factors are governed by two facts: renewable technologies should have priority if they can be well established, and both safety and effects should be studied thoroughly before implementing these technologies.

The survey carried out matches with the Van Alphen et al. study in two facts: the general public presents a lack of knowledge on CCS technologies; and society prefers renewable technologies rather than CCS.

In the last question of the survey, the respondents were asked to order different alternatives related to aspects that the government should take into account when investing public funding in a CCS oxy-power plant. The results can be found in Figure 9.



**Figure 9:** Responses to the last question of the survey

The social factor has been studied according to the last question of the survey. Thus, each alternative appeals to a specific cycle characteristic that can be used as a criterion to evaluate the social factor.

Hence, the importance that people gave to the different characteristics has been scored from 1 to 5, 5 being the value attributed to the first-preferred one. This value was obtained using the equation shown below (Eq. 2), normalising it afterwards. Each one of these characteristics has been related to one of the cycle parameters obtained from the literature in order to analyse the different alternatives following an MCDA. The related parameter to each characteristic, score obtained for each factor and its respective normalised value can be observed in Table 7.

$$\text{Weighted Value}_i = \frac{5 \times N_{i,1} + 4 \times N_{i,2} + 3 \times N_{i,3} + 2 \times N_{i,4} + 1 \times N_{i,5}}{N_{total}} \quad (2)$$

$i$  = characteristic

$j$  = 1<sup>st</sup>, 2<sup>nd</sup>, 3<sup>rd</sup>, 4<sup>th</sup> or 5<sup>th</sup> choice

$N_{i,j}$  = Number of answers for characteristic  $i$  as choice  $j$

$N_{total}$  = Total number of respondents (always 136)

**Table 7:** Weighted and normalised values of each characteristic for the social factor

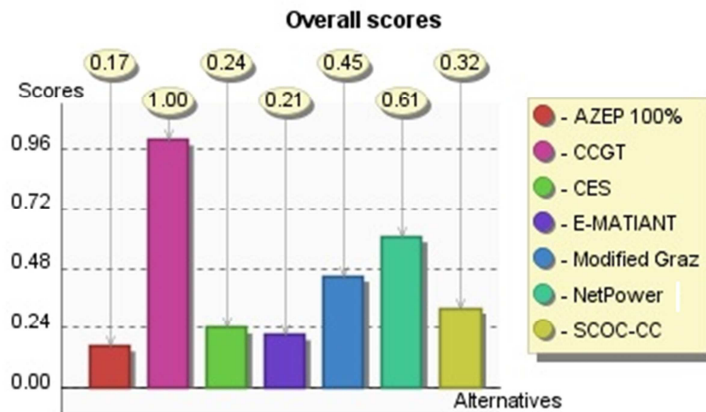
Characteristic	Related Parameter	Weighted Value	Normalised Value
The most efficient	Net efficiency	4.29	0.329
The one which needs less investment	CAPEX overcost	2.24	0.124
The one whose electricity cost is the lowest	COE overcost	2.54	0.154
The most environmentally beneficial	CO <sub>2</sub> eq	3.74	0.274
The most technically developed	Readiness	2.19	0.119

### 3. Results and discussion

When the data were entered in the DECERNS software, one cycle was ranked highest for each factor following a Multi-Criteria Decision Analysis.

#### 3.1 Technological

The best performing cycle in terms of technology is, without considering the CCGT, the NetPower cycle. However, the Modified Graz cycle has a similar score to that of the NetPower. The results of the analysis can be seen in Figure 10.

**Figure 10:** MCDA results for the technological factor

The Modified Graz and NetPower cycles are represented in Figure 11 and Figure 12, respectively.



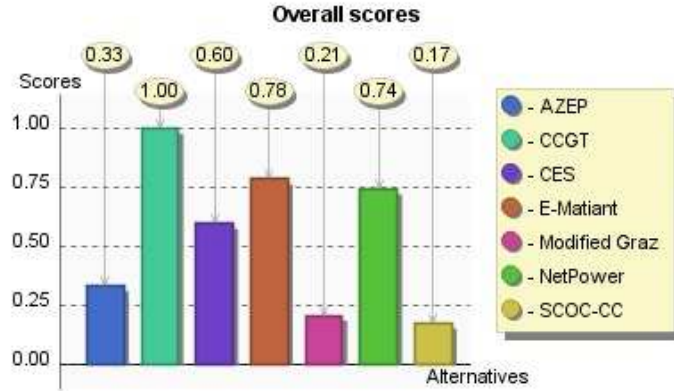


Figure 13: MCDA results for the economic factor

### 3.3. Environmental

Figure 14 shows the overall scores for the different cycles regarding their environmental benefits, meaning that the best cycle in terms of emissions is the NetPower, although the results are skewed because of the high amount of emissions released by the CCGT.

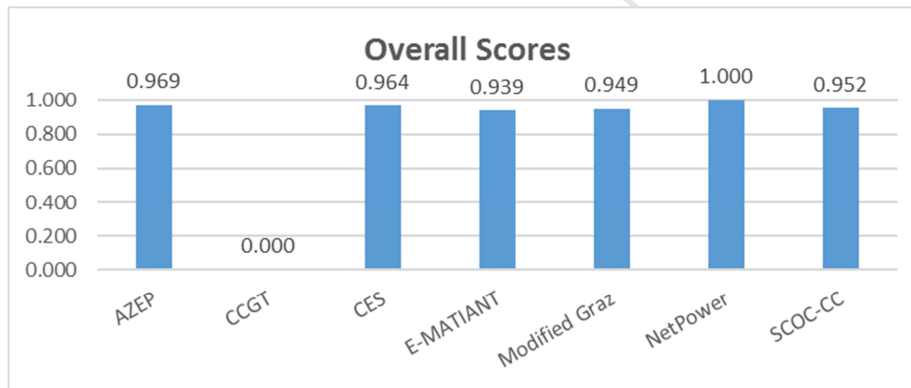


Figure 14: Results for the environmental factor

### 3.4. Social

Following the methodology explained in section 5.5, the social evaluation results are shown in Figure 15.

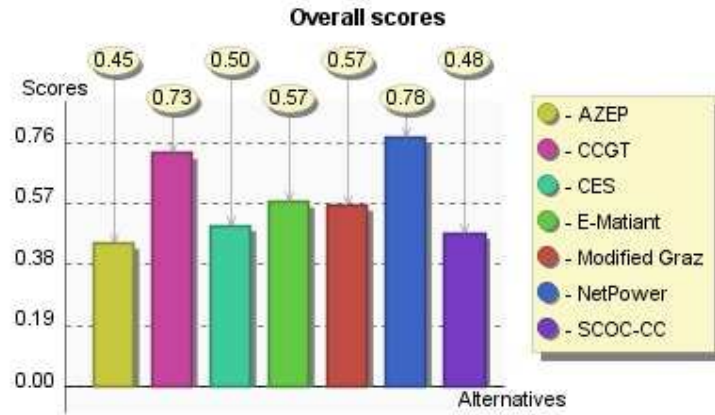


Figure 15: MCDA results for social factor

The NetPower cycle is the best solution in social terms with a higher score even than for the CCGT.

### 3.5. Overall Results

A way of summarising the results provided by the MCDA is by plotting them in a radial graph (Figure 16) where the four axes represent each of the aspects considered above.

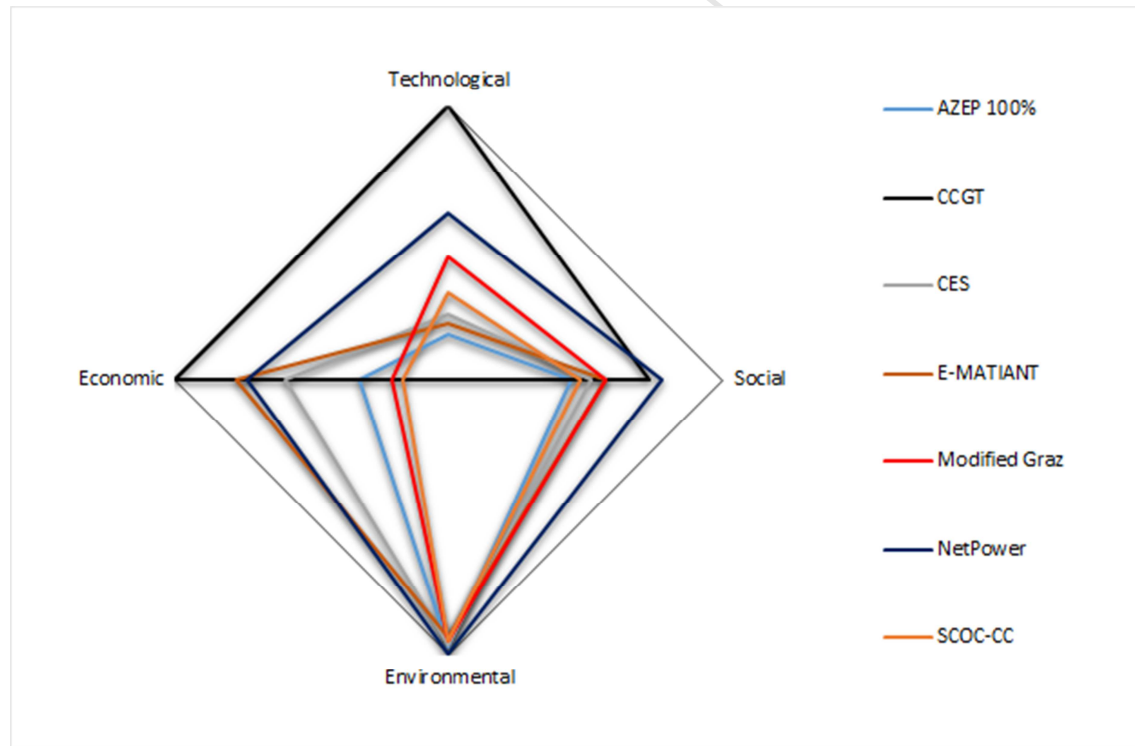


Figure 16: Radial graph of the MCDA results

When all factors are given equal weight, the NetPower is the cycle which stands out from the others, including the CCGT. The assigned weight was equal for each factor because, depending on the sector

that analyses the scenario, the importance given to each factor would vary. Although the CCGT has the maximum score in economic and technological factors, its score of 0 in the environmental factor lowers its overall mark. Figure 17 shows the final multi-criterial results of all the cycles showing that NetPower has the best overall performance.

The NetPower cycle has a simple design offering high efficiency which provides power generation and CO<sub>2</sub> capture with low investment and low COE. Also, if a Life Cycle Assessment is considered [31] it is the lowest in terms of CO<sub>2</sub>e emissions. The main drawback is that the thermodynamic data (e.g., LHV net efficiency) vary markedly depending on the source (company or independent researchers). However, recent publications as well as peer-review have demonstrated a more accurate value compared to past studies [52].

In order to increase the scores for the other cycles, raising them to the NetPower level, their technological and economic aspects must be improved. The adoption of political measures such as CO<sub>2</sub> Tax and Emission Allowances could enhance the undeveloped technologies offering public funding to those technologies that still need to be supported by the government in order to be more attractive economically. However, the result of these measures would be different for each cycle. Hence, more investment by governments would increase the readiness level of cycles but other intrinsic parameters such as the efficiency or the cost in terms of materials and equipment would not vary since they depend on the complexity of the cycles themselves [61].

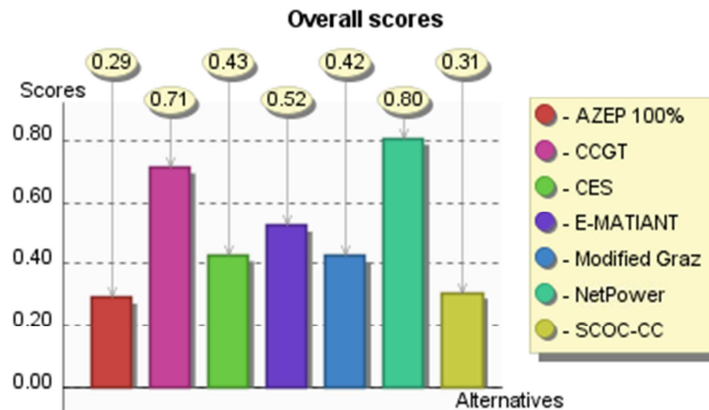


Figure 17: MCDA of the final results

#### 4. Conclusions

Nineteen oxy-turbine power cycles were summarised in terms of their main characteristics and parameters, and six of these cycles were analysed. This technical review concludes most of the cycles (except CES and NetPower) are in the early development stage and mainly studied only from a thermodynamic perspective. Overall, all of the oxy-turbine cycles involve complex schemes which require technically advanced equipment but they offer high efficiencies for power generation, while at the same time, offering nearly perfect CO<sub>2</sub> capture without generating hazardous emissions such as NO<sub>x</sub> and the best overall cycle

efficiencies. Oxy-turbine power cycles also provide net efficiencies up to 65%, comparable to a combined cycle gas turbine (CCGT) power plant (58-60 %).

Renewable sources such as solar, biomass and biofuels have also been proposed in some oxy-turbine cycles. Generally, the application of renewable technologies in these cycles does not provide significant advantages in terms of design and efficiency. However, the benefits of renewable implementation are the reduction in fossil fuel consumption and, in the case of solar, decrease in the required oxygen supply providing this can be done without major loss of efficiency or other problems.

The PESTLE analysis has shown that from a political and legislative point of view, the oxy-turbine cycles need to be supported by government measures that attract stakeholders to invest in these clean technologies. Concerning social opinion, a survey has been carried out in which 136 respondents were asked specific questions regarding CCS. Their answers show that, in general, society is unaware of the existence and requirement for these techniques, which is in agreement with previous studies on the subject. This lack of public knowledge about CCS science causes the public to favour renewable options instead of CCS technologies even when the latter are more cost effective.

From the MCDA, the NetPower cycle was identified as the best option among the oxy-turbine cycles proposed for the PESTLE analysis. Further research needs to be carried out in order to demonstrate the reliability of these cycles in real industrial situations. For instance, high temperatures and flue gas composition cause an aggressive environment which implies that materials selection needs to be carefully addressed and demonstrated in trials carried out over extensive periods.

### **Acknowledgments**

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**Highlights**

- Oxy-turbine power cycles achieve efficiencies as high as combined cycle gas turbines
- They have the extra benefit of full carbon dioxide capture and no nitric oxide emissions
- The main operational parameters of 19 oxy-turbine technologies are evaluated
- A survey was undertaken to obtain a social view of carbon capture and storage
- The best cycle option was identified based on technical, risk and multi-criteria analysis