Wear debris: basic features and machine health diagnostics

M. A. Khan, A. G. Starr

Through Life Support Research Group, School of Mechanical, Aerospace and Civil Engineering,
The University of Manchester, M60 1QD, UK.

Tel : (44) (0) 161 306 5724, Fax : (44) (0) 161 306 4601

muhammad.khan-8@postgrad.manchester.ac.uk

a.starr@manchester.ac.uk

ABSTRACT

Modern high speed and power machinery components like gears, bearings, pumps, hydraulics and motors normally suffer from wear phenomena during operation. The study of wear debris can help estimate the condition of the surface of a component, so its basic features may be used to diagnose component health prior to failure. In this paper, a review is presented of the current literature related to wear debris and its analysis. The basic features of wear debris are highlighted, and their possible potential to diagnose the health of machine components is discussed. The basic features of wear debris have been classified with respect to the approach of measurement for component health diagnostics. In addition, each feature has been detailed with its possible measurement descriptors, its trend during machine component operation, and its distinct health diagnostics capability. Finally the paper proposes advances in machine component health diagnostics solution, by optimising the diagnostic capabilities of basic wear debris features.

Keywords: Wear, wear debris basic features, wear debris detection descriptors, machine component health diagnostics.

1. INTRODUCTION

The term wear debris may be defined as the particles which are generated in a mechanical system (like turbines, generators and engines), when the system components (like gears and bearings) are degraded due to wear phenomena in such a way that the degradation causes material loss. In common observation the wear debris is basically solid, but properties like softness or elasticity may tend the shape to be similar to slurry rather than a solid ⁽¹⁾. Usually debris is formed from the surface interactions of components of any system, so basic features of the debris may contain valuable information regarding the wear mechanisms, the modes occurring at the location of interaction and the effects of wear on component health ⁽²⁾.

It is observed that wear debris particles are widely varying in size, distribution and other feature properties, but that their source and behaviour is important in condition monitoring and maintenance decision-making. In the sections below we consider classification, size, quantity and concentration and their trends, the size distribution, shape, and composition. The treatment is generalised across a wide range of machinery, so precise dimensions have been deliberately omitted in places – a particle which is “large” for a hydraulic system is trivial in a marine gearbox – but trends in behaviour are emphasised.

2. CLASSIFICATION OF WEAR DEBRIS BASIC FEATURES

With respect to the approach of debris measurement for the determination of component health diagnostics, wear debris basic features, can be classified into three categories ^(1 – 15):

- Quantitative;
- Qualitative;
- Material properties.

The wear debris features within these three categories are shown in table 1.

Classification Category	Quantitative	Qualitative	Material
Basic Features	<ul style="list-style-type: none"> • Size • Quantity/Concentration • Size distribution 	<ul style="list-style-type: none"> • Shape 	<ul style="list-style-type: none"> • Composition

Table 1. Classification of wear debris basic features

3. QUANTITATIVE FEATURE ‘SIZE’

The bodily magnitude of any wear debris is usually termed its size. But factors like porosities, surface roughness and complexity in the physical contours make it hard to define an accurate measurement scheme for size.

According to the literature ^(4, 16), two types of measurement descriptors can be used to measure the size of wear debris, as detailed below.

3.1. Optical size measurement (OSM) descriptors

OSM descriptors are used to determine the size of wear debris by means of visual dimensional analysis. The following are some useful OSM descriptors.

- Largest diameter – the longest dimension of wear debris.
- Feret’s diameter – the maximum distance between two parallel lines, set at a fixed angle and just touching the physical contour of the wear debris. (The debris should be positioned in a defined orientation).
- Martin’s diameter – the breadth of wear debris, where a fixed angle line bisects the debris overall projected area into two equal areas.
- Volume diameter – the diameter of a sphere whose volume is the same as that of the wear debris.
- Free falling diameter – the diameter of a sphere having the same free-falling speed as the wear debris.
- Stokes’s diameter – the free falling diameter in the laminar flow region.
- Axial ratio – the ratio of breadth and longest dimension of the wear debris.

3.2. Non-optical size measurement (NSM) descriptors

NSM descriptors are used to determine the size of wear debris by correlating its physical actions to its size value, for example the ability of the debris to block the machine lubricant lines or choke the filters. Similarly the strength of the wear debris can act as an attribute to increase the component wear phenomena.

3.3. General trends of wear debris ‘size’ features in machine component operation

The trends of wear debris size are different for different types of wear occurring during machine component operation. For steel and steel based alloys, the following five basic wear types dominate, according to Anderson ⁽¹⁷⁾ and Bowen et al ⁽¹⁸⁾.

- Rubbing/break in wear – found as normal benign wear in sliding surfaces.
- Cutting – usually occurs as abnormal abrasive wear due to the interpenetration of sliding wear.
- Rolling fatigue – usually occurs in rolling element bearings and gear systems as a result of fatigue wear mode.
- Combined rolling and sliding – occurs in the abnormal wear regime of wear fatigue mode and scuffing wear.

- Severe sliding – occurs due to excessive load and high speed.

The trends of wear debris size for the above are given in table 2.

3.4.Diagnostic capability of the wear debris ‘size’ feature

Information from the quantitative size features is distinctly useful for diagnosing wear process severity during machine component operation, according to Roylance and Raadnui ⁽¹⁰⁾. As the size of wear debris increases, so the area of surface degradation on the machine component increases too. And as the surface degradation area on machine component increases, so does the severity of the wear process taking place. Mathematically we can say,

$$\text{Wear debris size} \propto \text{Wear process severity} \quad (1)$$

4. QUANTITY AND CONCENTRATION

The total physical amount of wear debris present in the lubricant of any machine is commonly termed its quantity or concentration. Regardless of its appropriateness, the term ‘mass’ for this feature is not often used in the available literature on wear debris.

4.1. Quantity measurement descriptors

The following five basic quantity measurement descriptors can be used for wear debris, according to Leschonski ⁽¹⁹⁾.

- Number – utilizing a counting process for wear debris quantity
- Length – measuring the length of the surface where all the wear debris are placed.
- Area – measuring the physical area of the surface where all wear debris are placed.
- Volume – utilizing volume measuring apparatus for quantifying wear debris.
- Weight/mass – for example the increased weight of a filter paper due to the wear debris after a lubricant sample is filtered.

4.2.General trends of quantity features in machine component operation

Tracking the wear progress through monitoring of the wear debris concentration or quantity as a function of time is one of the primary objectives of condition monitoring for a machine component. Moubray⁽²⁰⁾ has described six patterns to represent the range of possible trends of the quantity during any machine component operation. By using these patterns, hypothetical quantity feature trends during machine component operation are explained below in the context of wear.

4.2.1. Trend-1

In this trend, as shown in figure 1, wear debris are initially generated in large quantity with a decreasing trend (“running in” wear). This is similar to the common “bath tub” curve, usually applied to the whole life population-specific failure rate or hazard plot. With time the decreasing trend stabilizes and then follows a zone of operation in which wear debris are generated at a constant rate. This is termed the middle zone or “useful life” period. As the time passes, the middle zone comes to an end and once again wear debris are generated in large quantity but this time with increasing trend, which continues until component failure.

4.2.2. Trend-2

In trend 2, as shown in figure 2, as operation starts, wear debris are generated at a constant rate. This constant mode remains for most of component life, and is followed by a failure zone at the end, in which a large quantity of wear debris is generated with increasing trend.

4.2.3. Trend-3

In trend 3, as shown in figure 3, the wear debris quantity increases linearly with time.

4.2.4. Trend-4

In trend 4, as shown in figure 4, at the start the wear debris is generated in large quantity with increasing trend, but after some time the trend of quantity generation becomes constant and remains so until component failure.

4.2.5. Trend-5

In trend 5, as shown in figure 5, wear debris generation is constant throughout the whole component life.

4.2.6. Trend-6

In trend 6, as shown in figure 6, at the start the wear debris is generated in large quantity with decreasing trend, but after some time the trend of quantity generation becomes constant and remains so until component failure.

4.3. Diagnostic capability of the wear debris quantity feature

The information contained in the quantitative features of wear debris analysis distinctly diagnoses wear rate during machine component operation, according to Neale et al⁽²¹⁾. From the trend discussion above, it may be understood that during the whole life cycle of a machine component, generated wear debris appear at different rates. By the study of the quantity features, one can determine the rate of wear by using following relationship.

$$\text{Wear rate} = \frac{\text{Current wear debris level} - \text{Immediately previous wear debris level}}{\text{Time between the measurements}} \quad (2)$$

5. QUANTIFICATION OF SIZE DISTRIBUTION

The wear debris size distribution changes during the component life, and is one of the key characteristics which can be used as the basis for machine health diagnosis. It is basically a representation of overall wear debris generated during any machine wearable component operation with respect to size. But the effectiveness of diagnosis on the basis of this characteristic will become less as contamination in the system increases⁽²²⁾.

5.1. Size distribution measurement descriptors

There are number of ways to measure the size distribution of generated wear debris during machine component operation, but two broad classifications can be made^(17, 19, 22-24).

- Statistics based descriptors – based on metrics like mean, standard deviation, skewness and kurtosis.
- Probability based descriptors – based on probability functions like uniform distribution, exponential distribution, normal distribution, gamma distribution and Weibull distribution.

5.2. General trends of wear debris size distribution in machine component operation

In machine systems there are generally three major operating zones from initiation to failure: running in, useful operation and rapid wear. The zones are influenced by different wear modes and different trends of wear debris size distribution. Figure 7 demonstrates the variability in size distribution trends from initial life to failure of the machine system.

As illustrated in figure 7, during the initial stages or running in zone, the machine component begins to be affected by the wear process and small particles are generated at a high rate, usually attributed to the removal of asperities left by manufacturing processes. As the system passes this running-in zone, no important change in size distribution is observed. Only the quantity rate is decreasing, and the size of generated debris is consistent which does not alter the size distribution curve. But as the machine component leaves this running-in zone, an increase in size and a gradual decrease in rate of quantity of generated debris occurs. With size increasing and quantity rate decreasing, the machine component

enters into the useful operating life zone. This zone possesses an overall uniform size distribution trend of particles larger in size, but smaller in quantity, than running-in wear. And at the end of this useful operating life zone, the machine component enters the rapid wear zone, in which both rate of quantity and size of generated debris increase rapidly and the rising trend continues until ultimate failure.

It should be noted that small debris may be counted in very large numbers, in the order 10^6 to 10^8 particles per 100ml for some machines, while the large debris in the wear zone may be counted in much smaller numbers, in the order 10^4 to 10^6 particles per 100ml⁽²⁵⁾.

5.3.Diagnostic capability of the wear debris size distribution

The information obtained from the quantification of the size distribution of the wear debris diagnoses zones of wear and their transition times during machine component operation. Through the determination of zones of wear and the wear transition time, a useful conclusion for machine component health diagnostics and prognostics can be made. The transition from the useful operational life zone to the rapid wear zone is of particular interest, because it gives a clear warning of the onset of an irreversible degradation and finite life.

6. QUALITATIVE FEATURE ‘SHAPE’

Generally, the term shape for wear debris denotes two distinct characteristics of the debris, which are form and proportions⁽²⁶⁾. Form describes the tendency of a particle to become a definite geometrical (either regular or irregular) structure like a cube or a sphere. While proportion describes the relative ratio of difference between the same class of geometrical structures like cuboids and spheroids. To define the shape of wear debris in a more comprehensive way, this relative ratio of difference may be further analyzed in qualitative terms, e.g. debris edge details and its surface texture.

6.1.Shape measurement descriptors

Physical form, edge details and surface texture, which are the three basic characteristics of shape feature, have a large variety of descriptors for their measurements. Some of the important ones are listed below ^(4, 10, 16).

6.1.1. Physical form measurement descriptors

These descriptors are based on debris macroscopic dimensional analysis.

- Aspect ratio – length to width ratio of debris.
- Elongation – length to width ratio along the debris shape.
- Roundness.
- Circularity.
- Sphere diameter – ratio of two times debris area and its perimeter.

6.1.2. Surface texture and edge detail measurement descriptors

These descriptors are based on microscopic dimensional analysis of the particles.

- Fourier descriptor – consists of finding the centre of gravity of debris and its perimeter.
- Fractal dimension – an irregular debris shape enclosed by polygons of constant sides. These sides and perimeter of polygons determine the characteristic surface texture factor.
- Curvature determiner – using changes of angle that occur along the perimeter by successively moving three adjacent points on debris, and measuring the inclusive angle formed by the projecting two lines through the points such that they intersect at the middle point.

6.2.General trends of shape features in machine component operation

General trends of the wear debris shape features can comprehensively understood by describing the trends with respect to its physical appearance, as described in table 3 ^(1, 4, 5, 21, 27). There are several types of shapes observed, and attention must be paid to their specific sizes, because these are linked to particular degradation mechanisms. Shapes include spheres, ovoids, chunks and slabs, platelets and flakes, curls, spirals and slivers, rolls and long thin particles. Generally the trend is increasing quantity and size with severity.

6.3.Diagnostic capability of wear debris shape features

Information arising from the qualitative shape features from wear debris may be used to diagnose both the wear type and mode ^(1, 3, 5, 7, 10, 28). All the five wear types as discussed above in section 3.3 have distinguishable shape features, as illustrated by figure 8 shown below. As a result, the shape can help identify the likely wear types occurring in the machine component. The wear type can then be used to predict the wear mode by utilizing the mapping as provided in figure 9.

7. MATERIAL FEATURE: COMPOSITION

By using the diagnostic capabilities of both quantitative and qualitative features, it is possible to establish appropriate alarms and limits to predict and identify impending machine component failure. But in order to further localize the source of the wear metal production, and hence guide the necessary maintenance actions, information on composition is important⁽²⁹⁾. The chemical composition of the wear debris is able to provide a much better idea of the source, as compared to the other characteristics like shape and size distribution.

7.1.Composition measurement descriptors

The descriptors of composition vary widely according to the type of measurement techniques. The most common descriptors are described below in two separate categories ^(1, 4, 5, 21).

7.1.1. Micro property descriptors

- Elemental content – the percentage of different elements in a wear debris oil sample is measured by atomic absorption or emission spectrometry.
- Molecular content – the percentage of different molecular structures in a wear debris oil sample can be measured by infra red spectrometry.

7.1.2. Macro property descriptors

- Colour
- Impact hardness
- Relative density
- Conductivity
- Polarity
- Specific heat capacity

7.2.Elements and their sources in general machine components

Hunt presented a detailed chart of elements and their related components in general mechanical systems^(1, 4). It covers the main 20 elements and their respective sources as given in table 4. It may be observed that the main machine elements are broadly distinguishable because of different basic composition, alloying or additives. It is also important to note that some components of similar composition would be indistinguishable from each other unless labelled, e.g. with a different alloy.

7.3.Diagnostic capability of the composition of wear debris

The most prominent diagnostic capability of the composition of wear debris is to localize the source as discussed above. This can be considered to be an advanced diagnosis, because it becomes important after the initial detection of change, and the advancing trend of other patterns discussed above, such as quantity. Some techniques can combine the monitoring of both composition and quantity, as long as limitations of the technology are considered – for example, spectrometric techniques will vaporise small particles suspended in the oil, but may have problems handling large particles.

8. CONCLUSIONS AND FURTHER WORK

This paper has reviewed wear debris classification, the analysis of size, quantity and concentration and their trends, size distribution, shape, and composition. An ideal diagnostic model for a machine system and its components should give an early diagnosis of degrading health, with accurate prognostics to enable maintenance decisions to be made, well before damage and catastrophic failure. However, it is difficult to establish such a model for a real machine, for the following reasons.

- The machine component working behaviour or trend cannot be predicted exactly. The estimation of future behaviour is always subject to uncertainty.
- Debris feature extraction and calculation techniques require compromises and assumptions due to the complex and intricate detail properties of the debris.
- The development and application of an ideal diagnostic model on a maintainable machine system may be excessively costly.
- Currently detection techniques are not capable of diagnosing all features in real time.

There are several ways to optimise a model by further research. Considering the capabilities of wear debris machine component health diagnostics discussed above, a hypothetical component health diagnostic model is proposed below.

8.1.Hypothesis for a component health diagnostic model

For a hypothetical component health diagnostic model, five features of measurement descriptors for size, quantity, size distribution, shape and composition are proposed in table 5, with their reasons for selection. The proposed diagnostic model is based on these five descriptors and one diagnostics information evaluator as illustrated by figure 11 and figure 12.

In figure 11, the descriptors are shown by the inputs A_i , B_i , C_i , D_i and E_i applied to the wear debris. On application, they will generate useful diagnostics within their capabilities. A diagnostic evaluator is also included, which takes the diagnostic information (i.e. the outputs A_o , B_o , C_o , D_o and E_o as shown in figure 11) and applies the evaluation rules as shown in figure 12. The component health diagnosis is performed by an intelligent rule application process. The illustrations of the model (figure 11 and 12) are intended to generate machine health information like wear severity, rate, mode, type, source, zone and transition time, by using well defined evaluation rules.

8.2.Future work

The model hypothesis above is a proposal and verification will be performed by the doing the following future work:

- experimental work using offline sampling on a gear tester machine to check the authenticity of the diagnostic capabilities of basic wear debris features as discussed above;
- basic wear debris feature descriptors will be modified after validation (if required) and then implemented;
- automation of the proposed model from debris collection to machine health estimation will be developed and validated.

Table Captions:

Table 2	Size trends vs Wear particle type ⁽¹⁷⁾
Table 3	General trends of debris shape in machine system ^(1, 4, 5, 21, 27)
Table 4	Elements mapping with possible sources ⁽⁴⁾
Table 5	Measurement descriptors for hypothetical component health diagnostic model

Figure Captions:

Figure 1	Quantity feature Trend 1
Figure 2	Quantity feature Trend 2
Figure 3	Quantity feature Trend 3
Figure 4	Quantity feature Trend 4
Figure 5	Quantity feature Trend 5
Figure 6	Quantity feature Trend 6
Figure 7	Size distribution trend for a general machine component operation ⁽²¹⁾
Figure 8	General wear debris shapes
Figure 9	Different shapes of different wear type debris ⁽²⁸⁾
Figure 10	Mapping between wear types and wear modes ⁽¹⁾
Figure 11	Proposed wear debris features diagnostic model
Figure 12	Diagnostic Evaluator

Table-2:

S.No	Wear type	Wear debris size trends
1	Rubbing wear/Break in wear	0.5 μ m –15 μ m or less in major dimension / 5 μ m - 15 μ m and for worst condition it may increase to 50 μ m - 200 μ m and can increase more if an interaction occurs between break in wear and excessive contamination. Major dimension to thickness ratio is 10:1 for large particle and 3:1 for small particle i.e. 0.5 μ m.
2	Cutting wear	2 μ m - 5 μ m wide & 25 μ m - 100 μ m long and due to effect of contaminants the available range is 0.25 μ m with 5 μ m.
3	Rolling fatigue <ul style="list-style-type: none"> Spall particles Spherical particles Laminar particles 	10 μ m - 100 μ m with a major dimension to thickness ratio of 10:1 3 μ m - 10 μ m 20 μ m - 50 μ m with a major dimension to thickness ratio of 30:1
4	Combined rolling and sliding	2 μ m – 20 μ m with a major dimension to thickness ratio between 4:1 to 10:1
5	Severe sliding wear	>15 μ m with major dimension to thickness ratio of 10:1 (approx.)

Table-3:

S.No.	Physical Appearance	Possible Sketch	Possible origins	Possible Trends in machine wear
1	Spheres (Metallic spheres between of 0.5µm to 20µm in diameter)	See figure 8	1. Metal fatigue (especially in bearings) 2. Welding 'sparks' 3. Glass peen beads	Usually spherical particles start to appear around 60% through the life of bearing. By 80% - 90% through the life they usually can be observed in large quantities, increasing rapidly towards failure.
2	Distorted Smooth ovoids (pebbles or granular) 1. Black granular particles of iron oxide vary in size up to 150 µm but more are less than 5 µm in length. 2. Orange or red granular particles of iron oxide vary in size up to 150 µm. 3. Atmospheric particles, usually sand and grit, swarf, rust, paint etc.	See figure 8	1. Oxidative wear of iron 2. Quarry dust 3. Atmospheric dust from material like seals, breather etc.	Black and orange granular particles are mostly due to oxidative wear and commonly caused by excessive component operating temperatures and/or inadequate lubrication. Atmospheric particles enter inside the machine system due to poor sealing and may intensify the wear process or make blockage in lubricant paths.
3	Chunks and slabs (Coarse, dull grey appearance with highly polished bright spots, irregular metal particles with length and width and thickness of same order of about 1mm during severe pitting)	See figure 8	1. Metal fatigue (surface fatigue of gears) 2. Bearing pitting 3. Rock debris	Fatigue spalls, pitting and break up produce chunks of sharp rough metals. While rough slabs are generated by sliding action or by fatigue involving very high temperature or inadequate lubrication.
4	Platelet and flakes 1. Very large metal flakes often above 1 mm in length, some times appearing as rounded petals. 2. Large metal flakes about 1 mm in length. Usually curled rectangular in shape. 3. Medium size flakes of 150 µm to 1 mm size in length, severely torn and plastically worked. Solder-like balls can also be formed for low melting point materials. 4. Medium sized flakes of 15 µm to 1 mm size in length, roughly torn with evidence of plastic flow. 5. Small sized flakes of 1 µm to 15 µm in length	See figure 8	1. Fatigue failures of plain, rolling and ball bearing 2. Piston rings scuffing 3. Plain bearing wiping 4. Piston cylinders 5. Surface fatigue of gears	1. Very large flakes usually appear in rapid failure zone and their presence shows that total failure is likely to be imminent. 2. Large flakes are usually very thin with feathery edges caused by surface fatigue in rapid failure zone. 3. Medium size flakes usually appear when catastrophic sliding wear occurs, which tends towards a complete breakdown of component surfaces. 4. Medium size flakes are often found when soft materials (like a piston) are under wear; due to localized adhesion they tend to exhibit larger particles and higher wear rates. 5. Small metal flakes are often found during running-in wear.

	with 1 μm or less in thickness.			Many of these flakes are formed during the starting and stopped of a machine.
5	Curls, spirals and slivers	See figure 8	Machining debris produced at high temperature	The spiral debris is produced by a ploughing action in valves and bearings where a harder part of a component, or a sharp ingested particle, digs into softer surface. Usually occurs in loose fitting components like poor housing to a bearing race.
6	Rolls	See figure 8	Probably similar to platelets but in rolled form	A roll is a sort of combination of spiral and platelets. Their generation and behaviour in a wear process is same as platelets.
7	Long thin particles 1. Large metal splinters of several mm in length 2. Smaller splinters of metal of about 1mm in length 3. Tiny short hair-like strands of metal about 100 μm in length 4. Miniature metal, spirals, loops and bent wires of about 100 μm in length. 5. Rolling pins of polymeric materials with a size 5 μm to 25 μm in length.	See figure 8	1. Labyrinth seals 2. Gear teeth, Circlip washer etc. 3. Needle roller bearing 4. Polymers	Usually an increase of long thin particles shows an indication of metal deterioration increase. Thin particles like polymeric materials can cause increase in severity of wear specially in manufacturing machine systems by acting as contaminants.

Table-4:

S.No.	Element	Possible Sources
1	Aluminium	Spacers, shims, washers, pistons on reciprocating engines, cases on accessories, bearing cages in planetary gears, crankcase in reciprocating engines and bearing surfaces.
2	Antimony	Bearing alloys, grease.
3	Barium	Oil additive, grease, water (leaks).
4	Boron	Seals, airborne dust, water, coolants.
5	Calcium	Oil additive, grease, some bearings.
6	Chromium	Plating metal, seals, bearings cages, piston rings, cylinder walls in reciprocating engines, chromate corrosion inhibitors.
7	Copper	Main or rod bearing thrust bearings, wrist pin bushes, oil coolers, gears, valves, turbocharger bushes, washers, copper radiator.
8	Iron	Cylinder walls, valves guides, rocker arms, piston rings, ball and roller bearings, bearing races, spring gears, safety wire, lock washers, locking nuts, locking pins, bolts.
9	Lead	Bearing metal, seals, solder, paints, grease.
10	Manganese	Valves, blowers, exhaust and intake systems.
11	Magnesium	Aircraft engine case for accessories, component housing, marine equipment.
12	Molybdenum	Piston rings, electric motors.
13	Nickel	Bearing metal, valve train metals, turbine blades.
14	Phosphorus	Coolant leak, Oil additive.
15	Silicon	Airborne dust, seals.
16	Silver	Bearing cages, puddle pumps, gear teeth, shafts, bearing in reciprocating engines.
17	Sodium	Coolant leaks, grease, marine equipment.
18	Tin	Bearing metal and thrust metal bushes, wrist and piston pins, pistons, rings, oil seals, solder.
19	Titanium	Bearing hub wear, compressor blades and discs especially in aero engines.
20	Zinc	Brass components, neoprene seals, grease, coolant leaks, oil additives

Table-5:

Basic wear debris feature	Measurement descriptor and possible working definition	Reason for selection
Size	Largest calculated diameter (LCD) The LCD descriptor is proposed, based on a smart algorithm incorporating all the possible OSM size measurement descriptors. The algorithm will return the largest calculated diameter.	From the discussion 3.1, all the OSM parameters use visual dimensional analysis. This measures a dimension of wear debris bodily appearance, representing surface degradation of the component. So by using LCD as a size measurement descriptor, the possible largest surface degradation on the machine component may be determined. This degradation may also provide a good diagnosis of wear severity. Wear severity is a critical diagnosis of health, as indicated by the size of wear debris.
Quantity	Number and Density determiner (NDD) NDD is proposed as to be a combination of number and derived density descriptors of quantity feature, derived from mass and volume descriptors.	By proposing a combination of number and density, the main aim is to determine the wear rate of machine component in terms of number (counts of debris) as well as in terms of physical level. Through combination of these two a diagnosis of health and wear rate will be achieved.
Size distribution	Statistical probability distributor (SPD) SPD is proposed as an algorithm combining four statistical descriptors (mean, standard deviation, skewness and kurtosis) with probability based descriptors. It will initially determine the values of the descriptors and determine the trend for the observed wear debris sample. The trend will be guided for predictive curve fitting from probability based descriptors.	By utilizing the SPD descriptor, trends of the size distribution in wear debris samples can be handled.
Shape	Shape factor (SF) SF is proposed as a combination of aspect ratio, fractal dimension and curvature determiner descriptors of the shape features of wear debris. Aspect ratio is proposed for determination of physical form, fractal dimension is proposed for surface texture and a curvature determiner is proposed for analyzing edge details of wear debris.	By using the SF, all three shape feature basics (physical form, surface texture and edge detail) are comprehensively described and measured.
Composition	Derived macro property factor (DMPF) DMPF is proposed to be as a combination of macro property descriptors like colour, specific heat capacity, conductivity etc.	The determination of novel research directions is the main aim of the DMPF descriptor, because no mature research is available for determining such a descriptor that can utilize the physical properties of wear debris for the determination of its composition.

Figure 1:

Figure 2:

Figure 3:

Figure 4:

Figure 5:

Figure 6:

Figure 7:

Figure 8:

Rolls

Long thin particles

Spheres

Chunks and slabs

Platelet and flakes

Distorted
Smooth Ovoids

Curls, Spirals and
Slivers

Figure 9:

Figure 10:

Figure 11:

Figure 12:

REFERENCES

1. B. J. Roylance and T. Hunt, 'Wear debris analysis', First edition, Coxmoor Publishing, 1999.
2. N. Myshkin, L. Markova and A. Grigoriev, 'Condition Monitoring and Predictive Analysis of Tribosystems by Wear Debris', Practising Oil Analysis Magazine, March 2005.
3. K. Xu, A.R. Luxmoore and F. Deravi, 'Comparison of shape features for the classification of wear particles', Engineering Applications of Artificial Intelligence, Vol 10, No 5, pp 485 – 493, 1997.
4. T. Hunt, 'Wear debris analysis and particle detection in liquids', Elsevier Applied Science, 1993.
5. A. Davis, 'Handbook of condition monitoring techniques and methodology', First edition (edited), Chapman and Hall, 1998.
6. M. Flanagan, J. R. Jordan and H. W. Whittington, 'Wear debris detection and analysis techniques for lubricant based condition monitoring', Journal of Physics, Vol 21, No 11, pp 1011-1016, 1988.
7. B. J. Roylance, J. A. Williams and R. Dwyer Joyce, 'Wear debris and associated wear phenomena fundamental research and practice', Proceedings of Institution of Mechanical Engineers, Vol 214, Part J, pp 79 – 105, February 2000.
8. T. P. Sperring and T. J. Nowell, 'Syclops – A qualitative debris classification system developed for RAF early failure detection centers', Tribology International, Vol 38, No 10, pp 898- 903, June 2005.
9. V.F. Leavers, 'Classifying wear debris particles with automatic image analysis', Article in Practising Oil Analysis Magazine, November 2005.
10. B. J. Roylance and S. Raadnui, 'The morphological attributes of wear particles - their role in identifying wear mechanisms', Wear, Vol 175, No 1, pp 115 -124, 1994.
11. L. Hentschel and N. W. Page, 'Selection of descriptors for particle shape characterization', Journal of Particle and Particle System characterization, Vol 20, No 1, pp 25 -38, February 2003.
12. W. Huysman, 'Utilizing analytical Ferrography for root cause analysis and failure prevention', http://www.reliabilityweb.com/art05/analytical_ferrography.htm. [Last accessed: May 2006]
13. S. Raadnui and B. J. Roylance, 'Classification of wear particle shape', Lubrication Engineering, Vol 51, No 5, pp 432 - 437, 1995.
14. G. W. Stachowiak, 'Wear Materials, Mechanisms and Practice', Edited, John Wiley and Sons, 2005.
15. J. Fitch, 'A much closer look at particle contamination', Practising Oil Analysis Magazine, September 2005.
16. T. Allen, 'Particle size measurement', Fifth edition, Vol 1, Chapman and Hall, 1997.
17. D. P. Anderson, 'Wear particle atlas', Report NAEC-92-163, Naval Air Engineering Centre, 1982.
18. R. Bowen et al, 'Ferrography', Tribology international, Vol 9, pp 109 – 115, 1976.
19. K. Leschonski, 'Representation and Evaluation of Particle Size Analysis Data', Journal of Particle and Particle System Characterization, Vol 1, No 3, pp 89 - 95, 1984.
20. J. Moubray, 'Reliability-centred maintenance', Second edition, Butterworth Heinemann, 1997.
21. M. Neale and associates, 'Guide to the condition monitoring of machinery', HMSO, 1979.
22. G. Pocock, 'Particle size analysis for machinery health monitoring', Nature, Vol 270, pp 414 - 415, 1977.
23. N. R. J. Fieller et al, 'Statistics of particle size data', Applied statistics, Vol 41, No 1, pp 127- 146, 1992.
24. B. J. Roylance and G. Pocock, 'Wear studies through particle size distribution-I', Wear, Vol 90, No 1, pp 113 -136, 1983.
25. Heywood, 'Symposium on particle size analysis', Institution of Chemical Engineering Supplement 25, 14, 55, 1947.
26. A. Starr, 2005, Merging Condition Monitoring Data and Knowledge, I Mech E Seminar 1116: The use of on-line sensor technology in condition monitoring to improve maintenance, Farnborough UK
27. Y. Jin and C. Wang, 'Spherical particles generated during the running-in period of a diesel engine', Wear, Vol 131, No 2, pp 315 -328, 1989.
28. S. Raadnui, 'Wear particle analysis – utilization of quantitative computer image analysis: a review', Tribology International, Vol 38, No 10, pp 871 -878, October 2005.
29. J. Fitch, 'Maximizing fault detection in rotating equipment using wear debris analysis', Practising Oil Analysis Magazine, March 1999.

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Khan, M. A.

British Institute of Non-destructive Testing

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